



COMUNE DI AREZZO

PNRR MISSIONE 5 - COMPONENTE 2 - INVESTIMENTO 2.1 - CUP B11B21002280005 -
PROCEDURA NEGOZIATA PER L'APPALTO DELLA PROGETTAZIONE ESECUTIVA E DEI
LAVORI INERENTI LA REALIZZAZIONE DI UNA PISTA CICLABILE DI COLLEGAMENTO
TRA CECILIANO E LA ROTATORIA POSTA ALL'INTERSEZIONE TRA LA SP1 SETTEPONTI
E LA TANGENZIALE URBANA. CIG 9834798C0BI

IMPRESA ASSEGNATARIA:
LAMBERTO GOTTARDI
Loc. Battifolle, 75 - 52100 Arezzo



PROGETTO ESECUTIVO

PROGETTISTI:

Ing. Pietro Cretella
Loc. Vignale, 2 - 52100 Arezzo



COORDINATORE DELLE SICUREZZA:

Ing. Pietro Cretella
Loc. Vignale, 2 - 52100 Arezzo

Ing. Enrico Gennai opere strutturali
Via XXV Aprile, 82 - 52100 Arezzo

RUP Comune di Arezzo:

Ing. Roberto Bernardini
Direttore Ufficio Mobilità

P.I. Massimo Pasquini imp elettrici
Loc. Bagnoro, 17/F - 52100 Arezzo

OGGETTO DEL DISEGNO:
FASCICOLO DEI CALCOLI

SCALA DEL DISEGNO

NUMERO DEL DISEGNO:

A9

Emittitore	Fase	Lotto	Zona	Specialità	Indice	N°	Revisione
	ESEC	unico					
Mod	Data	Descrizione	File				
	12-2023	esecutivi	pista ciclabile Case Nuove Ceciliano				

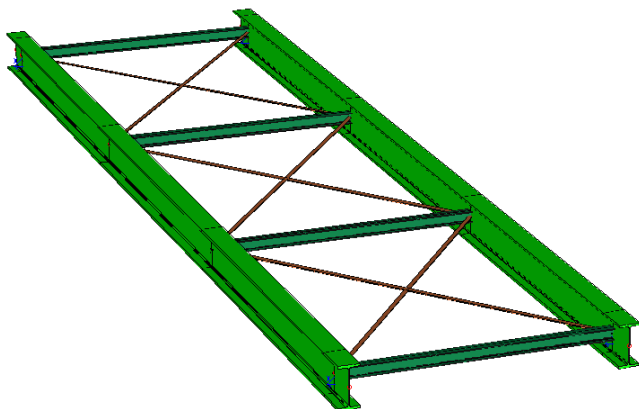
Timbri e firme

A9 – FASCICOLO DEI CALCOLI CARPENTERIE METALLICHE

In conformità al paragrafo 10.1 del D.M. 17.01.2018 e relativa CIRCOLARE applicativa

INTRODUZIONE AI MODELLI DI CALCOLO

Per il calcolo della struttura è stato analizzato un modello di calcolo che considera la struttura nel suo insieme (modello tridimensionale, analisi spaziale).



Si è scelto di riportare nel presente tabulato i dati di input e le verifiche degli elementi strutturali in forma ridotta a causa della grande quantità di dati numerici del modello. I risultati principali sono comunque riportati in forma grafica e meglio comprensibile nella relazione di calcolo allegata.

IMPOSTAZIONE DEL MODELLO E RISULTATI DELL'ANALISI - SIMBOLOGIE ADOTTATE DA MASTERSAP

Diamo una breve descrizione delle simbologie adottate da MasterSap.

I NODI

La struttura è individuata da nodi riportati in coordinate.

Ogni nodo possiede sei gradi di libertà, associati alle sei possibili deformazioni. I gradi di libertà possono essere liberi (spostamenti generalizzati incogniti), bloccati (spostamenti generalizzati corrispondente uguale a zero), di tipo slave o linked (il parametro cinematico dipende dalla relazione con altri gradi di libertà).

Si può intervenire sui gradi di libertà bloccando uno o più gradi. I blocchi vengono applicate nella direzione della terna locale del nodo.

Le relazioni complesse creano un legame tra uno o più gradi di libertà di un nodo detto slave con quelli di un altro nodo detto master. Esistono tre tipi di relazioni complesse.

Le relazioni di tipo link prescrivono l'uguaglianza tra gradi di libertà analoghi di nodi diversi. Specificare una relazione di tipo link significa specificare il nodo slave assieme ai gradi di libertà che partecipano al vincolo ed il nodo master. I gradi di libertà slave saranno eguagliati ai rispettivi gradi di libertà del nodo master.

La relazione di piano rigido prescrive che il nodo slave appartiene ad un piano

rigido e quindi che i due spostamenti in piano e la rotazione normale al piano sono legati ai tre parametri di roto-traslazione rigida di un piano.

Il Corpo rigido prescrive che il nodo slave fa parte di un corpo rigido e tutti e sei i suoi gradi di libertà sono legati ai sei gradi di libertà posseduti dal corpo rigido (i gradi di libertà del suo nodo master).

I MATERIALI

I materiali sono individuati da un codice specifico e descritti dal modulo di elasticità, dal coefficiente di Poisson, dal peso specifico, dal coefficiente di dilatazione termica.

LE SEZIONI

Le sezioni sono individuate in ogni caso da un codice numerico specifico, dal tipo e dai relativi parametri identificativi. La simbologia adottata dal programma è la seguente:

- Rettangolare piena (Rp);
- Rettangolare cava (Rc);
- Circolare piena (Cp);
- Circolare cava (Cc);
- T (T.);
- T rovescia (Tr);
- L (L.);
- C (C.);
- C rovescia (Cr);
- Cassone (Ca);
- Profilo singolo (Ps);
- Profilo doppio (Pd);
- Generica (Ge).

I CARICHI

I carichi agenti sulla struttura possono essere suddivisi in carichi nodali e carichi elementari. I carichi nodali sono forze e coppie concentrate applicate ai nodi della discretizzazione. I carichi elementari sono forze, coppie e sollecitazioni termiche.

I carichi in luce sono individuati da un codice numerico, da un tipo e da una descrizione. Sono previsti carichi distribuiti trapezoidali riferiti agli assi globali (f_X, f_Y, f_Z, f_V) e locali (f_x, f_y, f_z), forze concentrate riferite agli assi globali (F_X, F_Y, F_Z, F_V) o locali (F_x, F_y, F_z), momenti concentrati riferiti agli assi locali (M_x, M_y, M_z), momento torcente distribuito riferito all'asse locale x (m_x), carichi termici (t_x, t_y, t_z), descritti con i relativi parametri identificativi, aliquote inerziali comprese, rispetto al riferimento locale. I carichi in luce possono essere attribuiti solo a elementi finiti del tipo trave o trave di fondazione.

GLI ELEMENTI FINITI

La struttura può essere suddivisa in sottostrutture, chiamate gruppi.

ELEMENTO TRUSS (ASTA RETICOLARE)

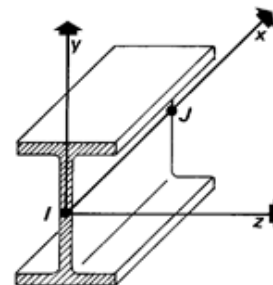
L'elemento truss (asta reticolare) rappresenta il modello meccanico della biella elastica.

Possiede 2 nodi I e J e di conseguenza 12 gradi di libertà.

Gli elementi truss sono caratterizzati da 4 parametri fisici e geometrici ovvero:

1. A Area della sezione.
2. E. Modulo elastico.
3. ρ . Densità di peso (peso per unità di volume).
4. α . Coefficiente termico di dilatazione cubica.

I dati di input e i risultati del calcolo relativi all'elemento stesso sono riferiti alla terna locale di riferimento indicata in figura.



Riferimento locale

ELEMENTO FRAME (TRAVE E PILASTRO, TRAVE DI FONDAZIONE)

L'elemento frame implementa il modello della trave nello spazio tridimensionale. E' caratterizzato da 2 nodi principali I e J posti alle sue estremità ed un nodo geometrico facoltativo K che serve solamente a fissare univocamente la posizione degli assi locali.

L'elemento frame possiede 12 gradi di libertà.

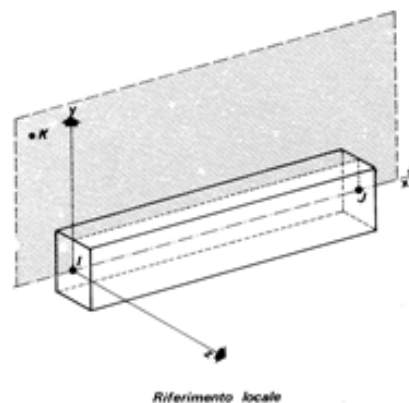
Ogni elemento viene riferito a una terna locale destra x, y, z, come mostrato in figura. L'elemento frame supporta varie opzioni tra cui:

1. deformabilità da taglio (travi tozze);
2. sconnessioni totali o parziali alle estremità;
3. connessioni elastiche alle estremità;
4. offsets, ovvero tratti rigidi eventualmente fuori asse alle estremità;
5. suolo elastico alla Winkler nelle tre direzioni locali e a torsione.

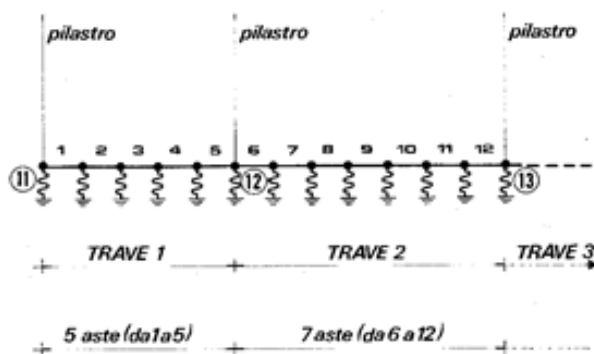
L'elemento frame supporta i seguenti carichi:

1. carichi distribuiti trapezoidali in tutte le direzioni locali o globali;
2. sollecitazioni termiche uniformi e gradienti termici nelle due direzioni principali;
3. forza concentrata in tutte le direzioni locali o globali applicata in un punto arbitrario;
4. carichi generici mediante prescrizione delle reazioni di incastro perfetto.

I gruppi formati da elementi del tipo trave riportano, in ordine, i numeri dei nodi iniziale (I), finale (J) e di riferimento (K), la situazione degli svincoli ai nodi I e J (indicate in legenda eventuali situazioni diverse dall'incastro perfetto ad entrambi i nodi), i codici dei materiali e delle sezioni, la situazione di carico nelle otto possibili condizioni A, B, C, D, E, F, G, H: se è presente un numero, esso individua il coefficiente moltiplicativo del carico corrispondente.



I gruppi relativi all'elemento trave di fondazione riportano informazioni analoghe; le condizioni di carico sono limitate a due (A e B); È indicata la caratteristica del suolo, la larghezza di contatto con il terreno e il numero di suddivisioni interne. Per la trave di fondazione il programma abilita automaticamente solo i gradi di libertà relativi alla rotazione intorno agli assi globali X, Y e alla traslazione secondo Z, bloccando gli altri gradi di libertà. Ogni trave di fondazione è suddivisa in un numero adeguato di parti (aste). Ogni singola asta interagisce con



il terreno mediante un elemento finito del tipo vincolo elastico alla traslazione verticale t_z convergente ai suoi nodi (vedi figura), il cui valore di rigidezza viene determinato da programma moltiplicando la costante di sottofondo assegnata dall'utente per l'area di contatto con il terreno in corrispondenza del nodo.

I tipi di carichi ammessi sono solo di tipo distribuito f_z , f_v , f_y . Inoltre accade che:

$V_i = V_f$; $d_i = d_f = 0$, ovvero il carico è di tipo rettangolare esteso per tutta la lunghezza della trave.

ELEMENTO SHELL (GUSCIO)

L'elemento shell implementa il modello del guscio piatto ortotropo nello spazio tridimensionale. E' caratterizzato da 3 o 4 nodi I, J, K ed L posti nei vertici e 6 gradi di libertà per ogni nodo. Il comportamento flessionale e quello membranale sono disaccoppiati.

Gli elementi guscio/piastra si caratterizzano perché possono subire carichi nel piano ma anche ortogonali al piano ed essere quindi soggetti anche ad azioni flettenti e torcenti.

Gli elementi in esame hanno formalmente tutti i sei gradi di libertà attivi, ma non posseggono rigidità per la rotazione ortogonale al piano dell'elemento. Nei gruppi shell definiti "platea" viene attuato il blocco di tre gradi di libertà, u_X , u_Y , r_Z , per tutti i nodi del gruppo.

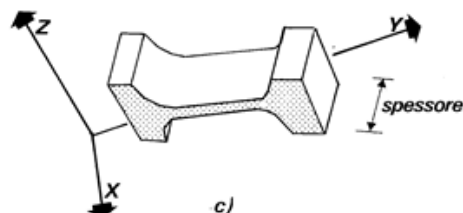
Ogni gruppo può contenere uno o più elementi (max 1999). Ogni elemento viene definito da questi parametri:

1. elemento numero (massimo 1999 per ogni gruppo);
2. nodi di riferimento I, J, K, L;
3. spessore;
4. materiale;
5. pressioni e relative aliquote dinamiche;
6. temperatura;
7. gradiente termico;
8. carichi distribuiti e relative aliquote dinamiche.

ELEMENTO PLANE (STATO PIANO DI TENSIONE, DI DEFORMAZIONE, ASSIALSIMMETRICO)

L'elemento plane implementa i modelli dell'elasticità piana nelle tre classiche varianti degli stati piani di tensione, di deformazione e dei problemi assialsimmetrici, per materiali ortotropi nello spazio bidimensionale. E' caratterizzato da 3 o 4 nodi I, J, K, L posti nei vertici e 2 gradi di libertà per ogni nodo.

Gli elementi in stato piano di tensione, di deformazione o assialsimmetrici sono elementi piani quadrilateri (4 nodi) o triangolari (3 nodi) bidimensionali, caratterizzati da due dimensioni dello stesso ordine di grandezza, prevalenti sulla terza dimensione, che individua lo spessore. Vengono utilizzati per rappresentare strutture bidimensionali caricate nel piano: sono nulle le tensioni ortogonali al piano dell'elemento.



Gli elementi in Stato Piano di Deformazione sono elementi per cui è nulla la deformazione ortogonale al piano, ma non la tensione relativa. Vanno obbligatoriamente analizzati nel piano YZ e si assume uno sviluppo unitario sulla terza dimensione (lungo X). Hanno attivi i due gradi di libertà relativi agli spostamenti nel piano YZ.

Gli elementi Assialsimmetrici rappresentano solidi simmetrici, ottenuti per rotazione intorno all'asse verticale Z e simmetricamente caricati; sono individuati dalla loro sezione nel piano YZ. Anche gli elementi assialsimmetrici vanno studiati nel piano YZ e hanno attivi i gradi di libertà relativi agli spostamenti in questo piano.

Il programma analizza il loro comportamento per uno sviluppo angolare di un radiante.

Ogni gruppo può contenere uno o più elementi (max 1999). Ogni elemento viene definito con questi parametri:

1. numero elemento (massimo 1999 per gruppo);
2. nodi di riferimento I, J, K, L;
3. spessore;
4. materiale;
5. carichi (o pressioni) e relative aliquote dinamiche;
6. temperatura.

ELEMENTO BOUNDARY (VINCOLO)

L'elemento boundary è sostanzialmente un elemento molla con rigidezza assiale in una direzione specificata e rigidezza torsionale attorno alla stessa direzione. E' utile quando si vogliono determinare le reazioni vincolari oppure quando si vogliono imporre degli spostamenti o delle rotazioni di alcuni nodi (cedimenti vincolari).

I parametri relativi ad ogni singolo vincolo sono:

1. il nodo a cui è collegato il vincolo (o i vincoli, massimo sei);
2. la traslazione imposta (L) o la rotazione imposta (radianti);
3. la rigidezza (per le traslazioni in F/L , per le rotazioni in $F*L/rad$).

STAMPA DEI DATI DI PROGETTO

INTESTAZIONE E DATI CARATTERISTICI DELLA STRUTTURA

Nome dell'archivio di lavoro	Struttura R01
Intestazione del lavoro	
Tipo di struttura	Nello Spazio
Tipo di analisi	Statica e Dinamica
Tipo di soluzione	Lineare
Unita' di misura delle forze	kg
Unita' di misura delle lunghezze	m
Normativa	NTC-2018

Normativa

Vita nominale costruzione	50 anni
Classe d'uso costruzione	III
Vita di riferimento	75 anni
Localita'	Arezzo - Localita' San Polo 1
Longitudine (WGS84)	11.8698
Latitudine (WGS84)	43.4826
Categoria del suolo	E
Coefficiente topografico	1
Coefficiente di smorzamento	5%
Eccentricita' accidentale	0%
Numero di frequenze	30
Comportamento strutturale	NON Dissipativo

PARAMETRI SISMICI

	TR	ag/g	FO	TC*	CC	Ss	Pga (ag*S) (m/s ²)
SLO	45	0.0644	2.5100	0.27	1.95	1.60	1.011
SLD	75	0.0786	2.5130	0.28	1.91	1.60	1.234
SLV	712	0.1837	2.4140	0.30	1.86	1.51	2.725
SLE	712	0.1837	2.4140	0.30	1.86	1.51	2.725
SLC	1462	0.2272	2.4360	0.31	1.83	1.39	3.101

Stato limite ultimo

Fattore di comportamento q per sisma orizzontale	qor=1
--	-------

STATO LIMITE DI DANNO

Fattore di comportamento q per sisma orizzontale	qor=1.5
Coeff.moltiplicativo sisma	1.000

Parametri sismici

Angolo del sisma nel piano orizzontale	0
Sisma verticale	Presente
Fattore di comportamento qv per sisma verticale per SLV	1.5
Combinazione dei modi	CQC
Combinazione componenti azioni sismiche	NTC - Eurocodice 8
λ	0.3
μ	0.3

CARICHI PER ELEMENTI TRAVE, TRAVE DI FONDAZIONE E RETICOLARE

Carico distribuito con riferimento globale Z

Descrizione	Cod.	Cond. carico	Tipo Azione/categoria	Val. iniz.	Dist.iniz. nodo I	Val. finale	Dist.fin. nodo I	Aliq.inerz.	Aliq.inerz. SLD
Neve	5	Condizione 4	Variabile: Neve	- 100.000000	0.000	- 100.000000	0.000	0.0000	0.0000

Carico distribuito con riferimento globale X, agente sulla lunghezza reale

Descrizione	Cod.	Cond. carico	Tipo Azione/categoria	Val. iniz.	Dist.iniz. nodo I	Val. finale	Dist.fin. nodo I	Aliq.inerz.	Aliq.inerz. SLD
Vento	4	Condizione 3	Variabile: Vento	- 120.000000	0.000	- 120.000000	0.000	0.0000	0.0000

Carico distribuito con riferimento globale Z, agente sulla lunghezza reale

Descrizione	Cod.	Cond. carico	Tipo Azione/categoria	Val. iniz.	Dist.iniz. nodo I	Val. finale	Dist.fin. nodo I	Aliq.inerz.	Aliq.inerz. SLD
Peso proprio solaio predalles	1	Condizione 1	Permanente: Permanente portato	- 370.000000	0.000	- 370.000000	0.000	1.0000	1.0000
Permanente (binder+tappeto usura+parapetti+tubazioni portate)	2	Condizione 5	Permanente: Permanente portato	- 370.000000	0.000	- 370.000000	0.000	1.0000	1.0000
Variabile folla	3	Condizione 2	Variabile: Aree di acquisto e congresso	- 500.000000	0.000	- 500.000000	0.000	0.0000	0.0000

LISTA MATERIALI UTILIZZATI

Codice	Descrizione	Tipo materiale	Mod. elast.	Coef. Poisson	Peso unit.	Dil. term.	Aliq. inerz.	Rigid. taglio	Rigid. fless.
1	Acciaio	Altro	+2.10e+10	0.300	7849.99951	+1.20e-05	1.000	+1.00e+00	+1.00e+00
2	Acciaio no peso	Altro	+2.10e+10	0.300	0.00000	+1.20e-05	1.000	+1.00e+00	+1.00e+00

RIEPILOGO DELLE SEZIONI UTILIZZATE NEL MODELLO STRUTTURALE

Sezione rettangolare

Codice	Base	H
3	0.060	0.010

Sezione profilo semplice

Codice	Codice sezione	Asse Y capovolto
1	HEB 600	No

Sezione profilo doppio

Codice	Codice sezione	Tipo accoppiamento	Distanza	Ali	Lati
2	UNP 160		0.015	esterne	

GRUPPI DELLA STRUTTURA

Elemento finito: TRAVE

Numero gruppo	Descrizione gruppo		
1	Travi		
2	Controventi di piano		
3	Travi di collegamento trasversali		
4	Travi fittizie		

Elemento finito: VINCOLO

Numero gruppo	Descrizione gruppo		
1	Vincoli esterni		

NODI DEL MODELLO

Nodo	Coord. X	Coord. Y	Coord. Z	Temper.	uX	uY	uZ	rX	rY	rZ
1	0.000	0.000	8.000	0.000	0	0	0	0	0	0
2	3.900	0.000	8.000	0.000	0	0	0	0	0	0
3	3.400	7.350	8.000	0.000	0	0	0	0	0	0
4	3.400	10.350	8.000	0.000	0	0	0	0	0	0
5	3.900	14.700	8.000	0.000	0	0	0	0	0	0
6	0.000	14.700	8.000	0.000	0	0	0	0	0	0
7	0.000	4.900	8.000	0.000	0	0	0	0	0	0
8	0.000	9.800	8.000	0.000	0	0	0	0	0	0
9	3.900	4.900	8.000	0.000	0	0	0	0	0	0
10	3.900	9.800	8.000	0.000	0	0	0	0	0	0
11	3.900	-0.500	8.000	0.000	0	0	0	0	0	0
12	0.000	-0.500	8.000	0.000	0	0	0	0	0	0
13	3.900	15.050	8.000	0.000	0	0	0	0	0	0
14	0.000	15.050	8.000	0.000	0	0	0	0	0	0
15	3.900	7.350	8.000	0.000	0	0	0	0	0	0
16	3.900	10.350	8.000	0.000	0	0	0	0	0	0
17	2.100	7.350	8.000	0.000	0	0	0	0	0	0
18	2.100	10.350	8.000	0.000	0	0	0	0	0	0
19	0.000	10.350	8.000	0.000	0	0	0	0	0	0
20	0.000	7.350	8.000	0.000	0	0	0	0	0	0
21	3.400	-0.500	8.000	0.000	0	0	0	0	0	0
22	0.000	2.500	8.000	0.000	0	0	0	0	0	0
23	2.100	2.500	8.000	0.000	0	0	0	0	0	0
24	3.400	2.500	8.000	0.000	0	0	0	0	0	0
25	3.900	2.500	8.000	0.000	0	0	0	0	0	0
26	2.100	-0.500	8.000	0.000	0	0	0	0	0	0

Legenda: descrizione della simbologia adottata per i gradi di liberta'

Simbolo	Descrizione del Grado di Liberta'
0	libero
1	bloccato
MASTER	Master di una o piu' relazioni

GRUPPI elemento finito TRAVE

Gruppo numero: 1 - Descrizione: Travi

Asta	Nodi			Connessioni				Offset strutturali/Conci rigidi
	I	J	K	Nodo I	Nodo J	Mat.	Sez.	
1	1	22	0	Rigida	Rigida	1	1	
2	7	20	0	Rigida	Rigida	1	1	
3	8	19	0	Rigida	Rigida	1	1	
4	2	25	0	Rigida	Rigida	1	1	
5	9	15	0	Rigida	Rigida	1	1	
6	10	16	0	Rigida	Rigida	1	1	
7	11	2	0	Rigida	Rigida	1	1	
8	12	1	0	Rigida	Rigida	1	1	
9	6	14	0	Rigida	Rigida	1	1	
10	5	13	0	Rigida	Rigida	1	1	
11	15	10	0	Rigida	Rigida	1	1	
12	16	5	0	Rigida	Rigida	1	1	
13	19	6	0	Rigida	Rigida	1	1	
14	20	8	0	Rigida	Rigida	1	1	
15	22	7	0	Rigida	Rigida	1	1	
16	25	9	0	Rigida	Rigida	1	1	

Gruppo numero: 2 - Descrizione: Controventi di piano

Asta	Nodi			Connessioni				Offset strutturali/Conci rigidi
	I	J	K	Nodo I	Nodo J	Mat.	Sez.	
1	1	9	0	(1)	(1)	2	3	
2	9	8	0	(1)	(1)	2	3	
3	8	5	0	(1)	(1)	2	3	
4	6	10	0	(1)	(1)	2	3	
5	10	7	0	(1)	(1)	2	3	
6	7	2	0	(1)	(1)	2	3	

Legenda delle connessioni

Nota	Descrizione
1	Fx=Rigida Fy=Rigida Fz=Rigida Mx=Rigida My=Svinc. Mz=Svinc.

Gruppo numero: 3 - Descrizione: Travi di collegamento trasversali

Asta	Nodi			Connessioni				Offset strutturali/Conci rigidi
	I	J	K	Nodo I	Nodo J	Mat.	Sez.	
1	1	2	0	(1)	(1)	1	2	

Asta	Nodi			Connessioni			Offset strutturali/Conci rigidi
	I	J	K	Nodo I	Nodo J	Mat.	
2	7	9	0	(1)	(1)	1	2
3	8	10	0	(1)	(1)	1	2
4	6	5	0	(1)	(1)	1	2

Legenda delle connessioni

Nota	Descrizione
1	Fx=Rigida Fy=Rigida Fz=Rigida Mx=Rigida My=Rigida Mz=Svinc.

Gruppo numero: 4 - Descrizione: Travi fittizie

Asta	Nodi			Connessioni			Offset strutturali/Conci rigidi
	I	J	K	Nodo I	Nodo J	Mat.	
1	17	3	0	Rigida	Rigida	2	1
2	20	17	0	(1)	Rigida	2	1
3	4	16	0	Rigida	(1)	2	1
4	18	4	0	Rigida	Rigida	2	1
5	19	18	0	(1)	Rigida	2	1
6	3	15	0	Rigida	(1)	2	1
7	21	11	0	Rigida	(1)	2	1
8	22	23	0	(1)	Rigida	2	1
9	23	24	0	Rigida	Rigida	2	1
10	24	25	0	Rigida	(1)	2	1
11	12	26	0	(1)	Rigida	2	1
12	26	21	0	Rigida	Rigida	2	1

Legenda delle connessioni

Nota	Descrizione
1	Fx=Rigida Fy=Rigida Fz=Rigida Mx=Rigida My=Svinc. Mz=Svinc.

GRUPPI ELEMENTO finito VINCOLO

Gruppo numero: 1 - Descrizione: Vincoli esterni

Vincoli standard

Nodo	Rigid. Trasl. X	Rigid. Rotaz. X	Rigid. Trasl. Y	Rigid. Rotaz. Y	Rigid. Trasl. Z	Rigid. Rotaz. Z
1					+1.00e+09	
2	+1.00e+09				+1.00e+09	
5	+1.00e+09		+1.00e+09		+1.00e+09	
6					+1.00e+09	

COMBINAZIONI DI CARICO

Normativa: NORME TECNICHE PER LE COSTRUZIONI 2018 Italia

Combinazioni per le verifiche allo stato limite ultimo

Num.	Descrizione	Parametri	Tipo azione/categoria	Condizione	Moltiplicatore
1	Dinamica	Azione sismica: Presente	Permanente: Peso Proprio	Condizione peso proprio	1.000
			Permanente: Permanente portato	Condizione 1	1.000
			Permanente: Permanente portato	Condizione 5	1.000
			Variable: Aree di acquisto e congresso	Condizione 2	0.000
			Variable: Neve	Condizione 4	0.000
			Variable: Vento	Condizione 3	0.000
2	SLU1 - Statica solo Vento	Azione sismica: Sisma assente	Permanente: Peso Proprio	Condizione peso proprio	1.000
			Permanente: Permanente portato	Condizione 1	1.000
			Permanente: Permanente portato	Condizione 5	1.000
			Variable: Vento	Condizione 3	1.500
3	SLU2 - Statica Neve dom	Azione sismica: Sisma assente	Permanente: Peso Proprio	Condizione peso proprio	1.300
			Permanente: Permanente portato	Condizione 1	1.500
			Permanente: Permanente portato	Condizione 5	1.500
			Variable: Neve	Condizione 4	1.500
			Variable: Vento	Condizione 3	0.900
4	SLU3 - Statica Acc dom	Azione sismica: Sisma assente	Permanente: Peso Proprio	Condizione peso proprio	1.300
			Permanente: Permanente portato	Condizione 1	1.500
			Permanente: Permanente portato	Condizione 5	1.500
			Variable: Aree di acquisto e congresso	Condizione 2	1.500
			Variable: Vento	Condizione 3	0.900
5	SLU4 - Statica Vento dom	Azione sismica: Sisma assente	Permanente: Peso Proprio	Condizione peso proprio	1.300
			Permanente: Permanente portato	Condizione 1	1.500
			Permanente: Permanente portato	Condizione 5	1.500
			Variable: Aree di acquisto e congresso	Condizione 2	0.600
			Variable: Vento	Condizione 3	1.500
7	SLU5 - Statica soccorso PQS.1	Azione sismica: Sisma assente	Permanente: Peso Proprio	Condizione peso proprio	1.300
			Permanente: Permanente portato	Condizione 1	1.500
			Permanente: Permanente portato	Condizione 5	1.500
13	Cond.1 - Solo P.P. Struttura	Azione sismica: Sisma assente	Permanente: Peso Proprio	Condizione peso proprio	1.000
14	Cond.2 - Solo P.P. Solai Predalles - G1	Azione sismica: Sisma assente	Permanente: Permanente portato	Condizione 1	1.000
15	Cond.3 - Solo Portati - G2	Azione sismica: Sisma assente	Permanente: Permanente portato	Condizione 5	1.000
16	Cond.4 - Solo Variable Neve	Azione sismica: Sisma assente	Variable: Neve	Condizione 4	1.000
17	Cond.5 - Solo Variable Vento	Azione sismica: Sisma assente	Variable: Vento	Condizione 3	1.000
18	Cond.6 - Solo Variable Folla	Azione sismica: Sisma assente	Variable: Aree di acquisto e congresso	Condizione 2	1.000
19	Cond.7 - Solo Variable Soccorso PQS.1	Azione sismica: Sisma assente			
20	SLU 6 - Soccorso Pos.2	Azione sismica: Sisma assente	Permanente: Peso Proprio	Condizione peso proprio	1.300
			Permanente: Permanente portato	Condizione 1	1.500
			Permanente: Permanente portato	Condizione 5	1.500
22	Cond.8 - Solo Variable Soccorso PQS.2	Azione sismica: Sisma assente			

Combinazioni per le verifiche allo stato limite d'esercizio

Num.	Descrizione	Parametri	Tipo azione/categoria	Condizione	Moltiplicatore
8	SLE1 - Rara Vento dom	Tipologia: Rara	Permanente: Peso Proprio	Condizione peso proprio	1.000
			Permanente: Permanente portato	Condizione 1	1.000
			Permanente: Permanente portato	Condizione 5	1.000
			Variable: Aree di acquisto e congresso	Condizione 2	0.400
			Variable: Vento	Condizione 3	1.000
9	SLE2 - Rara Solo Vento	Tipologia: Rara	Permanente: Peso Proprio	Condizione peso proprio	1.000
			Permanente: Permanente portato	Condizione 1	1.000
			Permanente: Permanente portato	Condizione 5	1.000
			Variable: Vento	Condizione 3	1.000
10	SLE3 - Rara Acc dom	Tipologia: Rara	Permanente: Peso Proprio	Condizione peso proprio	1.000
			Permanente: Permanente portato	Condizione 1	1.000
			Permanente: Permanente portato	Condizione 5	1.000
			Variable: Aree di acquisto e congresso	Condizione 2	1.000
			Variable: Vento	Condizione 3	0.600
11	SLE4 - Neve dom	Tipologia: Rara	Permanente: Peso Proprio	Condizione peso proprio	1.000
			Permanente: Permanente portato	Condizione 1	1.000
			Permanente: Permanente portato	Condizione 5	1.000
			Variable: Neve	Condizione 4	1.000
			Variable: Vento	Condizione 3	0.600
12	SLE 5 - Soccorso POS.1	Tipologia: Rara	Permanente: Peso Proprio	Condizione peso proprio	1.000
			Permanente: Permanente portato	Condizione 1	1.000
			Permanente: Permanente portato	Condizione 5	1.000
21	SLE 6 - Soccorso POS.2	Tipologia: Rara	Permanente: Peso Proprio	Condizione peso proprio	1.000
			Permanente: Permanente portato	Condizione 1	1.000
			Permanente: Permanente portato	Condizione 5	1.000

Combinazioni per le verifiche allo stato limite di danno

Num.	Descrizione	Parametri	Tipo azione/categoria	Condizione	Moltiplicatore
6	S.L.D.	Azione sismica: Presente	Permanente: Peso Proprio	Condizione peso proprio	1.000
			Permanente: Permanente portato	Condizione 1	1.000
			Variable: Aree di acquisto e congresso	Condizione 2	0.000
			Variable: Neve	Condizione 4	0.000
			Variable: Vento	Condizione 3	0.000

Normativa: NORME TECNICHE PER LE COSTRUZIONI 2018 Italia

CARICHI NODALI

Num. comb. car.	Descrizione							
1	Dinamica							
2	SLU1 - Statica solo Vento							
3	SLU2 - Statica Neve dom							
4	SLU3 - Statica Acc dom							
5	SLU4 - Statica Vento dom							
6	S.L.D.							
7	SLU5 - Statica soccorso POS.1	Nodo	FX	FY	FZ	MX	MY	MZ
		3		+3.60e+03	-6.00e+03			
		4		+1.80e+03	-3.00e+03			
		18		+1.80e+03	-3.00e+03			
		17		+3.60e+03	-6.00e+03			
8	SLE1 - Rara Vento dom							
9	SLE2 - Rara Solo Vento							
10	SLE3 - Rara Acc dom							
11	SLE4 - Neve dom							
12	SLE 5 - Soccorso POS.1	Nodo	FX	FY	FZ	MX	MY	MZ
		3		+2.40e+03	-4.00e+03			
		4		+1.20e+03	-2.00e+03			
		18		+1.20e+03	-2.00e+03			
		17		+2.40e+03	-4.00e+03			
13	Cond.1 - Solo P.P. Struttura							
14	Cond.2 - Solo P.P. Solaio Predalles - G1							
15	Cond.3 - Solo Portati - G2							
16	Cond.4 - Solo Variabile Neve							
17	Cond.5 - Solo Variabile Vento							
18	Cond.6 - Solo Variabile Folla							
19	Cond.7 - Solo Variabile Soccorso POS.1	Nodo	FX	FY	FZ	MX	MY	MZ
		3		-2.40e+03	-4.00e+03			
		4		-1.20e+03	-2.00e+03			
		18		-1.20e+03	-2.00e+03			
		17		-2.40e+03	-4.00e+03			
20	SLU 6 - Soccorso Pos.2	Nodo	FX	FY	FZ	MX	MY	MZ
		23		+1.80e+03	-3.00e+03			
		26		+3.60e+03	-6.00e+03			
		24		+1.80e+03	-3.00e+03			
		21		+3.60e+03	-6.00e+03			
21	SLE 6 - Soccorso POS:2	Nodo	FX	FY	FZ	MX	MY	MZ
		23		+1.20e+03	-2.00e+03			

Num. comb. car.	Descrizione							
		26		+2.40e+03	-4.00e+03			
		24		+1.20e+03	-2.00e+03			
		21		+2.40e+03	-4.00e+03			
22	Cond.8 - Solo Variabile Soccorso POS.2	Nodo	FX	FY	FZ	MX	MY	MZ
		23		-1.20e+03	-2.00e+03			
		26		-2.40e+03	-4.00e+03			
		24		-1.20e+03	-2.00e+03			
		21		-2.40e+03	-4.00e+03			

REAZIONI VINCOLARI STATICA

FORZE MOMENTI PER GRUPPI VINCOLO

Gruppo numero: 1 - Descrizione: Vincoli esterni

Nodo	c.c.	FX	FY	FZ	MX	MY	MZ
1	1	-0.000e+00	-0.000e+00	+1.314e+04	-0.000e+00	-0.000e+00	-0.000e+00
1	2	-0.000e+00	-0.000e+00	+1.314e+04	-0.000e+00	-0.000e+00	-0.000e+00
1	3	-0.000e+00	-0.000e+00	+2.165e+04	-0.000e+00	-0.000e+00	-0.000e+00
1	4	-0.000e+00	-0.000e+00	+3.084e+04	-0.000e+00	-0.000e+00	-0.000e+00
1	5	-0.000e+00	-0.000e+00	+2.395e+04	-0.000e+00	-0.000e+00	-0.000e+00
1	7	-0.000e+00	-0.000e+00	+2.165e+04	-0.000e+00	-0.000e+00	-0.000e+00
1	8	-0.000e+00	-0.000e+00	+1.621e+04	-0.000e+00	-0.000e+00	-0.000e+00
1	9	-0.000e+00	-0.000e+00	+1.314e+04	-0.000e+00	-0.000e+00	-0.000e+00
1	10	-0.000e+00	-0.000e+00	+2.080e+04	-0.000e+00	-0.000e+00	-0.000e+00
1	11	-0.000e+00	-0.000e+00	+1.468e+04	-0.000e+00	-0.000e+00	-0.000e+00
1	12	-0.000e+00	-0.000e+00	+1.467e+04	-0.000e+00	-0.000e+00	-0.000e+00
1	13	-0.000e+00	-0.000e+00	+1.812e+03	-0.000e+00	-0.000e+00	-0.000e+00
1	14	-0.000e+00	-0.000e+00	+5.667e+03	-0.000e+00	-0.000e+00	-0.000e+00
1	15	-0.000e+00	-0.000e+00	+5.667e+03	-0.000e+00	-0.000e+00	-0.000e+00
1	16	-0.000e+00	-0.000e+00	+1.532e+03	-0.000e+00	-0.000e+00	-0.000e+00
1	17	-0.000e+00	-0.000e+00	+8.020e-05	-0.000e+00	-0.000e+00	-0.000e+00
1	18	-0.000e+00	-0.000e+00	+7.658e+03	-0.000e+00	-0.000e+00	-0.000e+00
1	19	-0.000e+00	-0.000e+00	+1.526e+03	-0.000e+00	-0.000e+00	-0.000e+00
1	20	-0.000e+00	-0.000e+00	+2.448e+04	-0.000e+00	-0.000e+00	-0.000e+00
1	21	-0.000e+00	-0.000e+00	+1.656e+04	-0.000e+00	-0.000e+00	-0.000e+00
1	22	-0.000e+00	-0.000e+00	+3.418e+03	-0.000e+00	-0.000e+00	-0.000e+00
2	1	-5.012e-05	-0.000e+00	+1.314e+04	-0.000e+00	-0.000e+00	-0.000e+00
2	2	-3.110e+03	-0.000e+00	+1.314e+04	-0.000e+00	-0.000e+00	-0.000e+00
2	3	-1.866e+03	-0.000e+00	+2.165e+04	-0.000e+00	-0.000e+00	-0.000e+00
2	4	-1.866e+03	-0.000e+00	+3.084e+04	-0.000e+00	-0.000e+00	-0.000e+00
2	5	-3.110e+03	-0.000e+00	+2.395e+04	-0.000e+00	-0.000e+00	-0.000e+00
2	7	+8.449e+02	-0.000e+00	+2.484e+04	-0.000e+00	-0.000e+00	-0.000e+00
2	8	-2.074e+03	-0.000e+00	+1.621e+04	-0.000e+00	-0.000e+00	-0.000e+00
2	9	-2.074e+03	-0.000e+00	+1.314e+04	-0.000e+00	-0.000e+00	-0.000e+00
2	10	-1.244e+03	-0.000e+00	+2.080e+04	-0.000e+00	-0.000e+00	-0.000e+00
2	11	-1.244e+03	-0.000e+00	+1.468e+04	-0.000e+00	-0.000e+00	-0.000e+00
2	12	+5.633e+02	-0.000e+00	+1.680e+04	-0.000e+00	-0.000e+00	-0.000e+00
2	13	-5.919e-06	-0.000e+00	+1.812e+03	-0.000e+00	-0.000e+00	-0.000e+00
2	14	-2.210e-05	-0.000e+00	+5.667e+03	-0.000e+00	-0.000e+00	-0.000e+00
2	15	-2.210e-05	-0.000e+00	+5.667e+03	-0.000e+00	-0.000e+00	-0.000e+00
2	16	-5.973e-06	-0.000e+00	+1.532e+03	-0.000e+00	-0.000e+00	-0.000e+00
2	17	-2.074e+03	-0.000e+00	-8.020e-05	-0.000e+00	-0.000e+00	-0.000e+00
2	18	-2.987e-05	-0.000e+00	+7.658e+03	-0.000e+00	-0.000e+00	-0.000e+00
2	19	-5.633e+02	-0.000e+00	+3.657e+03	-0.000e+00	-0.000e+00	-0.000e+00
2	20	+8.449e+02	-0.000e+00	+3.162e+04	-0.000e+00	-0.000e+00	-0.000e+00
2	21	+5.633e+02	-0.000e+00	+2.132e+04	-0.000e+00	-0.000e+00	-0.000e+00
2	22	-5.633e+02	-0.000e+00	+8.174e+03	-0.000e+00	-0.000e+00	-0.000e+00
5	1	-5.024e-05	-4.320e-06	+1.288e+04	-0.000e+00	-0.000e+00	-0.000e+00
5	2	-3.048e+03	-4.320e-06	+1.288e+04	-0.000e+00	-0.000e+00	-0.000e+00
5	3	-1.828e+03	-5.616e-06	+2.122e+04	-0.000e+00	-0.000e+00	-0.000e+00
5	4	-1.828e+03	-5.616e-06	+3.022e+04	-0.000e+00	-0.000e+00	-0.000e+00
5	5	-3.048e+03	-5.616e-06	+2.347e+04	-0.000e+00	-0.000e+00	-0.000e+00
5	7	-8.449e+02	-1.080e+04	+2.618e+04	-0.000e+00	-0.000e+00	-0.000e+00
5	8	-2.032e+03	-4.320e-06	+1.588e+04	-0.000e+00	-0.000e+00	-0.000e+00
5	9	-2.032e+03	-4.320e-06	+1.288e+04	-0.000e+00	-0.000e+00	-0.000e+00
5	10	-1.219e+03	-4.320e-06	+2.039e+04	-0.000e+00	-0.000e+00	-0.000e+00
5	11	-1.219e+03	-4.320e-06	+1.438e+04	-0.000e+00	-0.000e+00	-0.000e+00
5	12	-5.633e+02	-7.200e+03	+1.769e+04	-0.000e+00	-0.000e+00	-0.000e+00

Nodo	c.c.	FX	FY	FZ	MX	MY	MZ
5	13	-6.934e-06	-4.320e-06	+1.778e+03	-0.000e+00	-0.000e+00	-0.000e+00
5	14	-2.165e-05	-3.341e-20	+5.552e+03	-0.000e+00	-0.000e+00	-0.000e+00
5	15	-2.165e-05	-3.341e-20	+5.552e+03	-0.000e+00	-0.000e+00	-0.000e+00
5	16	-5.853e-06	-8.733e-21	+1.501e+03	-0.000e+00	-0.000e+00	-0.000e+00
5	17	-2.032e+03	+1.589e-12	-4.022e-05	-0.000e+00	-0.000e+00	-0.000e+00
5	18	-2.926e-05	-4.894e-20	+7.503e+03	-0.000e+00	-0.000e+00	-0.000e+00
5	19	+5.633e+02	+7.200e+03	+4.804e+03	-0.000e+00	-0.000e+00	-0.000e+00
5	20	-8.449e+02	-1.080e+04	+1.940e+04	-0.000e+00	-0.000e+00	-0.000e+00
5	21	-5.633e+02	-7.200e+03	+1.317e+04	-0.000e+00	-0.000e+00	-0.000e+00
5	22	+5.633e+02	+7.200e+03	+2.876e+02	-0.000e+00	-0.000e+00	-0.000e+00
6	1	-0.000e+00	-0.000e+00	+1.288e+04	-0.000e+00	-0.000e+00	-0.000e+00
6	2	-0.000e+00	-0.000e+00	+1.288e+04	-0.000e+00	-0.000e+00	-0.000e+00
6	3	-0.000e+00	-0.000e+00	+2.122e+04	-0.000e+00	-0.000e+00	-0.000e+00
6	4	-0.000e+00	-0.000e+00	+3.022e+04	-0.000e+00	-0.000e+00	-0.000e+00
6	5	-0.000e+00	-0.000e+00	+2.347e+04	-0.000e+00	-0.000e+00	-0.000e+00
6	7	-0.000e+00	-0.000e+00	+2.199e+04	-0.000e+00	-0.000e+00	-0.000e+00
6	8	-0.000e+00	-0.000e+00	+1.588e+04	-0.000e+00	-0.000e+00	-0.000e+00
6	9	-0.000e+00	-0.000e+00	+1.288e+04	-0.000e+00	-0.000e+00	-0.000e+00
6	10	-0.000e+00	-0.000e+00	+2.039e+04	-0.000e+00	-0.000e+00	-0.000e+00
6	11	-0.000e+00	-0.000e+00	+1.438e+04	-0.000e+00	-0.000e+00	-0.000e+00
6	12	-0.000e+00	-0.000e+00	+1.490e+04	-0.000e+00	-0.000e+00	-0.000e+00
6	13	-0.000e+00	-0.000e+00	+1.778e+03	-0.000e+00	-0.000e+00	-0.000e+00
6	14	-0.000e+00	-0.000e+00	+5.552e+03	-0.000e+00	-0.000e+00	-0.000e+00
6	15	-0.000e+00	-0.000e+00	+5.552e+03	-0.000e+00	-0.000e+00	-0.000e+00
6	16	-0.000e+00	-0.000e+00	+1.501e+03	-0.000e+00	-0.000e+00	-0.000e+00
6	17	-0.000e+00	-0.000e+00	+4.022e-05	-0.000e+00	-0.000e+00	-0.000e+00
6	18	-0.000e+00	-0.000e+00	+7.503e+03	-0.000e+00	-0.000e+00	-0.000e+00
6	19	-0.000e+00	-0.000e+00	+2.012e+03	-0.000e+00	-0.000e+00	-0.000e+00
6	20	-0.000e+00	-0.000e+00	+1.915e+04	-0.000e+00	-0.000e+00	-0.000e+00
6	21	-0.000e+00	-0.000e+00	+1.300e+04	-0.000e+00	-0.000e+00	-0.000e+00
6	22	-0.000e+00	-0.000e+00	+1.206e+02	-0.000e+00	-0.000e+00	-0.000e+00

TABELLA INVILUPPI REAZIONI VINCOLARI

FORZE / MOMENTI ELEMENTO FINITO PLINTO - VINCOLO (EX +λ*EY+μ*EZ)

Gruppo: 1 - Descrizione: Vincoli esterni

Nodo	FX	FY	FZ	MX	MY	MZ
1	+0.00e+00	+0.00e+00	+2.33e+02	+0.00e+00	+0.00e+00	+0.00e+00
2	+1.38e+04	+0.00e+00	+2.33e+02	+0.00e+00	+0.00e+00	+0.00e+00
5	+1.29e+04	+5.74e+03	+2.18e+02	+0.00e+00	+0.00e+00	+0.00e+00
6	+0.00e+00	+0.00e+00	+2.18e+02	+0.00e+00	+0.00e+00	+0.00e+00

FORZE / MOMENTI ELEMENTO FINITO PLINTO - VINCOLO (λ*EX+EY+μ*EZ)

Gruppo: 1 - Descrizione: Vincoli esterni

Nodo	FX	FY	FZ	MX	MY	MZ
1	+0.00e+00	+0.00e+00	+2.33e+02	+0.00e+00	+0.00e+00	+0.00e+00
2	+7.68e+03	+0.00e+00	+2.33e+02	+0.00e+00	+0.00e+00	+0.00e+00
5	+7.67e+03	+1.73e+04	+2.18e+02	+0.00e+00	+0.00e+00	+0.00e+00
6	+0.00e+00	+0.00e+00	+2.18e+02	+0.00e+00	+0.00e+00	+0.00e+00

FORZE / MOMENTI ELEMENTO FINITO PLINTO - VINCOLO (λ*EX+λ*EY+EZ)

Gruppo: 1 - Descrizione: Vincoli esterni

Nodo	FX	FY	FZ	MX	MY	MZ
1	+0.00e+00	+0.00e+00	+7.75e+02	+0.00e+00	+0.00e+00	+0.00e+00
2	+4.95e+03	+0.00e+00	+7.75e+02	+0.00e+00	+0.00e+00	+0.00e+00
5	+4.76e+03	+5.31e+03	+7.27e+02	+0.00e+00	+0.00e+00	+0.00e+00
6	+0.00e+00	+0.00e+00	+7.27e+02	+0.00e+00	+0.00e+00	+0.00e+00

TABELLA MASSE ECCITATE

PROSPETTO RIASSUNTIVO MODI PRINCIPALI

Periodo principale	T1	Massa	Massa %	Modo	Note
Direzione X	+2.14e-01	+3.66e+03	68	3	--
Direzione Y	+1.24e-01	+3.00e+03	56	4	--
Direzione Z	+3.08e-01	+3.64e+03	68	1	--

Periodo	T2	Massa	Massa %	Modo	Note
Direzione X	+2.60e-02	+4.35e+02	8	13	--
Direzione Y	+3.34e-02	+1.78e+03	34	12	--
Direzione Z	+3.37e-02	+1.13e+02	2	10	--

PROSPETTO RIASSUNTIVO MASSE ECCITATE PER QUOTA MAGGIORE DI: 0.00

Analisi	Direz.X	%	Direz.Y	%	Direz.Z	%
--	+4.71e+03	89	+4.97e+03	94	+3.78e+03	71

FREQUENZE PROPRIE DI OSCILLAZIONE

Numero	Pulsazione	Frequenza	Periodo	Precisione
1	2.038e+01	3.244e+00	3.083e-01	4.441e-16
2	2.043e+01	3.252e+00	3.075e-01	4.441e-16
3	2.942e+01	4.683e+00	2.136e-01	4.441e-16
4	5.063e+01	8.058e+00	1.241e-01	4.441e-16
5	5.128e+01	8.162e+00	1.225e-01	4.441e-16
6	6.675e+01	1.062e+01	9.414e-02	4.441e-16
7	8.044e+01	1.280e+01	7.812e-02	4.441e-16
8	8.049e+01	1.281e+01	7.807e-02	4.441e-16
9	1.220e+02	1.941e+01	5.152e-02	4.441e-16
10	1.865e+02	2.968e+01	3.370e-02	4.441e-16
11	1.865e+02	2.968e+01	3.369e-02	4.441e-16
12	1.881e+02	2.994e+01	3.339e-02	4.441e-16
13	2.420e+02	3.852e+01	2.596e-02	4.441e-16
14	3.145e+02	5.005e+01	1.998e-02	4.441e-16
15	3.145e+02	5.005e+01	1.998e-02	4.441e-16
16	3.304e+02	5.258e+01	1.902e-02	4.441e-16
17	3.653e+02	5.814e+01	1.720e-02	4.441e-16
18	3.680e+02	5.857e+01	1.707e-02	4.441e-16
19	3.715e+02	5.912e+01	1.691e-02	4.441e-16
20	5.288e+02	8.417e+01	1.188e-02	4.441e-16
21	5.304e+02	8.442e+01	1.185e-02	4.441e-16
22	5.961e+02	9.487e+01	1.054e-02	4.441e-16
23	6.639e+02	1.057e+02	9.464e-03	4.441e-16
24	7.583e+02	1.207e+02	8.286e-03	4.441e-16
25	7.790e+02	1.240e+02	8.066e-03	4.441e-16
26	7.790e+02	1.240e+02	8.065e-03	4.441e-16
27	8.039e+02	1.279e+02	7.816e-03	4.441e-16
28	8.418e+02	1.340e+02	7.464e-03	4.441e-16
29	8.443e+02	1.344e+02	7.442e-03	4.441e-16
30	8.780e+02	1.397e+02	7.156e-03	4.441e-16

COEFFICIENTI DI PARTECIPAZIONE MODALE

Modo	Direz.X	Direz.Y	Direz.Z
1	-9.820e-08	2.458e-09	-6.034e+01
2	-6.708e-06	-2.382e-06	7.857e-10
3	-6.051e+01	1.343e+00	9.811e-08
4	1.404e+00	5.479e+01	1.414e-09
5	-9.684e+00	2.397e+00	-2.330e-08

Modo	Direz.X	Direz.Y	Direz.Z
6	8.306e+00	-7.049e-01	2.538e-09
7	-1.935e-09	-2.047e-09	4.923e+00
8	9.318e-08	1.621e-07	-2.417e-11
9	3.969e-01	-3.251e-01	-8.091e-09
10	-2.265e-08	1.151e-08	1.063e+01
11	8.368e-08	7.077e-07	3.930e-11
12	7.954e-01	4.222e+01	-2.791e-09
13	-2.086e+01	-3.766e-01	-1.547e-10
14	4.270e-08	-2.863e-09	-2.674e+00
15	-1.982e-08	-1.024e-08	3.372e-12
16	1.935e+01	-3.653e-01	1.686e-08
17	-1.888e+00	-3.178e-01	5.778e-09
18	-2.295e+00	-3.467e-01	2.875e-09
19	1.716e+00	-3.883e-01	-2.700e-09
20	-1.567e-01	1.254e+01	-2.945e-10
21	4.918e-01	1.483e+00	1.403e-09
22	-1.945e+00	-8.762e-02	-2.285e-08
23	1.894e-02	-1.047e-01	3.103e-11
24	-7.203e+00	9.516e-03	-2.703e-08
25	6.102e-08	-1.915e-10	1.961e-01
26	-2.618e-07	1.887e-09	-3.304e-13
27	-1.119e+00	1.830e-02	-6.629e-09
28	4.015e-01	-3.503e-03	1.645e-09
29	-7.256e-02	1.121e-03	-2.909e-10
30	4.651e-02	4.642e+00	-5.306e-11

MASSA ECCITATA
per quota Z maggiore di :0.00

Modo	Direz.X	%	Direz.Y	%	Direz.Z	%
Modo: 1	+9.64e-15	0	+6.04e-18	0	+3.64e+03	69
Progressiva	+9.64e-15	0	+6.04e-18	0	+3.64e+03	69
Modo: 2	+4.50e-11	0	+5.67e-12	0	+6.17e-19	0
Progressiva	+4.50e-11	0	+5.67e-12	0	+3.64e+03	69
Modo: 3	+3.66e+03	69	+1.80e+00	0	+9.63e-15	0
Progressiva	+3.66e+03	69	+1.80e+00	0	+3.64e+03	69
Modo: 4	+1.97e+00	0	+3.00e+03	57	+2.00e-18	0
Progressiva	+3.66e+03	69	+3.00e+03	57	+3.64e+03	69
Modo: 5	+9.38e+01	2	+5.75e+00	0	+5.43e-16	0
Progressiva	+3.76e+03	71	+3.01e+03	57	+3.64e+03	69
Modo: 6	+6.90e+01	1	+4.97e-01	0	+6.44e-18	0
Progressiva	+3.83e+03	72	+3.01e+03	57	+3.64e+03	69
Modo: 7	+3.75e-18	0	+4.19e-18	0	+2.42e+01	0
Progressiva	+3.83e+03	72	+3.01e+03	57	+3.66e+03	69
Modo: 8	+8.68e-15	0	+2.63e-14	0	+5.84e-22	0
Progressiva	+3.83e+03	72	+3.01e+03	57	+3.66e+03	69
Modo: 9	+1.57e-01	0	+1.06e-01	0	+6.55e-17	0
Progressiva	+3.83e+03	72	+3.01e+03	57	+3.66e+03	69
Modo: 10	+5.13e-16	0	+1.33e-16	0	+1.13e+02	2
Progressiva	+3.83e+03	72	+3.01e+03	57	+3.78e+03	71
Modo: 11	+7.00e-15	0	+5.01e-13	0	+1.54e-21	0
Progressiva	+3.83e+03	72	+3.01e+03	57	+3.78e+03	71
Modo: 12	+6.33e-01	0	+1.78e+03	34	+7.79e-18	0
Progressiva	+3.83e+03	72	+4.79e+03	90	+3.78e+03	71
Modo: 13	+4.35e+02	8	+1.42e-01	0	+2.39e-20	0
Progressiva	+4.26e+03	80	+4.79e+03	90	+3.78e+03	71
Modo: 14	+1.82e-15	0	+8.20e-18	0	+7.15e+00	0
Progressiva	+4.26e+03	80	+4.79e+03	90	+3.78e+03	71

Modo	Direz.X	%	Direz.Y	%	Direz.Z	%
Modo: 15	+3.93e-16	0	+1.05e-16	0	+1.14e-23	0
Progressiva	+4.26e+03	80	+4.79e+03	90	+3.78e+03	71
Modo: 16	+3.74e+02	7	+1.33e-01	0	+2.84e-16	0
Progressiva	+4.64e+03	87	+4.79e+03	90	+3.78e+03	71
Modo: 17	+3.56e+00	0	+1.01e-01	0	+3.34e-17	0
Progressiva	+4.64e+03	87	+4.79e+03	90	+3.78e+03	71
Modo: 18	+5.27e+00	0	+1.20e-01	0	+8.26e-18	0
Progressiva	+4.65e+03	88	+4.79e+03	90	+3.78e+03	71
Modo: 19	+2.95e+00	0	+1.51e-01	0	+7.29e-18	0
Progressiva	+4.65e+03	88	+4.79e+03	90	+3.78e+03	71
Modo: 20	+2.46e-02	0	+1.57e+02	3	+8.67e-20	0
Progressiva	+4.65e+03	88	+4.95e+03	93	+3.78e+03	71
Modo: 21	+2.42e-01	0	+2.20e+00	0	+1.97e-18	0
Progressiva	+4.65e+03	88	+4.95e+03	93	+3.78e+03	71
Modo: 22	+3.78e+00	0	+7.68e-03	0	+5.22e-16	0
Progressiva	+4.65e+03	88	+4.95e+03	93	+3.78e+03	71
Modo: 23	+3.59e-04	0	+1.10e-02	0	+9.63e-22	0
Progressiva	+4.65e+03	88	+4.95e+03	93	+3.78e+03	71
Modo: 24	+5.19e+01	1	+9.05e-05	0	+7.30e-16	0
Progressiva	+4.70e+03	89	+4.95e+03	93	+3.78e+03	71
Modo: 25	+3.72e-15	0	+3.67e-20	0	+3.85e-02	0
Progressiva	+4.70e+03	89	+4.95e+03	93	+3.78e+03	71
Modo: 26	+6.86e-14	0	+3.56e-18	0	+1.10e-25	0
Progressiva	+4.70e+03	89	+4.95e+03	93	+3.78e+03	71
Modo: 27	+1.25e+00	0	+3.35e-04	0	+4.39e-17	0
Progressiva	+4.71e+03	89	+4.95e+03	93	+3.78e+03	71
Modo: 28	+1.61e-01	0	+1.23e-05	0	+2.71e-18	0
Progressiva	+4.71e+03	89	+4.95e+03	93	+3.78e+03	71
Modo: 29	+5.26e-03	0	+1.26e-06	0	+8.46e-20	0
Progressiva	+4.71e+03	89	+4.95e+03	93	+3.78e+03	71
Modo: 30	+2.16e-03	0	+2.16e+01	0	+2.81e-21	0
Progressiva	+4.71e+03	89	+4.97e+03	94	+3.78e+03	71

MASSA TOTALE ECCITABILE

Direzione X
+5.31e+03

Direzione Y
+5.31e+03

Direzione Z
+5.31e+03

VERIFICHE DEGLI ELEMENTI STRUTTURALI

INTERPRETAZIONE DEI RISULTATI DELLE VERIFICHE

Si riportano le descrizioni delle simbologie adottate per le verifiche.

VERIFICHE DI OPERE IN ACCIAIO, ALLUMINIO O LEGNO CON IL METODO DELLE TENSIONI AMMISSIBILI E DEGLI STATI LIMITE

I RISULTATI PER ASTE RETICOLARI

Viene eseguita la verifica per aste soggette unicamente a sforzo normale. Per tutte le combinazioni di carico, viene effettuata la verifica di resistenza per aste e di stabilità per aste compresse. Per aste compresse viene utilizzato il metodo "ω".

Viene riportata una descrizione dei parametri di progetto e successivamente, in sequenza per ogni asta:

- numero combinazione di carico;
- sforzo normale N (corrispondente a F_x), positivo se di trazione;
- sezione utile (cm^2); rappresenta il valore A_x , eventualmente diminuito per effetto del coefficiente di riduzione dell'area;
- snellezza; è la snellezza più elevata dell'asta fra le due corrispondenti ai piani di flessione e quella ulteriore, eventuale, derivante da assi principali di inerzia della sezione non coincidenti con gli assi locali y e z (come avviene per la sezione a L); nelle note è indicato il piano di massima snellezza cui si riferisce il valore riportato;
- S_f , tensione nell'acciaio o nell'alluminio (in kg/cm^2 , N/mm^2 o daN/cm^2); nel caso del legno la voce diventa esplicitamente tensione, anziché S_f .

A fine riga compaiono due note; la prima indica il piano di massima snellezza; la seconda, eventuale, è riservata a informazioni di commento.

Nel caso dei profili a freddo la stampa dei risultati riporta anche il valore di Q che concorre a determinare il coefficiente "ω" e la tensione massima che non può essere superata.

I RISULTATI PER TRAVI E PILASTRI

Le sollecitazioni sono riferite al sistema locale x, y, z :

- numero combinazione di carico;
- ascissa di calcolo (cm);

- in sequenza F_x, F_y, F_z (F), M_x, M_y, M_z ($F \cdot m$).

Le convenzioni sui segni delle sollecitazioni sono:

- F_x (sforzo normale) è positivo se di trazione;
- F_y (forza tagliante) è positiva se agisce, a sinistra della sezione interessata, nel verso positivo dell'asse locale corrispondente;
- F_z (forza tagliante) è positiva se agisce, a sinistra della sezione interessata, nel verso negativo dell'asse locale corrispondente;
- M_x (momento torcente) è positivo se antiorario intorno a x a sinistra dell'ascissa in esame;
- M_y (momento flettente) è positivo se tende le fibre posteriori, cioè quelle disposte nel verso negativo dell'asse z;
- M_z (momento flettente) è positivo se tende le fibre inferiori, cioè quelle disposte nel verso negativo dell'asse y.

Il tabulato di uscita riporta inoltre in ordine:

- $S_f(F_x)$, (Tens.(F_x) per il legno): tensione derivante solo da sforzo normale;
- $S_f(M)$, (Tens.(M) per il legno): tensione derivante solo dagli effetti flettenti di M_y e M_z ; viene riportato il valore massimo riscontrato fra tutti i punti soggetti a indagine;
- tensione da torsione, derivante da M_x , valore massimo riscontrato;
- tensione di taglio, derivante da F_y e F_z , valore massimo riscontrato;
- S_f ideale: tensione ideale massima nel caso di acciaio e alluminio. Nel caso del legno, invece, viene riportata una "tensione (F_x, M)" derivante dall'interazione fra F_x e M , in cui si somma il contributo tensionale dovuto allo sforzo normale con quello derivante dal momento flettente, la cui entità viene però riparametrizzata tramite il rapporto fra le tensioni ammissibili a sforzo normale e momento flettente. In questo modo $tens(F_x, M)$ viene confrontata, per la sua accettabilità, con la tensione massima ammessa a sforzo normale;
- locazione, ovvero il punto della sezione in cui si verifica il massimo della tensione ideale;
- Nota: compare un avviso qualora la tensione ideale o "tens (F_x, M)" superi il valore massimo ammissibile, che dipende anche dal relativo coefficiente di incremento connesso alle combinazioni di carico.

Alla fine del tabulato delle verifiche di resistenza, se attivata l'opzione sulla combinazione dei carichi, la procedura propone uno specchietto che riepiloga nell'ordine:

- numero della combinazione di carico che dà luogo al momento massimo: tale sollecitazione si può infatti verificare per effetto di una combinazione di carico spaziale di MasterSap (in questo caso viene riportato il relativo numero o simbolo identificativo) o a causa della combinazione dei carichi permanenti e accidentali (contrassegnata in stampa dal simbolo --);
- x_{Mmax} : ascissa dell'asta in cui si verifica il momento massimo positivo;
- M_{max} : valore del momento massimo positivo;
- x_{fmax} : ascissa in cui si verifica la freccia massima in campata;
- F_{max} : valore della freccia massima in campata;
- f_{max}/l : rapporto fra freccia massima e luce dell'asta.

La verifica di stabilità viene effettuata per le sole combinazioni di carico che presentano, in almeno un'ascissa, condizioni di lavoro a pressoflessione. Il prospetto riepilogativo della verifica a stabilità riporta le informazioni relative all'asta iniziale e finale coinvolte, e inoltre:

- numero combinazione di carico;
- valore dello sforzo normale; (compressione più elevata trovata in tutte le ascisse soggette a verifica);
- valore del momento flettente M_y equivalente;
- valore del momento flettente M_z equivalente;
- snellezza ω (che influisce sullo sforzo normale), solo per acciaio e alluminio;
- snellezza nel piano locale "yx" (che influisce su M_z);
- snellezza nel piano locale "zx" (che influisce su M_y);
- ω ; ω_1 (solo per acciaio e alluminio);
- tensione nell'acciaio o alluminio; nel caso del legno viene riportata un valore di tensione (F_x , M) calcolato nei modi già espressi per la verifica di resistenza;
- Nota, eventuale, qualora le tensioni superino i limiti ammessi, oppure quando la snellezza supera il valore 250 (200 per il legno e alluminio).

VERIFICHE DI OPERE IN ACCIAIO CON IL METODO DELL'EUROCODICE 3

I RISULTATI PER ASTE RETICOLARI

Il tabulato riporta una descrizione dei parametri di progetto e successivamente, in sequenza per ogni asta:

- numero combinazione di carico;
- sforzo normale N (corrispondente a F_x), positivo se di trazione;
- classe della sezione; non viene riportata se agisce la trazione;
- A_{net} oppure A_{eff} : viene riportato il valore della sezione (cm^2) utilizzata in fase di verifica;
- snellezza adimensionale; dipende dalla snellezza dell'asta nei due piani di e quella ulteriore, eventuale, derivante da assi principali di inerzia della sezione non coincidenti con gli assi locali y e z (come avviene per la sezione a L); viene ovviamente determinata solo per aste compresse;
- χ_{minimo} : rappresenta il minimo fra i coefficienti di riduzione del modo di instabilità intorno agli assi coinvolti nella verifica, che possono riguardare anche gli assi principali di inerzia;
- I.R., indice di resistenza: viene determinato l'indice di verifica a resistenza, ottenuto come rapporto fra la sollecitazione esterna N_{sd} e la resistenza di progetto, comunemente indicate con il termine $N_t.Rd$ (nel caso trazione) oppure $N_c.Rd$ (nel caso compressione);
- I.S., indice di stabilità: viene determinato l'indice all'instabilità flessionale, ottenuto come rapporto fra la sollecitazione esterna N_{sd} e la resistenza di progetto all'instabilità $N_b.Rd$ nei piani di flessione sopra specificati.

A fine riga compaiono due note; la prima indica il piano di massima snellezza e il suo valore; la seconda, eventuali informazioni di commento.

Se è abilitata la verifica di stabilità per aste consecutive (superelementi) viene riportato un ulteriore tabulato riguardante la verifica globale delle aste che costituiscono il superelemento; la sola differenza con il precedente riguarda l'indicazione, nel prospetto, della lunghezza totale che influisce sul valore di snellezza e quindi sul risultato finale della verifica.

I RISULTATI PER TRAVI E PILASTRI

Il tabulato riporta:

- numero combinazione di carico;
- ascissa di calcolo (cm);
- in sequenza F_x , F_y , F_z (F), M_x , M_y , M_z (F*m).

Le convenzioni sui segni delle sollecitazioni sono:

- F_x (sforzo normale) è positivo se di trazione;
- F_y (forza tagliante) è positiva se agisce, a sinistra della sezione interessata, nel verso positivo dell'asse locale corrispondente;
- F_z (forza tagliante) è positiva se agisce, a sinistra della sezione interessata, nel verso negativo dell'asse locale corrispondente;
- M_x (momento torcente) è positivo se antiorario intorno a x a sinistra dell'ascissa in esame;
- M_y (momento flettente) è positivo se tende le fibre posteriori, cioè quelle disposte nel verso negativo dell'asse z;
- M_z (momento flettente) è positivo se tende le fibre inferiori, cioè quelle disposte nel verso negativo dell'asse y.

Vengono poi riportate:

- classe: rappresenta la classe della sezione; qualora i singoli componenti della sezione (ad esempio ala e anima) abbiano classi diverse viene presa quella più alta; non viene riportata in caso di trazione o taglio puro.

Il potenziale svergolamento viene indagato solo per sezioni a I. Viene riportato il valore di χ_{LT} , che determina il momento resistente di progetto. La stabilità euleriana comporta la determinazione di tre coefficienti χ_{min} , k_y , k_z . Il tabulato propone:

- numero combinazione di carico;
- valore dello sforzo normale F_x (compressione più elevata trovata);
- momento flettente M_y più elevato riscontrato in tutte le ascisse;
- momento flettente M_z più elevato riscontrato in tutte le ascisse;
- classe: rappresenta la classe della sezione;
- χ_{minimo} : rappresenta il minimo fra i coefficienti di riduzione del modo di instabilità intorno agli assi coinvolti nella verifica.

RISULTATI DELLE VERIFICHE

Si riportano i risultati ottenuti con i verificatori per le aste più sollecitate.

VERIFICA ELEMENTI IN ACCIAIO

AMV s.r.l.
Via San Lorenzo, 106 Tel. 0481/779903
34077 Ronchi dei Legionari (GO)

Lavoro: **Struttura R01** Intestazione lavoro:
Elemento: **TRAVE** Metodo di verifica: **Eurocodice 3 - NTC 2018**
Gruppo: **1** Descrizione: **Travi**
Tabella: **Tabella travi** Struttura: **Nuova**
Tipo acciaio: **S 355** Beta piano 'yx': **1.000** Beta piano 'zx': **1.000**
Tipologia sismica: **Senza prescrizioni aggiuntive**
γM0: **1.050** γM1: **1.050** γM1': **1.050** γM2: **1.250** γrv: **0.000** γM0 Pf: **1.000** γM1 Pf: **1.000**
Tipo collegamento: **saldato** Connessione su un solo lato Connessione sul lato corto (solo 'L')

ASTA NUM. **1** NI 1 NF 22 Lungh. 250.0 cm SEZ. 1 Ps HEB 600

categoria: p.p. y Permanente Congresso Neve qy tot.
qy medio: 211.95 1443.00 975.00 195.00 2824.95 kg/m

Sollecitazioni di calcolo e di verifica

Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	cm	kg			kg*m							
1A	0	-7246	12006	532	0	381	-206	3	0.05	0.01	0.02	
1B	0	-7246	12474	532	0	381	-208	3	0.06	0.01	0.02	
1C	0	-7246	12006	-532	0	-381	-206	3	0.05	0.01	0.02	
1D	0	-7246	12474	-532	0	-381	-208	3	0.06	0.01	0.02	
1E	0	7246	12006	532	0	381	-206	1	0.05	0.01	0.01	
1F	0	7246	12474	532	0	381	-208	1	0.06	0.01	0.01	
1G	0	7246	12006	-532	0	-381	-206	1	0.05	0.01	0.01	
1H	0	7246	12474	-532	0	-381	-208	1	0.06	0.01	0.01	
1I	0	-2849	12006	254	0	228	-206	3	0.05	0.00	0.01	
1J	0	-2849	12474	254	0	228	-208	3	0.06	0.00	0.01	
1K	0	-2849	12006	-254	0	-228	-206	3	0.05	0.00	0.01	
1L	0	-2849	12474	-254	0	-228	-208	3	0.06	0.00	0.01	
1M	0	2849	12006	254	0	228	-206	1	0.05	0.00	0.00	
1N	0	2849	12474	254	0	228	-208	1	0.06	0.00	0.00	
1O	0	2849	12006	-254	0	-228	-206	1	0.05	0.00	0.00	
1P	0	2849	12474	-254	0	-228	-208	1	0.06	0.00	0.00	
1Q	0	-2330	11460	181	0	141	-204	3	0.05	0.00	0.01	
1R	0	-2330	13020	181	0	141	-210	3	0.06	0.00	0.01	
1S	0	-2330	11460	-181	0	-141	-204	3	0.05	0.00	0.01	
1T	0	-2330	13020	-181	0	-141	-210	3	0.06	0.00	0.01	
1U	0	2330	11460	181	0	141	-204	1	0.05	0.00	0.00	
1V	0	2330	13020	181	0	141	-210	1	0.06	0.00	0.00	
1W	0	2330	11460	-181	0	-141	-204	1	0.05	0.00	0.00	
1X	0	2330	13020	-181	0	-141	-210	1	0.06	0.00	0.00	
2	0	-1262	12240	581	0	-21	-207	3	0.06	0.00	0.00	
3	0	-757	20190	348	0	-13	-342	3	0.09	0.00	0.00	
4	0	-757	28800	348	0	-13	-488	3	0.13	0.00	0.00	
5	0	-1262	22340	581	0	-21	-378	3	0.10	0.00	0.00	
7	0	527	20330	18	0	27	-270	1	0.09	0.00	0.00	
20	0	-1552	19630	20	0	31	-2070	3	0.09	0.00	0.01	
22	0	1035	1059	-13	0	-21	-1177	1	0.00	0.00	0.01	
1A	125	-7246	9940	532	0	984	14098	3	0.05	0.01	0.11	
1B	125	-7246	10407	532	0	984	13511	3	0.05	0.01	0.11	
1C	125	-7246	9940	-532	0	-984	14098	3	0.05	0.01	0.11	
1D	125	-7246	10407	-532	0	-984	13511	3	0.05	0.01	0.11	
1E	125	7246	9940	532	0	984	14098	1	0.05	0.01	0.06	
1F	125	7246	10407	532	0	984	13511	1	0.05	0.01	0.06	
1G	125	7246	9940	-532	0	-984	14098	1	0.05	0.01	0.06	
1H	125	7246	10407	-532	0	-984	13511	1	0.05	0.01	0.06	
1I	125	-2849	9940	254	0	-186	14098	3	0.05	0.00	0.08	
1J	125	-2849	10407	254	0	-186	13511	3	0.05	0.00	0.08	
1K	125	-2849	9940	-254	0	186	14098	3	0.05	0.00	0.08	
1L	125	-2849	10407	-254	0	186	13511	3	0.05	0.00	0.08	
1M	125	2849	9940	254	0	-186	14098	1	0.05	0.00	0.06	
1N	125	2849	10407	254	0	-186	13511	1	0.05	0.00	0.06	
1O	125	2849	9940	-254	0	186	14098	1	0.05	0.00	0.06	
1P	125	2849	10407	-254	0	186	13511	1	0.05	0.00	0.06	
1Q	125	-2330	9394	181	0	323	14781	3	0.04	0.00	0.09	
1R	125	-2330	10953	181	0	323	12828	3	0.05	0.00	0.08	
1S	125	-2330	9394	-181	0	-323	14781	3	0.04	0.00	0.09	
1T	125	-2330	10953	-181	0	-323	12828	3	0.05	0.00	0.08	
1U	125	2330	9394	181	0	323	14781	1	0.04	0.00	0.07	
1V	125	2330	10953	181	0	323	12828	1	0.05	0.00	0.06	
1W	125	2330	9394	-181	0	-323	14781	1	0.04	0.00	0.07	
1X	125	2330	10953	-181	0	-323	12828	1	0.05	0.00	0.06	
2	125	-1262	10174	86	0	-438	13804	3	0.05	0.00	0.09	
3	125	-757	16775	51	0	-263	22764	3	0.08	0.00	0.13	
4	125	-757	23920	51	0	-263	32460	3	0.11	0.00	0.17	

5	125	-1262	18560	86	0	-438	25189	3	0.08	0.00	0.14	
7	125	527	17280	18	0	4	23236	1	0.08	0.00	0.10	
20	125	-1552	16580	20	0	6	20561	3	0.08	0.00	0.11	
22	125	1035	1059	-13	0	-4	146	1	0.00	0.00	0.00	
1A	250	-7246	7873	532	0	1587	25815	3	0.04	0.01	0.19	
1B	250	-7246	8341	532	0	1587	24645	3	0.04	0.01	0.18	
1C	250	-7246	7873	-532	0	-1587	25815	3	0.04	0.01	0.19	
1D	250	-7246	8341	-532	0	-1587	24645	3	0.04	0.01	0.18	
1E	250	7246	7873	532	0	1587	25815	1	0.04	0.01	0.12	
1F	250	7246	8341	532	0	1587	24645	1	0.04	0.01	0.11	
1G	250	7246	7873	-532	0	-1587	25815	1	0.04	0.01	0.12	
1H	250	7246	8341	-532	0	-1587	24645	1	0.04	0.01	0.11	
1I	250	-2849	7873	254	0	-601	25815	3	0.04	0.00	0.15	
1J	250	-2849	8341	254	0	-601	24645	3	0.04	0.00	0.15	
1K	250	-2849	7873	-254	0	601	25815	3	0.04	0.00	0.15	
1L	250	-2849	8341	-254	0	601	24645	3	0.04	0.00	0.15	
1M	250	2849	7873	254	0	-601	25815	1	0.04	0.00	0.12	
1N	250	2849	8341	254	0	-601	24645	1	0.04	0.00	0.11	
1O	250	2849	7873	-254	0	601	25815	1	0.04	0.00	0.12	
1P	250	2849	8341	-254	0	601	24645	1	0.04	0.00	0.11	
1Q	250	-2330	7327	181	0	505	27181	3	0.03	0.00	0.16	
1R	250	-2330	8886	181	0	505	23279	3	0.04	0.00	0.14	
1S	250	-2330	7327	-181	0	-505	27181	3	0.03	0.00	0.16	
1T	250	-2330	8886	-181	0	-505	23279	3	0.04	0.00	0.14	
1U	250	2330	7327	181	0	505	27181	1	0.03	0.00	0.12	
1V	250	2330	8886	181	0	505	23279	1	0.04	0.00	0.11	
1W	250	2330	7327	-181	0	-505	27181	1	0.03	0.00	0.12	
1X	250	2330	8886	-181	0	-505	23279	1	0.04	0.00	0.11	
2	250	-1262	8107	-409	0	-236	25230	3	0.04	0.00	0.14	
3	250	-757	13360	-246	0	-141	41600	3	0.06	0.00	0.22	
4	250	-757	19040	-246	0	-141	59310	3	0.09	0.00	0.31	
5	250	-1262	14780	-409	0	-236	46030	3	0.07	0.00	0.24	
7	250	527	14230	18	0	-18	42930	1	0.06	0.00	0.19	
20	250	-1552	13530	20	0	-18	39380	3	0.06	0.00	0.20	
22	250	1035	1059	-13	0	12	1470	1	0.00	0.00	0.01	

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	$\gamma_{min.}$	ky	kz	kLT	χ_{LT}	I.S.n.	I.S.m.	I.S.	Nota
--	kg	kg*m	kg*m										
1A	-7246	1587	25815	3	0.8987	1.0033	1.0005	--	--	0.01	--	0.19	Snell. 'zx' = 35
1B	-7246	1587	24645	3	0.8987	1.0033	1.0005	--	--	0.01	--	0.19	Snell. 'zx' = 35
1C	-7246	-1587	25815	3	0.8987	1.0033	1.0005	--	--	0.01	--	0.19	Snell. 'zx' = 35
1D	-7246	-1587	24645	3	0.8987	1.0033	1.0005	--	--	0.01	--	0.19	Snell. 'zx' = 35
1I	-2849	-601	25815	3	0.8987	1.0007	1.0002	--	--	0.00	--	0.15	Snell. 'zx' = 35
1J	-2849	-601	24645	3	0.8987	1.0007	1.0002	--	--	0.00	--	0.15	Snell. 'zx' = 35
1K	-2849	601	25815	3	0.8987	1.0007	1.0002	--	--	0.00	--	0.15	Snell. 'zx' = 35
1L	-2849	601	24645	3	0.8987	1.0007	1.0002	--	--	0.00	--	0.15	Snell. 'zx' = 35
1Q	-2330	505	27181	3	0.8987	1.0014	1.0002	--	--	0.00	--	0.16	Snell. 'zx' = 35
1R	-2330	505	23279	3	0.8987	1.0014	1.0002	--	--	0.00	--	0.14	Snell. 'zx' = 35
1S	-2330	-505	27181	3	0.8987	1.0014	1.0002	--	--	0.00	--	0.16	Snell. 'zx' = 35
1T	-2330	-505	23279	3	0.8987	1.0014	1.0002	--	--	0.00	--	0.14	Snell. 'zx' = 35
2	-1262	-438	25230	3	0.8987	1.0008	1.0001	--	--	0.00	--	0.14	Snell. 'zx' = 35
3	-757	-263	41600	3	0.8987	1.0006	1.0000	--	--	0.00	--	0.22	Snell. 'zx' = 35
4	-757	-263	59310	3	0.8987	1.0006	1.0000	--	--	0.00	--	0.31	Snell. 'zx' = 35
5	-1262	-438	46030	3	0.8987	1.0008	1.0001	--	--	0.00	--	0.25	Snell. 'zx' = 35
20	-1552	31	39380	3	0.8987	1.0091	1.0001	--	--	0.00	--	0.20	Snell. 'zx' = 35

ASTA NUM. 2 NI 7 NF 20 Lungh. 245.0 cm SEZ. 1 Ps HEB 600

categoria: p.p. y Permanente Congresso Neve qy tot.
 qy medio: 211.95 1443.00 975.00 195.00 2824.95 kg/m

Sollecitazioni di calcolo e di verifica

Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
--	cm	kg	kg	kg	kg*m	kg*m	kg*m					
1A	0	-14537	3992	1819	0	994	40912	3	0.02	0.02	0.26	
1B	0	-14537	4132	1819	0	994	38928	3	0.02	0.02	0.25	
1C	0	-14537	3992	-1819	0	-994	40912	3	0.02	0.02	0.26	
1D	0	-14537	4132	-1819	0	-994	38928	3	0.02	0.02	0.25	
1E	0	14537	3992	1819	0	994	40912	1	0.02	0.02	0.18	
1F	0	14537	4132	1819	0	994	38928	1	0.02	0.02	0.18	
1G	0	14537	3992	-1819	0	-994	40912	1	0.02	0.02	0.18	
1H	0	14537	4132	-1819	0	-994	38928	1	0.02	0.02	0.18	
1I	0	-5323	3992	589	0	342	40912	3	0.02	0.01	0.22	
1J	0	-5323	4132	589	0	342	38928	3	0.02	0.01	0.21	
1K	0	-5323	3992	-589	0	-342	40912	3	0.02	0.01	0.22	
1L	0	-5323	4132	-589	0	-342	38928	3	0.02	0.01	0.21	
1M	0	5323	3992	589	0	342	40912	1	0.02	0.01	0.18	
1N	0	5323	4132	589	0	342	38928	1	0.02	0.01	0.18	
1O	0	5323	3992	-589	0	-342	40912	1	0.02	0.01	0.18	
1P	0	5323	4132	-589	0	-342	38928	1	0.02	0.01	0.18	
1Q	0	-4583	3828	556	0	308	43228	3	0.02	0.00	0.23	
1R	0	-4583	4296	556	0	308	36612	3	0.02	0.00	0.20	
1S	0	-4583	3828	-556	0	-308	43228	3	0.02	0.00	0.23	
1T	0	-4583	4296	-556	0	-308	36612	3	0.02	0.00	0.20	
1U	0	4583	3828	556	0	308	43228	1	0.02	0.00	0.20	
1V	0	4583	4296	556	0	308	36612	1	0.02	0.00	0.17	
1W	0	4583	3828	-556	0	-308	43228	1	0.02	0.00	0.20	
1X	0	4583	4296	-556	0	-308	36612	1	0.02	0.00	0.17	
2	0	-2566	4062	717	0	352	39920	3	0.02	0.00	0.22	

3	0	-1540	6707	430	0	211	65790	3	0.03	0.00	0.34
4	0	-1540	9578	430	0	211	93760	3	0.04	0.00	0.49
5	0	-2566	7424	717	0	352	72790	3	0.03	0.00	0.38
7	0	1607	8278	1	0	6	70090	1	0.04	0.00	0.32
20	0	-1543	5808	4	0	14	60580	3	0.03	0.00	0.31
22	0	1029	-121	-2	0	-9	1184	1	0.00	0.00	0.01
1A	122	-14537	1965	1819	0	-1242	44729	3	0.01	0.02	0.28
1B	122	-14537	2105	1819	0	-1242	42584	3	0.01	0.02	0.27
1C	122	-14537	1965	-1819	0	1242	44729	3	0.01	0.02	0.28
1D	122	-14537	2105	-1819	0	1242	42584	3	0.01	0.02	0.27
1E	122	14537	1965	1819	0	-1242	44729	1	0.01	0.02	0.20
1F	122	14537	2105	1819	0	-1242	42584	1	0.01	0.02	0.19
1G	122	14537	1965	-1819	0	1242	44729	1	0.01	0.02	0.20
1H	122	14537	2105	-1819	0	1242	42584	1	0.01	0.02	0.19
1I	122	-5323	1965	589	0	-388	44729	3	0.01	0.01	0.25
1J	122	-5323	2105	589	0	-388	42584	3	0.01	0.01	0.23
1K	122	-5323	1965	-589	0	388	44729	3	0.01	0.01	0.25
1L	122	-5323	2105	-589	0	388	42584	3	0.01	0.01	0.23
1M	122	5323	1965	589	0	-388	44729	1	0.01	0.01	0.20
1N	122	5323	2105	589	0	-388	42584	1	0.01	0.01	0.19
1O	122	5323	1965	-589	0	388	44729	1	0.01	0.01	0.20
1P	122	5323	2105	-589	0	388	42584	1	0.01	0.01	0.19
1Q	122	-4583	1801	556	0	-376	47232	3	0.01	0.00	0.26
1R	122	-4583	2268	556	0	-376	40081	3	0.01	0.00	0.22
1S	122	-4583	1801	-556	0	376	47232	3	0.01	0.00	0.26
1T	122	-4583	2268	-556	0	376	40081	3	0.01	0.00	0.22
1U	122	4583	1801	556	0	-376	47232	1	0.01	0.00	0.21
1V	122	4583	2268	556	0	-376	40081	1	0.01	0.00	0.18
1W	122	4583	1801	-556	0	376	47232	1	0.01	0.00	0.21
1X	122	4583	2268	-556	0	376	40081	1	0.01	0.00	0.18
2	122	-2566	2035	232	0	-229	43657	3	0.01	0.00	0.23
3	122	-1540	3359	139	0	-137	71955	3	0.02	0.00	0.37
4	122	-1540	4797	139	0	-137	102558	3	0.02	0.00	0.53
5	122	-2566	3719	232	0	-229	79615	3	0.02	0.00	0.42
7	122	1607	5289	1	0	5	78401	1	0.02	0.00	0.35
20	122	-1543	2819	4	0	10	65861	3	0.01	0.00	0.34
22	122	1029	-121	-2	0	-6	1036	1	0.00	0.00	0.00
1A	245	-14537	-63	1819	0	-3479	46063	3	0.00	0.02	0.36
1B	245	-14537	77	1819	0	-3479	43757	3	0.00	0.02	0.35
1C	245	-14537	-63	-1819	0	3479	46063	3	0.00	0.02	0.36
1D	245	-14537	77	-1819	0	3479	43757	3	0.00	0.02	0.35
1E	245	14537	-63	1819	0	-3479	46063	1	0.00	0.02	0.21
1F	245	14537	77	1819	0	-3479	43757	1	0.00	0.02	0.20
1G	245	14537	-63	-1819	0	3479	46063	1	0.00	0.02	0.21
1H	245	14537	77	-1819	0	3479	43757	1	0.00	0.02	0.20
1I	245	-5323	-63	589	0	-1119	46063	3	0.00	0.01	0.28
1J	245	-5323	77	589	0	-1119	43757	3	0.00	0.01	0.26
1K	245	-5323	-63	-589	0	1119	46063	3	0.00	0.01	0.28
1L	245	-5323	77	-589	0	1119	43757	3	0.00	0.01	0.26
1M	245	5323	-63	589	0	-1119	46063	1	0.00	0.01	0.21
1N	245	5323	77	589	0	-1119	43757	1	0.00	0.01	0.20
1O	245	5323	-63	-589	0	1119	46063	1	0.00	0.01	0.21
1P	245	5323	77	-589	0	1119	43757	1	0.00	0.01	0.20
1Q	245	-4583	-226	556	0	-1061	48753	3	0.00	0.00	0.29
1R	245	-4583	241	556	0	-1061	41067	3	0.00	0.00	0.25
1S	245	-4583	-226	-556	0	1061	48753	3	0.00	0.00	0.29
1T	245	-4583	241	-556	0	1061	41067	3	0.00	0.00	0.25
1U	245	4583	-226	556	0	-1061	48753	1	0.00	0.00	0.22
1V	245	4583	241	556	0	-1061	41067	1	0.00	0.00	0.19
1W	245	4583	-226	-556	0	1061	48753	1	0.00	0.00	0.22
1X	245	4583	241	-556	0	1061	41067	1	0.00	0.00	0.19
2	245	-2566	7	-254	0	-215	44910	3	0.00	0.00	0.24
3	245	-1540	12	-152	0	-129	74020	3	0.00	0.00	0.38
4	245	-1540	17	-152	0	-129	105500	3	0.00	0.00	0.54
5	245	-2566	13	-254	0	-215	81900	3	0.00	0.00	0.43
7	245	1607	2300	1	0	4	83050	1	0.01	0.00	0.38
20	245	-1543	-170	4	0	5	67480	3	0.00	0.00	0.35
22	245	1029	-121	-2	0	-3	888	1	0.00	0.00	0.00

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	$\gamma_{min.}$	ky	kz	kLT	χ_{LT}	I.S.n.	I.S.m.	I.S.	Nota
	kg	kg*m											
1A	-14537	-3479	46063	3	0.9027	1.0007	1.0031	--	--	0.02	--	0.36	Snell. 'zx'= 35
1B	-14537	-3479	43757	3	0.9027	1.0007	1.0031	--	--	0.02	--	0.35	Snell. 'zx'= 35
1C	-14537	3479	46063	3	0.9027	1.0007	1.0031	--	--	0.02	--	0.36	Snell. 'zx'= 35
1D	-14537	3479	43757	3	0.9027	1.0007	1.0031	--	--	0.02	--	0.35	Snell. 'zx'= 35
1I	-5323	-1119	46063	3	0.9027	1.0007	1.0011	--	--	0.01	--	0.28	Snell. 'zx'= 35
1J	-5323	-1119	43757	3	0.9027	1.0007	1.0011	--	--	0.01	--	0.27	Snell. 'zx'= 35
1K	-5323	1119	46063	3	0.9027	1.0007	1.0011	--	--	0.01	--	0.28	Snell. 'zx'= 35
1L	-5323	1119	43757	3	0.9027	1.0007	1.0011	--	--	0.01	--	0.27	Snell. 'zx'= 35
1Q	-4583	-1061	48753	3	0.9027	1.0007	1.0010	--	--	0.01	--	0.29	Snell. 'zx'= 35
1R	-4583	-1061	41067	3	0.9027	1.0007	1.0010	--	--	0.01	--	0.25	Snell. 'zx'= 35
1S	-4583	1061	48753	3	0.9027	1.0007	1.0010	--	--	0.01	--	0.29	Snell. 'zx'= 35
1T	-4583	1061	41067	3	0.9027	1.0007	1.0010	--	--	0.01	--	0.25	Snell. 'zx'= 35
2	-2566	352	44910	3	0.9027	1.0007	1.0006	--	--	0.00	--	0.24	Snell. 'zx'= 35
3	-1540	211	74020	3	0.9027	1.0009	1.0003	--	--	0.00	--	0.39	Snell. 'zx'= 35
4	-1540	211	105500	3	0.9027	1.0009	1.0003	--	--	0.00	--	0.55	Snell. 'zx'= 35
5	-2566	352	81900	3	0.9027	1.0007	1.0006	--	--	0.00	--	0.43	Snell. 'zx'= 35
20	-1543	14	67480	3	0.9027	1.0090	1.0003	--	--	0.00	--	0.35	Snell. 'zx'= 35

ASTA NUM. 3 NI 8 NF 19 Lungh. 55.0 cm SEZ. 1 Ps HEB 600

categoria: p.p. y Permanente Congresso Neve qy tot.
 qy medio: 211.95 1443.00 975.00 195.00 2824.95 kg/m
 Sollecitazioni di calcolo e di verifica

Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	cm	kg			kg*m							
1A	0	-7762	-4244	2344	0	662	40978	3	0.02	0.01	0.24	
1B	0	-7762	-3998	2344	0	662	38942	3	0.02	0.01	0.23	
1C	0	-7762	-4244	-2344	0	-662	40978	3	0.02	0.01	0.24	
1D	0	-7762	-3998	-2344	0	-662	38942	3	0.02	0.01	0.23	
1E	0	7762	-4244	2344	0	662	40978	1	0.02	0.01	0.19	
1F	0	7762	-3998	2344	0	662	38942	1	0.02	0.01	0.18	
1G	0	7762	-4244	-2344	0	-662	40978	1	0.02	0.01	0.19	
1H	0	7762	-3998	-2344	0	-662	38942	1	0.02	0.01	0.18	
1I	0	-4449	-4244	795	0	265	40978	3	0.02	0.00	0.22	
1J	0	-4449	-3998	795	0	265	38942	3	0.02	0.00	0.21	
1K	0	-4449	-4244	-795	0	-265	40978	3	0.02	0.00	0.22	
1L	0	-4449	-3998	-795	0	-265	38942	3	0.02	0.00	0.21	
1M	0	4449	-4244	795	0	265	40978	1	0.02	0.00	0.19	
1N	0	4449	-3998	795	0	265	38942	1	0.02	0.00	0.18	
1O	0	4449	-4244	-795	0	-265	40978	1	0.02	0.00	0.19	
1P	0	4449	-3998	-795	0	-265	38942	1	0.02	0.00	0.18	
1Q	0	-2818	-4531	724	0	214	43353	3	0.02	0.00	0.23	
1R	0	-2818	-3711	724	0	214	36567	3	0.02	0.00	0.20	
1S	0	-2818	-4531	-724	0	-214	43353	3	0.02	0.00	0.23	
1T	0	-2818	-3711	-724	0	-214	36567	3	0.02	0.00	0.20	
1U	0	2818	-4531	724	0	214	43353	1	0.02	0.00	0.20	
1V	0	2818	-3711	724	0	214	36567	1	0.02	0.00	0.17	
1W	0	2818	-4531	-724	0	-214	43353	1	0.02	0.00	0.20	
1X	0	2818	-3711	-724	0	-214	36567	1	0.02	0.00	0.17	
2	0	-1262	-4121	92	0	395	39960	3	0.02	0.00	0.22	
3	0	-757	-6778	55	0	237	65850	3	0.03	0.00	0.34	
4	0	-757	-9640	55	0	237	93850	3	0.04	0.00	0.49	
5	0	-1262	-7494	92	0	395	72850	3	0.03	0.00	0.38	
7	0	590	-7312	16	0	21	72690	1	0.03	0.00	0.33	
20	0	-470	-6244	25	0	25	59740	3	0.03	0.00	0.31	
22	0	314	-121	-16	0	-17	592	1	0.00	0.00	0.00	
1A	28	-7762	-4699	2344	0	-20	39747	3	0.02	0.01	0.21	
1B	28	-7762	-4453	2344	0	-20	37778	3	0.02	0.01	0.20	
1C	28	-7762	-4699	-2344	0	20	39747	3	0.02	0.01	0.21	
1D	28	-7762	-4453	-2344	0	20	37778	3	0.02	0.01	0.20	
1E	28	7762	-4699	2344	0	-20	39747	1	0.02	0.01	0.18	
1F	28	7762	-4453	2344	0	-20	37778	1	0.02	0.01	0.17	
1G	28	7762	-4699	-2344	0	20	39747	1	0.02	0.01	0.18	
1H	28	7762	-4453	-2344	0	20	37778	1	0.02	0.01	0.17	
1I	28	-4449	-4699	795	0	7	39747	3	0.02	0.00	0.21	
1J	28	-4449	-4453	795	0	7	37778	3	0.02	0.00	0.20	
1K	28	-4449	-4699	-795	0	-7	39747	3	0.02	0.00	0.21	
1L	28	-4449	-4453	-795	0	-7	37778	3	0.02	0.00	0.20	
1M	28	4449	-4699	795	0	7	39747	1	0.02	0.00	0.18	
1N	28	4449	-4453	795	0	7	37778	1	0.02	0.00	0.17	
1O	28	4449	-4699	-795	0	-7	39747	1	0.02	0.00	0.18	
1P	28	4449	-4453	-795	0	-7	37778	1	0.02	0.00	0.17	
1Q	28	-2818	-4986	724	0	-3	42045	3	0.02	0.00	0.22	
1R	28	-2818	-4166	724	0	-3	35480	3	0.02	0.00	0.18	
1S	28	-2818	-4986	-724	0	3	42045	3	0.02	0.00	0.22	
1T	28	-2818	-4166	-724	0	3	35480	3	0.02	0.00	0.18	
1U	28	2818	-4986	724	0	-3	42045	1	0.02	0.00	0.19	
1V	28	2818	-4166	724	0	-3	35480	1	0.02	0.00	0.16	
1W	28	2818	-4986	-724	0	3	42045	1	0.02	0.00	0.19	
1X	28	2818	-4166	-724	0	3	35480	1	0.02	0.00	0.16	
2	28	-1262	-4576	-17	0	385	38763	3	0.02	0.00	0.21	
3	28	-757	-7529	-10	0	231	63883	3	0.03	0.00	0.33	
4	28	-757	-10715	-10	0	231	91048	3	0.05	0.00	0.47	
5	28	-1262	-8326	-17	0	385	70674	3	0.04	0.00	0.37	
7	28	590	-7983	16	0	16	70587	1	0.04	0.00	0.32	
20	28	-470	-6915	25	0	19	57932	3	0.03	0.00	0.30	
22	28	314	-121	-16	0	-12	559	1	0.00	0.00	0.00	
1A	55	-7762	-5154	2344	0	-701	38392	3	0.02	0.01	0.23	
1B	55	-7762	-4908	2344	0	-701	36488	3	0.02	0.01	0.22	
1C	55	-7762	-5154	-2344	0	701	38392	3	0.02	0.01	0.23	
1D	55	-7762	-4908	-2344	0	701	36488	3	0.02	0.01	0.22	
1E	55	7762	-5154	2344	0	-701	38392	1	0.02	0.01	0.17	
1F	55	7762	-4908	2344	0	-701	36488	1	0.02	0.01	0.16	
1G	55	7762	-5154	-2344	0	701	38392	1	0.02	0.01	0.17	
1H	55	7762	-4908	-2344	0	701	36488	1	0.02	0.01	0.16	
1I	55	-4449	-5154	795	0	-250	38392	3	0.02	0.00	0.21	
1J	55	-4449	-4908	795	0	-250	36488	3	0.02	0.00	0.20	
1K	55	-4449	-5154	-795	0	250	38392	3	0.02	0.00	0.21	
1L	55	-4449	-4908	-795	0	250	36488	3	0.02	0.00	0.20	
1M	55	4449	-5154	795	0	-250	38392	1	0.02	0.00	0.17	
1N	55	4449	-4908	795	0	-250	36488	1	0.02	0.00	0.16	
1O	55	4449	-5154	-795	0	250	38392	1	0.02	0.00	0.17	
1P	55	4449	-4908	-795	0	250	36488	1	0.02	0.00	0.16	
1Q	55	-2818	-5441	724	0	-220	40612	3	0.02	0.00	0.22	
1R	55	-2818	-4621	724	0	-220	34268	3	0.02	0.00	0.18	
1S	55	-2818	-5441	-724	0	220	40612	3	0.02	0.00	0.22	
1T	55	-2818	-4621	-724	0	220	34268	3	0.02	0.00	0.18	
1U	55	2818	-5441	724	0	-220	40612	1	0.02	0.00	0.18	
1V	55	2818	-4621	724	0	-220	34268	1	0.02	0.00	0.15	
1W	55	2818	-5441	-724	0	220	40612	1	0.02	0.00	0.18	
1X	55	2818	-4621	-724	0	220	34268	1	0.02	0.00	0.15	
2	55	-1262	-5031	-126	0	404	37440	3	0.02	0.00	0.20	
3	55	-757	-8281	-76	0	243	61710	3	0.04	0.00	0.32	
4	55	-757	-11790	-76	0	243	87950	3	0.05	0.00	0.46	

5	55	-1262	-9158	-126	0	404	68270	3	0.04	0.00	0.36
7	55	590	-8654	16	0	12	68300	1	0.04	0.00	0.31
20	55	-470	-7586	25	0	12	55940	3	0.03	0.00	0.29
22	55	314	-121	-16	0	-8	526	1	0.00	0.00	0.00

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	$\gamma_{min.}$	ky	kz	kLT	χ_{LT}	I.S.n.	I.S.m.	I.S.	Nota
	kg	kg*m											
1A	-7762	-701	40978	3	1.0000	0.9993	1.0004	--	--	0.01	--	0.24	Snell. 'zx'= 8
1B	-7762	-701	38942	3	1.0000	0.9993	1.0004	--	--	0.01	--	0.23	Snell. 'zx'= 8
1C	-7762	701	40978	3	1.0000	0.9993	1.0004	--	--	0.01	--	0.24	Snell. 'zx'= 8
1D	-7762	701	38942	3	1.0000	0.9993	1.0004	--	--	0.01	--	0.23	Snell. 'zx'= 8
1I	-4449	265	40978	3	1.0000	0.9996	1.0002	--	--	0.00	--	0.22	Snell. 'zx'= 8
1J	-4449	265	38942	3	1.0000	0.9996	1.0002	--	--	0.00	--	0.21	Snell. 'zx'= 8
1K	-4449	-265	40978	3	1.0000	0.9996	1.0002	--	--	0.00	--	0.22	Snell. 'zx'= 8
1L	-4449	-265	38942	3	1.0000	0.9996	1.0002	--	--	0.00	--	0.21	Snell. 'zx'= 8
1Q	-2818	-220	43353	3	1.0000	0.9997	1.0001	--	--	0.00	--	0.23	Snell. 'zx'= 8
1R	-2818	-220	36567	3	1.0000	0.9997	1.0001	--	--	0.00	--	0.20	Snell. 'zx'= 8
1S	-2818	220	43353	3	1.0000	0.9997	1.0001	--	--	0.00	--	0.23	Snell. 'zx'= 8
1T	-2818	220	36567	3	1.0000	0.9997	1.0001	--	--	0.00	--	0.20	Snell. 'zx'= 8
2	-1262	405	39960	3	1.0000	1.0002	1.0001	--	--	0.00	--	0.22	Snell. 'zx'= 8
3	-757	243	65850	3	1.0000	1.0001	1.0000	--	--	0.00	--	0.34	Snell. 'zx'= 8
4	-757	243	93850	3	1.0000	1.0001	1.0000	--	--	0.00	--	0.49	Snell. 'zx'= 8
5	-1262	405	72850	3	1.0000	1.0002	1.0001	--	--	0.00	--	0.39	Snell. 'zx'= 8
20	-470	25	59740	3	1.0000	1.0001	1.0000	--	--	0.00	--	0.31	Snell. 'zx'= 8

ASTA NUM. 4 NI 2 NF 25 Lungh. 250.0 cm SEZ. 1 Ps HEB 600

categoria: p.p. y Permanente Congresso Neve qy tot.
 qy medio: 211.95 1443.00 975.00 195.00 2824.95 kg/m

Sollecitazioni di calcolo e di verifica

Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	cm	kg			kg*m							
1A	0	-8098	12006	1187	0	1028	-206	3	0.05	0.01	0.04	
1B	0	-8098	12474	1187	0	1028	-208	3	0.06	0.01	0.04	
1C	0	-8098	12006	-1187	0	-1028	-206	3	0.05	0.01	0.04	
1D	0	-8098	12474	-1187	0	-1028	-208	3	0.06	0.01	0.04	
1E	0	8098	12006	1187	0	1028	-206	1	0.05	0.01	0.02	
1F	0	8098	12474	1187	0	1028	-208	1	0.06	0.01	0.02	
1G	0	8098	12006	-1187	0	-1028	-206	1	0.05	0.01	0.02	
1H	0	8098	12474	-1187	0	-1028	-208	1	0.06	0.01	0.02	
1I	0	-5012	12006	464	0	559	-206	3	0.05	0.01	0.02	
1J	0	-5012	12474	464	0	559	-208	3	0.06	0.01	0.02	
1K	0	-5012	12006	-464	0	-559	-206	3	0.05	0.01	0.02	
1L	0	-5012	12474	-464	0	-559	-208	3	0.06	0.01	0.02	
1M	0	5012	12006	464	0	559	-206	1	0.05	0.01	0.01	
1N	0	5012	12474	464	0	559	-208	1	0.06	0.01	0.01	
1O	0	5012	12006	-464	0	-559	-206	1	0.05	0.01	0.01	
1P	0	5012	12474	-464	0	-559	-208	1	0.06	0.01	0.01	
1Q	0	-3026	11460	381	0	366	-204	3	0.05	0.00	0.02	
1R	0	-3026	13020	381	0	366	-210	3	0.06	0.00	0.02	
1S	0	-3026	11460	-381	0	-366	-204	3	0.05	0.00	0.02	
1T	0	-3026	13020	-381	0	-366	-210	3	0.06	0.00	0.02	
1U	0	3026	11460	381	0	366	-204	1	0.05	0.00	0.01	
1V	0	3026	13020	381	0	366	-210	1	0.06	0.00	0.01	
1W	0	3026	11460	-381	0	-366	-204	1	0.05	0.00	0.01	
1X	0	3026	13020	-381	0	-366	-210	1	0.06	0.00	0.01	
2	0	1331	12240	328	0	220	-207	1	0.06	0.00	0.00	
3	0	799	20190	197	0	132	-342	1	0.09	0.00	0.00	
4	0	799	28800	197	0	132	-488	1	0.13	0.00	0.00	
5	0	1331	22340	328	0	220	-378	1	0.10	0.00	0.00	
7	0	-538	23530	-29	0	-59	-340	3	0.11	0.00	0.00	
20	0	-5568	21840	-32	0	-62	-4540	3	0.10	0.01	0.03	
22	0	3712	2533	22	0	42	-2823	1	0.01	0.00	0.01	
1A	125	-8098	9940	1187	0	-478	14098	3	0.05	0.01	0.10	
1B	125	-8098	10407	1187	0	-478	13511	3	0.05	0.01	0.09	
1C	125	-8098	9940	-1187	0	478	14098	3	0.05	0.01	0.10	
1D	125	-8098	10407	-1187	0	478	13511	3	0.05	0.01	0.09	
1E	125	8098	9940	1187	0	-478	14098	1	0.05	0.01	0.06	
1F	125	8098	10407	1187	0	-478	13511	1	0.05	0.01	0.06	
1G	125	8098	9940	-1187	0	478	14098	1	0.05	0.01	0.06	
1H	125	8098	10407	-1187	0	478	13511	1	0.05	0.01	0.06	
1I	125	-5012	9940	464	0	-43	14098	3	0.05	0.01	0.08	
1J	125	-5012	10407	464	0	-43	13511	3	0.05	0.01	0.08	
1K	125	-5012	9940	-464	0	43	14098	3	0.05	0.01	0.08	
1L	125	-5012	10407	-464	0	43	13511	3	0.05	0.01	0.08	
1M	125	5012	9940	464	0	-43	14098	1	0.05	0.01	0.06	
1N	125	5012	10407	464	0	-43	13511	1	0.05	0.01	0.06	
1O	125	5012	9940	-464	0	43	14098	1	0.05	0.01	0.06	
1P	125	5012	10407	-464	0	43	13511	1	0.05	0.01	0.06	
1Q	125	-3026	9394	381	0	-120	14781	3	0.04	0.00	0.08	
1R	125	-3026	10953	381	0	-120	12828	3	0.05	0.00	0.07	
1S	125	-3026	9394	-381	0	120	14781	3	0.04	0.00	0.08	
1T	125	-3026	10953	-381	0	120	12828	3	0.05	0.00	0.07	
1U	125	3026	9394	381	0	-120	14781	1	0.04	0.00	0.07	
1V	125	3026	10953	381	0	-120	12828	1	0.05	0.00	0.06	
1W	125	3026	9394	-381	0	120	14781	1	0.04	0.00	0.07	
1X	125	3026	10953	-381	0	120	12828	1	0.05	0.00	0.06	
2	125	1331	10174	328	0	-190	13804	1	0.05	0.00	0.06	

3	125	799	16775	197	0	-114	22764	1	0.08	0.00	0.10
4	125	799	23920	197	0	-114	32460	1	0.11	0.00	0.15
5	125	1331	18560	328	0	-190	25189	1	0.08	0.00	0.11
7	125	-538	20480	-29	0	-23	27161	3	0.09	0.00	0.14
20	125	-5568	18790	-32	0	-22	20851	3	0.09	0.01	0.11
22	125	3712	2533	22	0	15	343	1	0.01	0.00	0.00
1A	250	-8098	7873	1187	0	-1983	25815	3	0.04	0.01	0.20
1B	250	-8098	8341	1187	0	-1983	24645	3	0.04	0.01	0.20
1C	250	-8098	7873	-1187	0	1983	25815	3	0.04	0.01	0.20
1D	250	-8098	8341	-1187	0	1983	24645	3	0.04	0.01	0.20
1E	250	8098	7873	1187	0	-1983	25815	1	0.04	0.01	0.12
1F	250	8098	8341	1187	0	-1983	24645	1	0.04	0.01	0.11
1G	250	8098	7873	-1187	0	1983	25815	1	0.04	0.01	0.12
1H	250	8098	8341	-1187	0	1983	24645	1	0.04	0.01	0.11
1I	250	-5012	7873	464	0	-644	25815	3	0.04	0.01	0.16
1J	250	-5012	8341	464	0	-644	24645	3	0.04	0.01	0.15
1K	250	-5012	7873	-464	0	644	25815	3	0.04	0.01	0.16
1L	250	-5012	8341	-464	0	644	24645	3	0.04	0.01	0.15
1M	250	5012	7873	464	0	-644	25815	1	0.04	0.01	0.12
1N	250	5012	8341	464	0	-644	24645	1	0.04	0.01	0.11
1O	250	5012	7873	-464	0	644	25815	1	0.04	0.01	0.12
1P	250	5012	8341	-464	0	644	24645	1	0.04	0.01	0.11
1Q	250	-3026	7327	381	0	-606	27181	3	0.03	0.00	0.16
1R	250	-3026	8886	381	0	-606	23279	3	0.04	0.00	0.14
1S	250	-3026	7327	-381	0	606	27181	3	0.03	0.00	0.16
1T	250	-3026	8886	-381	0	606	23279	3	0.04	0.00	0.14
1U	250	3026	7327	381	0	-606	27181	1	0.03	0.00	0.12
1V	250	3026	8886	381	0	-606	23279	1	0.04	0.00	0.11
1W	250	3026	7327	-381	0	606	27181	1	0.03	0.00	0.12
1X	250	3026	8886	-381	0	606	23279	1	0.04	0.00	0.11
2	250	1331	8107	328	0	-601	25230	1	0.04	0.00	0.11
3	250	799	13360	197	0	-360	41600	1	0.06	0.00	0.19
4	250	799	19040	197	0	-360	59310	1	0.09	0.00	0.27
5	250	1331	14780	328	0	-601	46030	1	0.07	0.00	0.21
7	250	-538	17430	-29	0	13	50850	3	0.08	0.00	0.26
20	250	-5568	15740	-32	0	18	42430	3	0.07	0.01	0.22
22	250	3712	2533	22	0	-12	3509	1	0.01	0.00	0.02

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χ_{min}	ky	kz	kLT	χ_{LT}	I.S.n.	I.S.m.	I.S.	Nota
	kg	kg*m											
1A	-8098	-1983	25815	3	0.8987	0.9986	1.0006	--	--	0.01	--	0.20	Snell. 'zx'= 35
1B	-8098	-1983	24645	3	0.8987	0.9986	1.0006	--	--	0.01	--	0.20	Snell. 'zx'= 35
1C	-8098	1983	25815	3	0.8987	0.9986	1.0006	--	--	0.01	--	0.20	Snell. 'zx'= 35
1D	-8098	1983	24645	3	0.8987	0.9986	1.0006	--	--	0.01	--	0.20	Snell. 'zx'= 35
1I	-5012	-644	25815	3	0.8987	0.9978	1.0003	--	--	0.01	--	0.16	Snell. 'zx'= 35
1J	-5012	-644	24645	3	0.8987	0.9978	1.0003	--	--	0.01	--	0.15	Snell. 'zx'= 35
1K	-5012	644	25815	3	0.8987	0.9978	1.0003	--	--	0.01	--	0.16	Snell. 'zx'= 35
1L	-5012	644	24645	3	0.8987	0.9978	1.0003	--	--	0.01	--	0.15	Snell. 'zx'= 35
1Q	-3026	-606	27181	3	0.8987	0.9993	1.0002	--	--	0.00	--	0.16	Snell. 'zx'= 35
1R	-3026	-606	23279	3	0.8987	0.9993	1.0002	--	--	0.00	--	0.14	Snell. 'zx'= 35
1S	-3026	606	27181	3	0.8987	0.9993	1.0002	--	--	0.00	--	0.16	Snell. 'zx'= 35
1T	-3026	606	23279	3	0.8987	0.9993	1.0002	--	--	0.00	--	0.14	Snell. 'zx'= 35
7	-538	-59	50850	3	0.8987	1.0000	1.0000	--	--	0.00	--	0.26	Snell. 'zx'= 35
20	-5568	-62	42430	3	0.8987	1.0000	1.0002	--	--	0.01	--	0.22	Snell. 'zx'= 35

ASTA NUM. 5 NI 9 NF 15 Lungh. 245.0 cm SEZ. 1 Ps HEB 600

categoria: p.p. y Permanente Congresso Neve qy tot.
qy medio: 211.95 1443.00 975.00 195.00 2824.95 kg/m

Sollecitazioni di calcolo e di verifica

Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	cm	kg			kg*m							
1A	0	-17067	3992	1860	0	1083	40912	3	0.02	0.02	0.26	
1B	0	-17067	4132	1860	0	1083	38928	3	0.02	0.02	0.25	
1C	0	-17067	3992	-1860	0	-1083	40912	3	0.02	0.02	0.26	
1D	0	-17067	4132	-1860	0	-1083	38928	3	0.02	0.02	0.25	
1E	0	17067	3992	1860	0	1083	40912	1	0.02	0.02	0.18	
1F	0	17067	4132	1860	0	1083	38928	1	0.02	0.02	0.18	
1G	0	17067	3992	-1860	0	-1083	40912	1	0.02	0.02	0.18	
1H	0	17067	4132	-1860	0	-1083	38928	1	0.02	0.02	0.18	
1I	0	-13089	3992	597	0	349	40912	3	0.02	0.01	0.23	
1J	0	-13089	4132	597	0	349	38928	3	0.02	0.01	0.22	
1K	0	-13089	3992	-597	0	-349	40912	3	0.02	0.01	0.23	
1L	0	-13089	4132	-597	0	-349	38928	3	0.02	0.01	0.22	
1M	0	13089	3992	597	0	349	40912	1	0.02	0.01	0.18	
1N	0	13089	4132	597	0	349	38928	1	0.02	0.01	0.18	
1O	0	13089	3992	-597	0	-349	40912	1	0.02	0.01	0.18	
1P	0	13089	4132	-597	0	-349	38928	1	0.02	0.01	0.18	
1Q	0	-6959	3828	567	0	330	43228	3	0.02	0.01	0.24	
1R	0	-6959	4296	567	0	330	36612	3	0.02	0.01	0.20	
1S	0	-6959	3828	-567	0	-330	43228	3	0.02	0.01	0.24	
1T	0	-6959	4296	-567	0	-330	36612	3	0.02	0.01	0.20	
1U	0	6959	3828	567	0	330	43228	1	0.02	0.01	0.20	
1V	0	6959	4296	567	0	330	36612	1	0.02	0.01	0.17	
1W	0	6959	3828	-567	0	-330	43228	1	0.02	0.01	0.20	
1X	0	6959	4296	-567	0	-330	36612	1	0.02	0.01	0.17	
2	0	2572	4062	262	0	218	39920	1	0.02	0.00	0.18	
3	0	1543	6707	158	0	131	65790	1	0.03	0.00	0.30	

4	0	1543	9578	158	0	131	93760	1	0.04	0.00	0.42	
5	0	2572	7424	262	0	218	72790	1	0.03	0.00	0.33	
7	0	-1570	11470	-5	0	-3	85610	3	0.05	0.00	0.44	
20	0	-9148	5557	-7	0	-1	63020	3	0.03	0.01	0.33	
22	0	6098	-288	5	0	0	2816	1	0.00	0.01	0.01	
1A	122	-17067	1965	1860	0	-1202	44729	3	0.01	0.02	0.28	
1B	122	-17067	2105	1860	0	-1202	42584	3	0.01	0.02	0.27	
1C	122	-17067	1965	-1860	0	1202	44729	3	0.01	0.02	0.28	
1D	122	-17067	2105	-1860	0	1202	42584	3	0.01	0.02	0.27	
1E	122	17067	1965	1860	0	-1202	44729	1	0.01	0.02	0.20	
1F	122	17067	2105	1860	0	-1202	42584	1	0.01	0.02	0.19	
1G	122	17067	1965	-1860	0	1202	44729	1	0.01	0.02	0.20	
1H	122	17067	2105	-1860	0	1202	42584	1	0.01	0.02	0.19	
1I	122	-13089	1965	597	0	-386	44729	3	0.01	0.01	0.25	
1J	122	-13089	2105	597	0	-386	42584	3	0.01	0.01	0.24	
1K	122	-13089	1965	-597	0	386	44729	3	0.01	0.01	0.25	
1L	122	-13089	2105	-597	0	386	42584	3	0.01	0.01	0.24	
1M	122	13089	1965	597	0	-386	44729	1	0.01	0.01	0.20	
1N	122	13089	2105	597	0	-386	42584	1	0.01	0.01	0.19	
1O	122	13089	1965	-597	0	386	44729	1	0.01	0.01	0.20	
1P	122	13089	2105	-597	0	386	42584	1	0.01	0.01	0.19	
1Q	122	-6959	1801	567	0	-367	47232	3	0.01	0.01	0.26	
1R	122	-6959	2268	567	0	-367	40081	3	0.01	0.01	0.22	
1S	122	-6959	1801	-567	0	367	47232	3	0.01	0.01	0.26	
1T	122	-6959	2268	-567	0	367	40081	3	0.01	0.01	0.22	
1U	122	6959	1801	567	0	-367	47232	1	0.01	0.01	0.21	
1V	122	6959	2268	567	0	-367	40081	1	0.01	0.01	0.18	
1W	122	6959	1801	-567	0	367	47232	1	0.01	0.01	0.21	
1X	122	6959	2268	-567	0	367	40081	1	0.01	0.01	0.18	
2	122	2572	2035	262	0	-103	43657	1	0.01	0.00	0.20	
3	122	1543	3359	158	0	-62	71955	1	0.02	0.00	0.32	
4	122	1543	4797	158	0	-62	102558	1	0.02	0.00	0.46	
5	122	2572	3719	262	0	-103	79615	1	0.02	0.00	0.36	
7	122	-1570	8483	-5	0	4	97836	3	0.04	0.00	0.50	
20	122	-9148	2568	-7	0	8	68001	3	0.01	0.01	0.36	
22	122	6098	-288	5	0	-5	2464	1	0.00	0.01	0.01	
1A	245	-17067	-63	1860	0	-3487	46063	3	0.01	0.02	0.36	
1B	245	-17067	77	1860	0	-3487	43757	3	0.01	0.02	0.35	
1C	245	-17067	-63	-1860	0	3487	46063	3	0.01	0.02	0.36	
1D	245	-17067	77	-1860	0	3487	43757	3	0.01	0.02	0.35	
1E	245	17067	-63	1860	0	-3487	46063	1	0.01	0.02	0.21	
1F	245	17067	77	1860	0	-3487	43757	1	0.01	0.02	0.20	
1G	245	17067	-63	-1860	0	3487	46063	1	0.01	0.02	0.21	
1H	245	17067	77	-1860	0	3487	43757	1	0.01	0.02	0.20	
1I	245	-13089	-63	597	0	-1121	46063	3	0.00	0.01	0.28	
1J	245	-13089	77	597	0	-1121	43757	3	0.00	0.01	0.27	
1K	245	-13089	-63	-597	0	1121	46063	3	0.00	0.01	0.28	
1L	245	-13089	77	-597	0	1121	43757	3	0.00	0.01	0.27	
1M	245	13089	-63	597	0	-1121	46063	1	0.00	0.01	0.21	
1N	245	13089	77	597	0	-1121	43757	1	0.00	0.01	0.20	
1O	245	13089	-63	-597	0	1121	46063	1	0.00	0.01	0.21	
1P	245	13089	77	-597	0	1121	43757	1	0.00	0.01	0.20	
1Q	245	-6959	-226	567	0	-1063	48753	3	0.00	0.01	0.29	
1R	245	-6959	241	567	0	-1063	41067	3	0.00	0.01	0.25	
1S	245	-6959	-226	-567	0	1063	48753	3	0.00	0.01	0.29	
1T	245	-6959	241	-567	0	1063	41067	3	0.00	0.01	0.25	
1U	245	6959	-226	567	0	-1063	48753	1	0.00	0.01	0.22	
1V	245	6959	241	567	0	-1063	41067	1	0.00	0.01	0.19	
1W	245	6959	-226	-567	0	1063	48753	1	0.00	0.01	0.22	
1X	245	6959	241	-567	0	1063	41067	1	0.00	0.01	0.19	
2	245	2572	7	262	0	-425	44910	1	0.00	0.00	0.20	
3	245	1543	12	158	0	-255	74020	1	0.00	0.00	0.33	
4	245	1543	17	158	0	-255	105500	1	0.00	0.00	0.48	
5	245	2572	13	262	0	-425	81900	1	0.00	0.00	0.37	
7	245	-1570	5496	-5	0	10	106400	3	0.02	0.00	0.54	
20	245	-9148	-421	-7	0	17	69320	3	0.00	0.01	0.36	
22	245	6098	-288	5	0	-11	2112	1	0.00	0.01	0.01	

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χ _{min.}	ky	kz	kLT	χLT	I.S.n.	I.S.m.	I.S.	Nota
	kg	kg*m											
1A	-17067	-3487	46063	3	0.9027	0.9997	1.0037	--	--	0.02	--	0.37	Snell. 'zx'= 35
1B	-17067	-3487	43757	3	0.9027	0.9997	1.0037	--	--	0.02	--	0.36	Snell. 'zx'= 35
1C	-17067	3487	46063	3	0.9027	0.9997	1.0037	--	--	0.02	--	0.37	Snell. 'zx'= 35
1D	-17067	3487	43757	3	0.9027	0.9997	1.0037	--	--	0.02	--	0.36	Snell. 'zx'= 35
1I	-13089	-1121	46063	3	0.9027	0.9998	1.0028	--	--	0.02	--	0.29	Snell. 'zx'= 35
1J	-13089	-1121	43757	3	0.9027	0.9998	1.0028	--	--	0.02	--	0.28	Snell. 'zx'= 35
1K	-13089	1121	46063	3	0.9027	0.9998	1.0028	--	--	0.02	--	0.29	Snell. 'zx'= 35
1L	-13089	1121	43757	3	0.9027	0.9998	1.0028	--	--	0.02	--	0.28	Snell. 'zx'= 35
1Q	-6959	-1063	48753	3	0.9027	0.9999	1.0015	--	--	0.01	--	0.29	Snell. 'zx'= 35
1R	-6959	-1063	41067	3	0.9027	0.9999	1.0015	--	--	0.01	--	0.25	Snell. 'zx'= 35
1S	-6959	1063	48753	3	0.9027	0.9999	1.0015	--	--	0.01	--	0.29	Snell. 'zx'= 35
1T	-6959	1063	41067	3	0.9027	0.9999	1.0015	--	--	0.01	--	0.25	Snell. 'zx'= 35
7	-1570	10	106400	3	0.9027	1.0000	1.0003	--	--	0.00	--	0.54	Snell. 'zx'= 35
20	-9148	17	69320	3	0.9027	1.0017	1.0020	--	--	0.01	--	0.37	Snell. 'zx'= 35

ASTA NUM. 6 NI 10 NF 16 Lungh. 55.0 cm SEZ. 1 Ps HEB 600

categoria: p.p. y Permanente Congresso Neve qy tot.
 qy medio: 211.95 1443.00 975.00 195.00 2824.95 kg/m

Sollecitazioni di calcolo e di verifica

Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	cm	kg			kg*m							
1A	0	-11886	-4244	2426	0	631	40978	3	0.02	0.01	0.24	
1B	0	-11886	-3998	2426	0	631	38942	3	0.02	0.01	0.23	
1C	0	-11886	-4244	-2426	0	-631	40978	3	0.02	0.01	0.24	
1D	0	-11886	-3998	-2426	0	-631	38942	3	0.02	0.01	0.23	
1E	0	11886	-4244	2426	0	631	40978	1	0.02	0.01	0.19	
1F	0	11886	-3998	2426	0	631	38942	1	0.02	0.01	0.18	
1G	0	11886	-4244	-2426	0	-631	40978	1	0.02	0.01	0.19	
1H	0	11886	-3998	-2426	0	-631	38942	1	0.02	0.01	0.18	
1I	0	-16451	-4244	800	0	230	40978	3	0.02	0.02	0.23	
1J	0	-16451	-3998	800	0	230	38942	3	0.02	0.02	0.22	
1K	0	-16451	-4244	-800	0	-230	40978	3	0.02	0.02	0.23	
1L	0	-16451	-3998	-800	0	-230	38942	3	0.02	0.02	0.22	
1M	0	16451	-4244	800	0	230	40978	1	0.02	0.02	0.19	
1N	0	16451	-3998	800	0	230	38942	1	0.02	0.02	0.18	
1O	0	16451	-4244	-800	0	-230	40978	1	0.02	0.02	0.19	
1P	0	16451	-3998	-800	0	-230	38942	1	0.02	0.02	0.18	
1Q	0	-6539	-4531	744	0	199	43353	3	0.02	0.01	0.23	
1R	0	-6539	-3711	744	0	199	36567	3	0.02	0.01	0.20	
1S	0	-6539	-4531	-744	0	-199	43353	3	0.02	0.01	0.23	
1T	0	-6539	-3711	-744	0	-199	36567	3	0.02	0.01	0.20	
1U	0	6539	-4531	744	0	199	43353	1	0.02	0.01	0.20	
1V	0	6539	-3711	744	0	199	36567	1	0.02	0.01	0.17	
1W	0	6539	-4531	-744	0	-199	43353	1	0.02	0.01	0.20	
1X	0	6539	-3711	-744	0	-199	36567	1	0.02	0.01	0.17	
2	0	1325	-4121	985	0	183	39960	1	0.02	0.00	0.18	
3	0	795	-6778	591	0	110	65850	1	0.03	0.00	0.30	
4	0	795	-9640	591	0	110	93850	1	0.04	0.00	0.42	
5	0	1325	-7494	985	0	183	72850	1	0.03	0.00	0.33	
7	0	-7668	-9039	-7	0	8	91810	3	0.04	0.01	0.48	
20	0	-10200	-6494	-15	0	6	60960	3	0.03	0.01	0.32	
22	0	6803	-288	10	0	-4	1408	1	0.00	0.01	0.01	
1A	28	-11886	-4699	2426	0	-67	39747	3	0.02	0.01	0.22	
1B	28	-11886	-4453	2426	0	-67	37778	3	0.02	0.01	0.21	
1C	28	-11886	-4699	-2426	0	67	39747	3	0.02	0.01	0.22	
1D	28	-11886	-4453	-2426	0	67	37778	3	0.02	0.01	0.21	
1E	28	11886	-4699	2426	0	-67	39747	1	0.02	0.01	0.18	
1F	28	11886	-4453	2426	0	-67	37778	1	0.02	0.01	0.17	
1G	28	11886	-4699	-2426	0	67	39747	1	0.02	0.01	0.18	
1H	28	11886	-4453	-2426	0	67	37778	1	0.02	0.01	0.17	
1I	28	-16451	-4699	800	0	-15	39747	3	0.02	0.02	0.22	
1J	28	-16451	-4453	800	0	-15	37778	3	0.02	0.02	0.21	
1K	28	-16451	-4699	-800	0	15	39747	3	0.02	0.02	0.22	
1L	28	-16451	-4453	-800	0	15	37778	3	0.02	0.02	0.21	
1M	28	16451	-4699	800	0	-15	39747	1	0.02	0.02	0.18	
1N	28	16451	-4453	800	0	-15	37778	1	0.02	0.02	0.17	
1O	28	16451	-4699	-800	0	15	39747	1	0.02	0.02	0.18	
1P	28	16451	-4453	-800	0	15	37778	1	0.02	0.02	0.17	
1Q	28	-6539	-4986	744	0	-19	42045	3	0.02	0.01	0.22	
1R	28	-6539	-4166	744	0	-19	35480	3	0.02	0.01	0.19	
1S	28	-6539	-4986	-744	0	19	42045	3	0.02	0.01	0.22	
1T	28	-6539	-4166	-744	0	19	35480	3	0.02	0.01	0.19	
1U	28	6539	-4986	744	0	-19	42045	1	0.02	0.01	0.19	
1V	28	6539	-4166	744	0	-19	35480	1	0.02	0.01	0.16	
1W	28	6539	-4986	-744	0	19	42045	1	0.02	0.01	0.19	
1X	28	6539	-4166	-744	0	19	35480	1	0.02	0.01	0.16	
2	28	1325	-4576	985	0	-88	38763	1	0.02	0.00	0.18	
3	28	795	-7529	591	0	-53	63883	1	0.03	0.00	0.29	
4	28	795	-10715	591	0	-53	91048	1	0.05	0.00	0.41	
5	28	1325	-8326	985	0	-88	70674	1	0.04	0.00	0.32	
7	28	-7668	-9710	-7	0	10	89232	3	0.04	0.01	0.46	
20	28	-10200	-7165	-15	0	10	59082	3	0.03	0.01	0.31	
22	28	6803	-288	10	0	-7	1328	1	0.00	0.01	0.01	
1A	55	-11886	-5154	2426	0	-765	38392	3	0.02	0.01	0.23	
1B	55	-11886	-4908	2426	0	-765	36488	3	0.02	0.01	0.22	
1C	55	-11886	-5154	-2426	0	765	38392	3	0.02	0.01	0.23	
1D	55	-11886	-4908	-2426	0	765	36488	3	0.02	0.01	0.22	
1E	55	11886	-5154	2426	0	-765	38392	1	0.02	0.01	0.17	
1F	55	11886	-4908	2426	0	-765	36488	1	0.02	0.01	0.16	
1G	55	11886	-5154	-2426	0	765	38392	1	0.02	0.01	0.17	
1H	55	11886	-4908	-2426	0	765	36488	1	0.02	0.01	0.16	
1I	55	-16451	-5154	800	0	-259	38392	3	0.02	0.02	0.22	
1J	55	-16451	-4908	800	0	-259	36488	3	0.02	0.02	0.21	
1K	55	-16451	-5154	-800	0	259	38392	3	0.02	0.02	0.22	
1L	55	-16451	-4908	-800	0	259	36488	3	0.02	0.02	0.21	
1M	55	16451	-5154	800	0	-259	38392	1	0.02	0.02	0.17	
1N	55	16451	-4908	800	0	-259	36488	1	0.02	0.02	0.16	
1O	55	16451	-5154	-800	0	259	38392	1	0.02	0.02	0.17	
1P	55	16451	-4908	-800	0	259	36488	1	0.02	0.02	0.16	
1Q	55	-6539	-5441	744	0	-236	40612	3	0.02	0.01	0.22	
1R	55	-6539	-4621	744	0	-236	34268	3	0.02	0.01	0.19	
1S	55	-6539	-5441	-744	0	236	40612	3	0.02	0.01	0.22	
1T	55	-6539	-4621	-744	0	236	34268	3	0.02	0.01	0.19	
1U	55	6539	-5441	744	0	-236	40612	1	0.02	0.01	0.18	
1V	55	6539	-4621	744	0	-236	34268	1	0.02	0.01	0.15	
1W	55	6539	-5441	-744	0	236	40612	1	0.02	0.01	0.18	
1X	55	6539	-4621	-744	0	236	34268	1	0.02	0.01	0.15	
2	55	1325	-5031	985	0	-359	37440	1	0.02	0.00	0.17	
3	55	795	-8281	591	0	-215	61710	1	0.04	0.00	0.28	
4	55	795	-11790	591	0	-215	87950	1	0.05	0.00	0.40	
5	55	1325	-9158	985	0	-359	68270	1	0.04	0.00	0.31	
7	55	-7668	-10380	-7	0	12	86470	3	0.05	0.01	0.45	
20	55	-10200	-7836	-15	0	14	57020	3	0.04	0.01	0.30	
22	55	6803	-288	10	0	-10	1249	1	0.00	0.01	0.01	

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	$\gamma_{min.}$	ky	kz	kLT	γ_{LT}	I.S.n.	I.S.m.	I.S.	Nota
	kg	kg*m											
1A	-11886	-765	40978	3	1.0000	0.9991	1.0006	--	--	0.01	--	0.25	Snell. 'zx'= 8
1B	-11886	-765	38942	3	1.0000	0.9991	1.0006	--	--	0.01	--	0.24	Snell. 'zx'= 8
1C	-11886	765	40978	3	1.0000	0.9991	1.0006	--	--	0.01	--	0.25	Snell. 'zx'= 8
1D	-11886	765	38942	3	1.0000	0.9991	1.0006	--	--	0.01	--	0.24	Snell. 'zx'= 8
1I	-16451	-259	40978	3	1.0000	0.9985	1.0008	--	--	0.02	--	0.23	Snell. 'zx'= 8
1J	-16451	-259	38942	3	1.0000	0.9985	1.0008	--	--	0.02	--	0.22	Snell. 'zx'= 8
1K	-16451	259	40978	3	1.0000	0.9985	1.0008	--	--	0.02	--	0.23	Snell. 'zx'= 8
1L	-16451	259	38942	3	1.0000	0.9985	1.0008	--	--	0.02	--	0.22	Snell. 'zx'= 8
1Q	-6539	-236	43353	3	1.0000	0.9995	1.0003	--	--	0.01	--	0.24	Snell. 'zx'= 8
1R	-6539	-236	36567	3	1.0000	0.9995	1.0003	--	--	0.01	--	0.20	Snell. 'zx'= 8
1S	-6539	236	43353	3	1.0000	0.9995	1.0003	--	--	0.01	--	0.24	Snell. 'zx'= 8
1T	-6539	236	36567	3	1.0000	0.9995	1.0003	--	--	0.01	--	0.20	Snell. 'zx'= 8
7	-7668	12	91810	3	1.0000	1.0011	1.0004	--	--	0.01	--	0.48	Snell. 'zx'= 8
20	-10200	14	60960	3	1.0000	1.0011	1.0005	--	--	0.01	--	0.32	Snell. 'zx'= 8

ASTA NUM. 7 NI 11 NF 2 Lungh. 50.0 cm SEZ. 1 Ps HEB 600

categoria: p.p. y Permanente Congresso Neve qy tot.
 qy medio: 211.95 1443.00 975.00 195.00 2824.95 kg/m

Sollecitazioni di calcolo e di verifica

Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	cm	kg			kg*m							
1A	0	-62	-2	1418	0	0	0	3	0.00	0.00	0.00	
1B	0	-62	2	1418	0	0	-0	3	0.00	0.00	0.00	
1C	0	-62	-2	-1418	0	-0	0	3	0.00	0.00	0.00	
1D	0	-62	2	-1418	0	-0	-0	3	0.00	0.00	0.00	
1E	0	62	-2	1418	0	0	0	--	0.00	0.00	0.00	
1F	0	62	2	1418	0	0	-0	--	0.00	0.00	0.00	
1G	0	62	-2	-1418	0	-0	0	--	0.00	0.00	0.00	
1H	0	62	2	-1418	0	-0	-0	--	0.00	0.00	0.00	
1I	0	-175	-2	800	0	0	0	3	0.00	0.00	0.00	
1J	0	-175	2	800	0	0	-0	3	0.00	0.00	0.00	
1K	0	-175	-2	-800	0	-0	0	3	0.00	0.00	0.00	
1L	0	-175	2	-800	0	-0	-0	3	0.00	0.00	0.00	
1M	0	175	-2	800	0	0	0	--	0.00	0.00	0.00	
1N	0	175	2	800	0	0	-0	--	0.00	0.00	0.00	
1O	0	175	-2	-800	0	-0	0	--	0.00	0.00	0.00	
1P	0	175	2	-800	0	-0	-0	--	0.00	0.00	0.00	
1Q	0	-55	-6	512	0	0	0	3	0.00	0.00	0.00	
1R	0	-55	6	512	0	0	-0	3	0.00	0.00	0.00	
1S	0	-55	-6	-512	0	-0	0	3	0.00	0.00	0.00	
1T	0	-55	6	-512	0	-0	-0	3	0.00	0.00	0.00	
1U	0	55	-6	512	0	0	0	--	0.00	0.00	0.00	
1V	0	55	6	512	0	0	-0	--	0.00	0.00	0.00	
1W	0	55	-6	-512	0	-0	0	--	0.00	0.00	0.00	
1X	0	55	6	-512	0	-0	-0	--	0.00	0.00	0.00	
2	0	0	0	-296	0	0	0	--	0.00	0.00	0.00	
3	0	0	0	-178	0	0	0	--	0.00	0.00	0.00	
4	0	0	0	-178	0	0	0	--	0.00	0.00	0.00	
5	0	0	0	-296	0	0	0	--	0.00	0.00	0.00	
7	0	-0	0	86	0	-0	-35	1	0.00	0.00	0.00	
20	0	-5077	-8462	94	0	0	-4	3	0.04	0.01	0.01	
22	0	3385	-5641	-63	0	0	-3	1	0.03	0.00	0.00	
1A	25	-62	-416	1418	0	-355	-51	3	0.00	0.00	0.01	
1B	25	-62	-412	1418	0	-355	-52	3	0.00	0.00	0.01	
1C	25	-62	-416	-1418	0	355	-51	3	0.00	0.00	0.01	
1D	25	-62	-412	-1418	0	355	-52	3	0.00	0.00	0.01	
1E	25	62	-416	1418	0	-355	-51	1	0.00	0.00	0.01	
1F	25	62	-412	1418	0	-355	-52	1	0.00	0.00	0.01	
1G	25	62	-416	-1418	0	355	-51	1	0.00	0.00	0.01	
1H	25	62	-412	-1418	0	355	-52	1	0.00	0.00	0.01	
1I	25	-175	-416	800	0	-200	-51	3	0.00	0.00	0.01	
1J	25	-175	-412	800	0	-200	-52	3	0.00	0.00	0.01	
1K	25	-175	-416	-800	0	200	-51	3	0.00	0.00	0.01	
1L	25	-175	-412	-800	0	200	-52	3	0.00	0.00	0.01	
1M	25	175	-416	800	0	-200	-51	1	0.00	0.00	0.00	
1N	25	175	-412	800	0	-200	-52	1	0.00	0.00	0.00	
1O	25	175	-416	-800	0	200	-51	1	0.00	0.00	0.00	
1P	25	175	-412	-800	0	200	-52	1	0.00	0.00	0.00	
1Q	25	-55	-420	512	0	-128	-50	3	0.00	0.00	0.00	
1R	25	-55	-408	512	0	-128	-53	3	0.00	0.00	0.00	
1S	25	-55	-420	-512	0	128	-50	3	0.00	0.00	0.00	
1T	25	-55	-408	-512	0	128	-53	3	0.00	0.00	0.00	
1U	25	55	-420	512	0	-128	-50	1	0.00	0.00	0.00	
1V	25	55	-408	512	0	-128	-53	1	0.00	0.00	0.00	
1W	25	55	-420	-512	0	128	-50	1	0.00	0.00	0.00	
1X	25	55	-408	-512	0	128	-53	1	0.00	0.00	0.00	
2	25	0	-414	-296	0	74	-52	1	0.00	0.00	0.00	
3	25	0	-683	-178	0	44	-85	1	0.00	0.00	0.00	
4	25	0	-976	-178	0	44	-122	1	0.00	0.00	0.00	
5	25	0	-756	-296	0	74	-95	1	0.00	0.00	0.00	
7	25	-0	-610	86	0	-22	-111	1	0.00	0.00	0.00	
20	25	-5077	-9072	94	0	-24	-2196	3	0.04	0.01	0.02	
22	25	3385	-5641	-63	0	16	-1413	1	0.03	0.00	0.01	

1A	50	-62	-829	1418	0	-709	-206	3	0.00	0.00	0.02		
1B	50	-62	-826	1418	0	-709	-208	3	0.00	0.00	0.02		
1C	50	-62	-829	-1418	0	709	-206	3	0.00	0.00	0.02		
1D	50	-62	-826	-1418	0	709	-208	3	0.00	0.00	0.02		
1E	50	62	-829	1418	0	-709	-206	1	0.00	0.00	0.01		
1F	50	62	-826	1418	0	-709	-208	1	0.00	0.00	0.01		
1G	50	62	-829	-1418	0	709	-206	1	0.00	0.00	0.01		
1H	50	62	-826	-1418	0	709	-208	1	0.00	0.00	0.01		
1I	50	-175	-829	800	0	-400	-206	3	0.00	0.00	0.01		
1J	50	-175	-826	800	0	-400	-208	3	0.00	0.00	0.01		
1K	50	-175	-829	-800	0	400	-206	3	0.00	0.00	0.01		
1L	50	-175	-826	-800	0	400	-208	3	0.00	0.00	0.01		
1M	50	175	-829	800	0	-400	-206	1	0.00	0.00	0.01		
1N	50	175	-826	800	0	-400	-208	1	0.00	0.00	0.01		
1O	50	175	-829	-800	0	400	-206	1	0.00	0.00	0.01		
1P	50	175	-826	-800	0	400	-208	1	0.00	0.00	0.01		
1Q	50	-55	-833	512	0	-256	-204	3	0.00	0.00	0.01		
1R	50	-55	-822	512	0	-256	-210	3	0.00	0.00	0.01		
1S	50	-55	-833	-512	0	256	-204	3	0.00	0.00	0.01		
1T	50	-55	-822	-512	0	256	-210	3	0.00	0.00	0.01		
1U	50	55	-833	512	0	-256	-204	1	0.00	0.00	0.01		
1V	50	55	-822	512	0	-256	-210	1	0.00	0.00	0.01		
1W	50	55	-833	-512	0	256	-204	1	0.00	0.00	0.01		
1X	50	55	-822	-512	0	256	-210	1	0.00	0.00	0.01		
2	50	0	-828	-296	0	148	-207	1	0.00	0.00	0.00		
3	50	0	-1366	-178	0	89	-342	1	0.01	0.00	0.00		
4	50	0	-1951	-178	0	89	-488	1	0.01	0.00	0.00		
5	50	0	-1513	-296	0	148	-378	1	0.01	0.00	0.00		
7	50	-0	-1220	86	0	-43	-340	1	0.01	0.00	0.00		
20	50	-5077	-9682	94	0	-47	-4540	3	0.04	0.01	0.03		
22	50	3385	-5641	-63	0	31	-2823	1	0.03	0.00	0.01		

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	$\chi_{min.}$	ky	kz	kLT	χ_{LT}	I.S.n.	I.S.m.	I.S.	Nota
--	kg	kg*m											
1A	-62	-709	-206	3	1.0000	1.0000	1.0000	--	--	0.00	--	0.02	Snell. 'zx'= 7
1B	-62	-709	-208	3	1.0000	1.0000	1.0000	--	--	0.00	--	0.02	Snell. 'zx'= 7
1C	-62	709	-206	3	1.0000	1.0000	1.0000	--	--	0.00	--	0.02	Snell. 'zx'= 7
1D	-62	709	-208	3	1.0000	1.0000	1.0000	--	--	0.00	--	0.02	Snell. 'zx'= 7
1I	-175	-400	-206	3	1.0000	1.0000	1.0000	--	--	0.00	--	0.01	Snell. 'zx'= 7
1J	-175	-400	-208	3	1.0000	1.0000	1.0000	--	--	0.00	--	0.01	Snell. 'zx'= 7
1K	-175	400	-206	3	1.0000	1.0000	1.0000	--	--	0.00	--	0.01	Snell. 'zx'= 7
1L	-175	400	-208	3	1.0000	1.0000	1.0000	--	--	0.00	--	0.01	Snell. 'zx'= 7
1Q	-55	-256	-204	3	1.0000	1.0000	1.0000	--	--	0.00	--	0.01	Snell. 'zx'= 7
1R	-55	-256	-210	3	1.0000	1.0000	1.0000	--	--	0.00	--	0.01	Snell. 'zx'= 7
1S	-55	256	-204	3	1.0000	1.0000	1.0000	--	--	0.00	--	0.01	Snell. 'zx'= 7
1T	-55	256	-210	3	1.0000	1.0000	1.0000	--	--	0.00	--	0.01	Snell. 'zx'= 7
7	-0	-43	-340	1	1.0000	1.0000	1.0000	--	--	--	--	--	Snell. 'zx'= 7
20	-5077	-47	-4540	3	1.0000	1.0002	1.0001	--	--	0.01	--	0.03	Snell. 'zx'= 7

ASTA NUM. 8 NI 12 NF 1 Lungh. 50.0 cm SEZ. 1 Ps HEB 600

categoria: p.p. y Permanente Congresso Neve qy tot.
qy medio: 211.95 1443.00 975.00 195.00 2824.95 kg/m

Sollecitazioni di calcolo e di verifica

Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
--	cm	kg			kg*m							
1A	0	-77	-2	1439	0	0	0	3	0.00	0.00	0.00	
1B	0	-77	2	1439	0	0	-0	3	0.00	0.00	0.00	
1C	0	-77	-2	-1439	0	-0	0	3	0.00	0.00	0.00	
1D	0	-77	2	-1439	0	-0	-0	3	0.00	0.00	0.00	
1E	0	77	-2	1439	0	0	0	--	0.00	0.00	0.00	
1F	0	77	2	1439	0	0	-0	--	0.00	0.00	0.00	
1G	0	77	-2	-1439	0	-0	0	--	0.00	0.00	0.00	
1H	0	77	2	-1439	0	-0	-0	--	0.00	0.00	0.00	
1I	0	-239	-2	794	0	0	0	3	0.00	0.00	0.00	
1J	0	-239	2	794	0	0	-0	3	0.00	0.00	0.00	
1K	0	-239	-2	-794	0	-0	0	3	0.00	0.00	0.00	
1L	0	-239	2	-794	0	-0	-0	3	0.00	0.00	0.00	
1M	0	239	-2	794	0	0	0	--	0.00	0.00	0.00	
1N	0	239	2	794	0	0	-0	--	0.00	0.00	0.00	
1O	0	239	-2	-794	0	-0	0	--	0.00	0.00	0.00	
1P	0	239	2	-794	0	-0	-0	--	0.00	0.00	0.00	
1Q	0	-73	-6	515	0	0	0	3	0.00	0.00	0.00	
1R	0	-73	6	515	0	0	-0	3	0.00	0.00	0.00	
1S	0	-73	-6	-515	0	-0	0	3	0.00	0.00	0.00	
1T	0	-73	6	-515	0	-0	-0	3	0.00	0.00	0.00	
1U	0	73	-6	515	0	0	0	--	0.00	0.00	0.00	
1V	0	73	6	515	0	0	-0	--	0.00	0.00	0.00	
1W	0	73	-6	-515	0	-0	0	--	0.00	0.00	0.00	
1X	0	73	6	-515	0	-0	-0	--	0.00	0.00	0.00	
2	0	0	-0	296	0	0	0	--	0.00	0.00	0.00	
3	0	0	-0	178	0	0	0	--	0.00	0.00	0.00	
4	0	0	-0	178	0	0	0	--	0.00	0.00	0.00	
5	0	0	-0	296	0	0	0	--	0.00	0.00	0.00	
7	0	0	-0	-86	0	0	35	1	0.00	0.00	0.00	
20	0	-2123	-3538	-94	0	0	4	3	0.02	0.00	0.00	
22	0	1415	-2359	63	0	0	3	1	0.01	0.00	0.00	
1A	25	-77	-416	1439	0	-360	-51	3	0.00	0.00	0.01	

1B	25	-77	-412	1439	0	-360	-52	3	0.00	0.00	0.01	
1C	25	-77	-416	-1439	0	360	-51	3	0.00	0.00	0.01	
1D	25	-77	-412	-1439	0	360	-52	3	0.00	0.00	0.01	
1E	25	77	-416	1439	0	-360	-51	1	0.00	0.00	0.01	
1F	25	77	-412	1439	0	-360	-52	1	0.00	0.00	0.01	
1G	25	77	-416	-1439	0	360	-51	1	0.00	0.00	0.01	
1H	25	77	-412	-1439	0	360	-52	1	0.00	0.00	0.01	
1I	25	-239	-416	794	0	-198	-51	3	0.00	0.00	0.01	
1J	25	-239	-412	794	0	-198	-52	3	0.00	0.00	0.01	
1K	25	-239	-416	-794	0	198	-51	3	0.00	0.00	0.01	
1L	25	-239	-412	-794	0	198	-52	3	0.00	0.00	0.01	
1M	25	239	-416	794	0	-198	-51	1	0.00	0.00	0.00	
1N	25	239	-412	794	0	-198	-52	1	0.00	0.00	0.00	
1O	25	239	-416	-794	0	198	-51	1	0.00	0.00	0.00	
1P	25	239	-412	-794	0	198	-52	1	0.00	0.00	0.00	
1Q	25	-73	-420	515	0	-129	-50	3	0.00	0.00	0.00	
1R	25	-73	-408	515	0	-129	-53	3	0.00	0.00	0.00	
1S	25	-73	-420	-515	0	129	-50	3	0.00	0.00	0.00	
1T	25	-73	-408	-515	0	129	-53	3	0.00	0.00	0.00	
1U	25	73	-420	515	0	-129	-50	1	0.00	0.00	0.00	
1V	25	73	-408	515	0	-129	-53	1	0.00	0.00	0.00	
1W	25	73	-420	-515	0	129	-50	1	0.00	0.00	0.00	
1X	25	73	-408	-515	0	129	-53	1	0.00	0.00	0.00	
2	25	0	-414	197	0	-62	-52	1	0.00	0.00	0.00	
3	25	0	-683	118	0	-37	-85	1	0.00	0.00	0.00	
4	25	0	-976	118	0	-37	-122	1	0.00	0.00	0.00	
5	25	0	-756	197	0	-62	-95	1	0.00	0.00	0.00	
7	25	0	-610	-86	0	22	-42	1	0.00	0.00	0.00	
20	25	-2123	-4148	-94	0	24	-957	3	0.02	0.00	0.01	
22	25	1415	-2359	63	0	-16	-587	1	0.01	0.00	0.00	
1A	50	-77	-829	1439	0	-720	-206	3	0.00	0.00	0.02	
1B	50	-77	-826	1439	0	-720	-208	3	0.00	0.00	0.02	
1C	50	-77	-829	-1439	0	720	-206	3	0.00	0.00	0.02	
1D	50	-77	-826	-1439	0	720	-208	3	0.00	0.00	0.02	
1E	50	77	-829	1439	0	-720	-206	1	0.00	0.00	0.02	
1F	50	77	-826	1439	0	-720	-208	1	0.00	0.00	0.02	
1G	50	77	-829	-1439	0	720	-206	1	0.00	0.00	0.02	
1H	50	77	-826	-1439	0	720	-208	1	0.00	0.00	0.02	
1I	50	-239	-829	794	0	-397	-206	3	0.00	0.00	0.01	
1J	50	-239	-826	794	0	-397	-208	3	0.00	0.00	0.01	
1K	50	-239	-829	-794	0	397	-206	3	0.00	0.00	0.01	
1L	50	-239	-826	-794	0	397	-208	3	0.00	0.00	0.01	
1M	50	239	-829	794	0	-397	-206	1	0.00	0.00	0.01	
1N	50	239	-826	794	0	-397	-208	1	0.00	0.00	0.01	
1O	50	239	-829	-794	0	397	-206	1	0.00	0.00	0.01	
1P	50	239	-826	-794	0	397	-208	1	0.00	0.00	0.01	
1Q	50	-73	-833	515	0	-258	-204	3	0.00	0.00	0.01	
1R	50	-73	-822	515	0	-258	-210	3	0.00	0.00	0.01	
1S	50	-73	-833	-515	0	258	-204	3	0.00	0.00	0.01	
1T	50	-73	-822	-515	0	258	-210	3	0.00	0.00	0.01	
1U	50	73	-833	515	0	-258	-204	1	0.00	0.00	0.01	
1V	50	73	-822	515	0	-258	-210	1	0.00	0.00	0.01	
1W	50	73	-833	-515	0	258	-204	1	0.00	0.00	0.01	
1X	50	73	-822	-515	0	258	-210	1	0.00	0.00	0.01	
3	50	0	-828	98	0	-99	-207	1	0.00	0.00	0.00	
4	50	0	-1366	59	0	-59	-342	1	0.01	0.00	0.00	
5	50	0	-1951	59	0	-59	-488	1	0.01	0.00	0.00	
7	50	0	-1513	98	0	-99	-378	1	0.01	0.00	0.00	
20	50	0	-1220	-86	0	43	-270	1	0.01	0.00	0.00	
20	50	-2123	-4758	-94	0	47	-2070	3	0.02	0.00	0.01	
22	50	1415	-2359	63	0	-31	-1177	1	0.01	0.00	0.01	

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	$\gamma_{min.}$	ky	kz	kLT	χ_{LT}	I.S.n.	I.S.m.	I.S.	Nota
	kg	kg*m											
1A	-77	-720	-206	3	1.0000	1.0000	1.0000	--	--	0.00	--	0.02	Snell. 'zx'= 7
1B	-77	-720	-208	3	1.0000	1.0000	1.0000	--	--	0.00	--	0.02	Snell. 'zx'= 7
1C	-77	720	-206	3	1.0000	1.0000	1.0000	--	--	0.00	--	0.02	Snell. 'zx'= 7
1D	-77	720	-208	3	1.0000	1.0000	1.0000	--	--	0.00	--	0.02	Snell. 'zx'= 7
1I	-239	-397	-206	3	1.0000	1.0000	1.0000	--	--	0.00	--	0.01	Snell. 'zx'= 7
1J	-239	-397	-208	3	1.0000	1.0000	1.0000	--	--	0.00	--	0.01	Snell. 'zx'= 7
1K	-239	397	-206	3	1.0000	1.0000	1.0000	--	--	0.00	--	0.01	Snell. 'zx'= 7
1L	-239	397	-208	3	1.0000	1.0000	1.0000	--	--	0.00	--	0.01	Snell. 'zx'= 7
1Q	-73	-258	-204	3	1.0000	1.0000	1.0000	--	--	0.00	--	0.01	Snell. 'zx'= 7
1R	-73	-258	-210	3	1.0000	1.0000	1.0000	--	--	0.00	--	0.01	Snell. 'zx'= 7
1S	-73	258	-204	3	1.0000	1.0000	1.0000	--	--	0.00	--	0.01	Snell. 'zx'= 7
1T	-73	258	-210	3	1.0000	1.0000	1.0000	--	--	0.00	--	0.01	Snell. 'zx'= 7
20	-2123	47	-2070	3	1.0000	1.0001	1.0000	--	--	0.00	--	0.01	Snell. 'zx'= 7

ASTA NUM. 9 NI 6 NF 14 Lungh. 35.0 cm SEZ. 1 Ps HEB 600

categoria: p.p. y Permanente Congresso Neve qy tot.
qy medio: 211.95 1443.00 975.00 195.00 2824.95 kg/m

Sollecitazioni di calcolo e di verifica Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	cm	kg			kg*m							
1A	0	-57	578	121	0	42	-101	3	0.00	0.00	0.00	
1B	0	-57	580	121	0	42	-102	3	0.00	0.00	0.00	
1C	0	-57	578	-121	0	-42	-101	3	0.00	0.00	0.00	

1D	0	-57	580	-121	0	-42	-102	3	0.00	0.00	0.00
1E	0	57	578	121	0	42	-101	1	0.00	0.00	0.00
1F	0	57	580	121	0	42	-102	1	0.00	0.00	0.00
1G	0	57	578	-121	0	-42	-101	1	0.00	0.00	0.00
1H	0	57	580	-121	0	-42	-102	1	0.00	0.00	0.00
1I	0	-168	578	45	0	16	-101	3	0.00	0.00	0.00
1J	0	-168	580	45	0	16	-102	3	0.00	0.00	0.00
1K	0	-168	578	-45	0	-16	-101	3	0.00	0.00	0.00
1L	0	-168	580	-45	0	-16	-102	3	0.00	0.00	0.00
1M	0	168	578	45	0	16	-101	1	0.00	0.00	0.00
1N	0	168	580	45	0	16	-102	1	0.00	0.00	0.00
1O	0	168	578	-45	0	-16	-101	1	0.00	0.00	0.00
1P	0	168	580	-45	0	-16	-102	1	0.00	0.00	0.00
1Q	0	-52	577	38	0	13	-101	3	0.00	0.00	0.00
1R	0	-52	582	38	0	13	-102	3	0.00	0.00	0.00
1S	0	-52	577	-38	0	-13	-101	3	0.00	0.00	0.00
1T	0	-52	582	-38	0	-13	-102	3	0.00	0.00	0.00
1U	0	52	577	38	0	13	-101	1	0.00	0.00	0.00
1V	0	52	582	38	0	13	-102	1	0.00	0.00	0.00
1W	0	52	577	-38	0	-13	-101	1	0.00	0.00	0.00
1X	0	52	582	-38	0	-13	-102	1	0.00	0.00	0.00
2	0	-0	579	139	0	24	-101	1	0.00	0.00	0.00
3	0	-0	956	83	0	15	-167	1	0.00	0.00	0.00
4	0	-0	1366	83	0	15	-239	1	0.01	0.00	0.00
5	0	-0	1059	139	0	24	-185	1	0.00	0.00	0.00
7	0	-0	854	-0	0	0	-150	1	0.00	0.00	0.00
20	0	0	854	-0	0	0	-150	1	0.00	0.00	0.00
22	0	0	0	-0	0	0	0	--	0.00	0.00	0.00
1A	18	-57	289	121	0	21	-25	3	0.00	0.00	0.00
1B	18	-57	290	121	0	21	-25	3	0.00	0.00	0.00
1C	18	-57	289	-121	0	-21	-25	3	0.00	0.00	0.00
1D	18	-57	290	-121	0	-21	-25	3	0.00	0.00	0.00
1E	18	57	289	121	0	21	-25	1	0.00	0.00	0.00
1F	18	57	290	121	0	21	-25	1	0.00	0.00	0.00
1G	18	57	289	-121	0	-21	-25	1	0.00	0.00	0.00
1H	18	57	290	-121	0	-21	-25	1	0.00	0.00	0.00
1I	18	-168	289	45	0	8	-25	3	0.00	0.00	0.00
1J	18	-168	290	45	0	8	-25	3	0.00	0.00	0.00
1K	18	-168	289	-45	0	-8	-25	3	0.00	0.00	0.00
1L	18	-168	290	-45	0	-8	-25	3	0.00	0.00	0.00
1M	18	168	289	45	0	8	-25	1	0.00	0.00	0.00
1N	18	168	290	45	0	8	-25	1	0.00	0.00	0.00
1O	18	168	289	-45	0	-8	-25	1	0.00	0.00	0.00
1P	18	168	290	-45	0	-8	-25	1	0.00	0.00	0.00
1Q	18	-52	287	38	0	7	-25	3	0.00	0.00	0.00
1R	18	-52	292	38	0	7	-26	3	0.00	0.00	0.00
1S	18	-52	287	-38	0	-7	-25	3	0.00	0.00	0.00
1T	18	-52	292	-38	0	-7	-26	3	0.00	0.00	0.00
1U	18	52	287	38	0	7	-25	1	0.00	0.00	0.00
1V	18	52	292	38	0	7	-26	1	0.00	0.00	0.00
1W	18	52	287	-38	0	-7	-25	1	0.00	0.00	0.00
1X	18	52	292	-38	0	-7	-26	1	0.00	0.00	0.00
2	18	-0	290	69	0	6	-25	1	0.00	0.00	0.00
3	18	-0	478	42	0	4	-42	1	0.00	0.00	0.00
4	18	-0	683	42	0	4	-60	1	0.00	0.00	0.00
5	18	-0	530	69	0	6	-46	1	0.00	0.00	0.00
7	18	-0	427	-0	0	0	-37	1	0.00	0.00	0.00
20	18	0	427	-0	0	0	-37	1	0.00	0.00	0.00
22	18	0	0	-0	0	0	0	--	0.00	0.00	0.00
1A	35	-57	-1	121	0	0	0	3	0.00	0.00	0.00
1B	35	-57	1	121	0	0	0	3	0.00	0.00	0.00
1C	35	-57	-1	-121	0	0	0	3	0.00	0.00	0.00
1D	35	-57	1	-121	0	0	0	3	0.00	0.00	0.00
1E	35	57	-1	121	0	0	0	--	0.00	0.00	0.00
1F	35	57	1	121	0	0	0	--	0.00	0.00	0.00
1G	35	57	-1	-121	0	0	0	--	0.00	0.00	0.00
1H	35	57	1	-121	0	0	0	--	0.00	0.00	0.00
1I	35	-168	-1	45	0	0	0	3	0.00	0.00	0.00
1J	35	-168	1	45	0	0	0	3	0.00	0.00	0.00
1K	35	-168	-1	-45	0	0	0	3	0.00	0.00	0.00
1L	35	-168	1	-45	0	0	0	3	0.00	0.00	0.00
1M	35	168	-1	45	0	0	0	--	0.00	0.00	0.00
1N	35	168	1	45	0	0	0	--	0.00	0.00	0.00
1O	35	168	-1	-45	0	0	0	--	0.00	0.00	0.00
1P	35	168	1	-45	0	0	0	--	0.00	0.00	0.00
1Q	35	-52	-2	38	0	0	0	3	0.00	0.00	0.00
1R	35	-52	2	38	0	0	0	3	0.00	0.00	0.00
1S	35	-52	-2	-38	0	0	0	3	0.00	0.00	0.00
1T	35	-52	2	-38	0	0	0	3	0.00	0.00	0.00
1U	35	52	-2	38	0	0	0	--	0.00	0.00	0.00
1V	35	52	2	38	0	0	0	--	0.00	0.00	0.00
1W	35	52	-2	-38	0	0	0	--	0.00	0.00	0.00
1X	35	52	2	-38	0	0	0	--	0.00	0.00	0.00
2	35	-0	0	0	0	0	0	--	0.00	0.00	0.00
3	35	-0	0	0	0	0	0	--	0.00	0.00	0.00
4	35	-0	-0	0	0	0	0	--	0.00	0.00	0.00
5	35	-0	0	0	0	0	0	--	0.00	0.00	0.00
7	35	-0	0	-0	0	0	0	--	0.00	0.00	0.00
20	35	0	0	-0	0	0	0	--	0.00	0.00	0.00
22	35	0	0	-0	0	0	0	--	0.00	0.00	0.00

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χ_{min}	ky	kz	kLT	χ_{LT}	I.S.n.	I.S.m.	I.S.	Nota
--	kg	kg*m											

1A	-57	42	-101	3	1.0000	1.0000	1.0000	--	--	0.00	--	0.00	Snell.	'zx'='	5
1B	-57	42	-102	3	1.0000	1.0000	1.0000	--	--	0.00	--	0.00	Snell.	'zx'='	5
1C	-57	-42	-101	3	1.0000	1.0000	1.0000	--	--	0.00	--	0.00	Snell.	'zx'='	5
1D	-57	-42	-102	3	1.0000	1.0000	1.0000	--	--	0.00	--	0.00	Snell.	'zx'='	5
1I	-168	16	-101	3	1.0000	1.0000	1.0000	--	--	0.00	--	0.00	Snell.	'zx'='	5
1J	-168	16	-102	3	1.0000	1.0000	1.0000	--	--	0.00	--	0.00	Snell.	'zx'='	5
1K	-168	-16	-101	3	1.0000	1.0000	1.0000	--	--	0.00	--	0.00	Snell.	'zx'='	5
1L	-168	-16	-102	3	1.0000	1.0000	1.0000	--	--	0.00	--	0.00	Snell.	'zx'='	5
1Q	-52	13	-101	3	1.0000	1.0000	1.0000	--	--	0.00	--	0.00	Snell.	'zx'='	5
1R	-52	13	-102	3	1.0000	1.0000	1.0000	--	--	0.00	--	0.00	Snell.	'zx'='	5
1S	-52	-13	-101	3	1.0000	1.0000	1.0000	--	--	0.00	--	0.00	Snell.	'zx'='	5
1T	-52	-13	-102	3	1.0000	1.0000	1.0000	--	--	0.00	--	0.00	Snell.	'zx'='	5
2	-0	24	-101	1	1.0000	1.0000	1.0000	--	--	--	--	--	Snell.	'zx'='	5
3	-0	15	-167	1	1.0000	1.0000	1.0000	--	--	--	--	--	Snell.	'zx'='	5
4	-0	15	-239	1	1.0000	1.0000	1.0000	--	--	--	--	--	Snell.	'zx'='	5
5	-0	24	-185	1	1.0000	1.0000	1.0000	--	--	--	--	--	Snell.	'zx'='	5
7	-0	0	-149	1	1.0000	1.0000	1.0000	--	--	--	--	--	Snell.	'zx'='	5

ASTA NUM. 10 NI 5 NF 13 Lungh. 35.0 cm SEZ. 1 Ps HEB 600

categoria: p.p. y Permanente Congresso Neve qy tot.
 qy medio: 211.95 1443.00 975.00 195.00 2824.95 kg/m
 Sollecitazioni di calcolo e di verifica

Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	cm	kg			kg*m							
1A	0	-2	578	111	0	39	-101	3	0.00	0.00	0.00	
1B	0	-2	580	111	0	39	-102	3	0.00	0.00	0.00	
1C	0	-2	578	-111	0	-39	-101	3	0.00	0.00	0.00	
1D	0	-2	580	-111	0	-39	-102	3	0.00	0.00	0.00	
1E	0	2	578	111	0	39	-101	1	0.00	0.00	0.00	
1F	0	2	580	111	0	39	-102	1	0.00	0.00	0.00	
1G	0	2	578	-111	0	-39	-101	1	0.00	0.00	0.00	
1H	0	2	580	-111	0	-39	-102	1	0.00	0.00	0.00	
1I	0	-8	578	34	0	12	-101	3	0.00	0.00	0.00	
1J	0	-8	580	34	0	12	-102	3	0.00	0.00	0.00	
1K	0	-8	578	-34	0	-12	-101	3	0.00	0.00	0.00	
1L	0	-8	580	-34	0	-12	-102	3	0.00	0.00	0.00	
1M	0	8	578	34	0	12	-101	1	0.00	0.00	0.00	
1N	0	8	580	34	0	12	-102	1	0.00	0.00	0.00	
1O	0	8	578	-34	0	-12	-101	1	0.00	0.00	0.00	
1P	0	8	580	-34	0	-12	-102	1	0.00	0.00	0.00	
1Q	0	-2	577	33	0	12	-101	3	0.00	0.00	0.00	
1R	0	-2	582	33	0	12	-102	3	0.00	0.00	0.00	
1S	0	-2	577	-33	0	-12	-101	3	0.00	0.00	0.00	
1T	0	-2	582	-33	0	-12	-102	3	0.00	0.00	0.00	
1U	0	2	577	33	0	12	-101	1	0.00	0.00	0.00	
1V	0	2	582	33	0	12	-102	1	0.00	0.00	0.00	
1W	0	2	577	-33	0	-12	-101	1	0.00	0.00	0.00	
1X	0	2	582	-33	0	-12	-102	1	0.00	0.00	0.00	
2	0	0	579	-0	0	0	-101	1	0.00	0.00	0.00	
3	0	0	956	-0	0	0	-167	1	0.00	0.00	0.00	
4	0	0	1366	-0	0	0	-239	1	0.01	0.00	0.00	
5	0	0	1059	-0	0	0	-185	1	0.00	0.00	0.00	
7	0	0	854	-0	0	0	-150	1	0.00	0.00	0.00	
20	0	0	854	0	0	0	-150	1	0.00	0.00	0.00	
22	0	-0	0	-0	0	0	0	--	0.00	0.00	0.00	
1A	18	-2	289	111	0	19	-25	3	0.00	0.00	0.00	
1B	18	-2	290	111	0	19	-25	3	0.00	0.00	0.00	
1C	18	-2	289	-111	0	-19	-25	3	0.00	0.00	0.00	
1D	18	-2	290	-111	0	-19	-25	3	0.00	0.00	0.00	
1E	18	2	289	111	0	19	-25	1	0.00	0.00	0.00	
1F	18	2	290	111	0	19	-25	1	0.00	0.00	0.00	
1G	18	2	289	-111	0	-19	-25	1	0.00	0.00	0.00	
1H	18	2	290	-111	0	-19	-25	1	0.00	0.00	0.00	
1I	18	-8	289	34	0	6	-25	3	0.00	0.00	0.00	
1J	18	-8	290	34	0	6	-25	3	0.00	0.00	0.00	
1K	18	-8	289	-34	0	-6	-25	3	0.00	0.00	0.00	
1L	18	-8	290	-34	0	-6	-25	3	0.00	0.00	0.00	
1M	18	8	289	34	0	6	-25	1	0.00	0.00	0.00	
1N	18	8	290	34	0	6	-25	1	0.00	0.00	0.00	
1O	18	8	289	-34	0	-6	-25	1	0.00	0.00	0.00	
1P	18	8	290	-34	0	-6	-25	1	0.00	0.00	0.00	
1Q	18	-2	287	33	0	6	-25	3	0.00	0.00	0.00	
1R	18	-2	292	33	0	6	-26	3	0.00	0.00	0.00	
1S	18	-2	287	-33	0	-6	-25	3	0.00	0.00	0.00	
1T	18	-2	292	-33	0	-6	-26	3	0.00	0.00	0.00	
1U	18	2	287	33	0	6	-25	1	0.00	0.00	0.00	
1V	18	2	292	33	0	6	-26	1	0.00	0.00	0.00	
1W	18	2	287	-33	0	-6	-25	1	0.00	0.00	0.00	
1X	18	2	292	-33	0	-6	-26	1	0.00	0.00	0.00	
2	18	0	290	-0	0	0	-25	1	0.00	0.00	0.00	
3	18	0	478	-0	0	0	-42	1	0.00	0.00	0.00	
4	18	0	683	-0	0	0	-60	1	0.00	0.00	0.00	
5	18	0	530	-0	0	0	-46	1	0.00	0.00	0.00	
7	18	0	427	-0	0	0	-37	1	0.00	0.00	0.00	
20	18	0	427	0	0	0	-37	1	0.00	0.00	0.00	
22	18	-0	0	-0	0	0	0	--	0.00	0.00	0.00	
1A	35	-2	-1	111	0	0	0	3	0.00	0.00	0.00	
1B	35	-2	1	111	0	0	0	3	0.00	0.00	0.00	
1C	35	-2	-1	-111	0	-0	0	3	0.00	0.00	0.00	
1D	35	-2	1	-111	0	-0	0	3	0.00	0.00	0.00	
1E	35	2	-1	111	0	0	0	--	0.00	0.00	0.00	

1F	35	2	1	111	0	0	0	--	0.00	0.00	0.00
1G	35	2	-1	-111	0	-0	0	--	0.00	0.00	0.00
1H	35	2	1	-111	0	-0	0	--	0.00	0.00	0.00
1I	35	-8	-1	34	0	0	0	3	0.00	0.00	0.00
1J	35	-8	1	34	0	0	0	3	0.00	0.00	0.00
1K	35	-8	-1	-34	0	0	0	3	0.00	0.00	0.00
1L	35	-8	1	-34	0	0	0	3	0.00	0.00	0.00
1M	35	8	-1	34	0	0	0	--	0.00	0.00	0.00
1N	35	8	1	34	0	0	0	--	0.00	0.00	0.00
1O	35	8	-1	-34	0	0	0	--	0.00	0.00	0.00
1P	35	8	1	-34	0	0	0	--	0.00	0.00	0.00
1Q	35	-2	-2	33	0	0	0	3	0.00	0.00	0.00
1R	35	-2	2	33	0	0	0	3	0.00	0.00	0.00
1S	35	-2	-2	-33	0	0	0	3	0.00	0.00	0.00
1T	35	-2	2	-33	0	0	0	3	0.00	0.00	0.00
1U	35	2	-2	33	0	0	0	--	0.00	0.00	0.00
1V	35	2	2	33	0	0	0	--	0.00	0.00	0.00
1W	35	2	-2	-33	0	0	0	--	0.00	0.00	0.00
1X	35	2	2	-33	0	0	0	--	0.00	0.00	0.00
2	35	0	0	-0	0	0	0	--	0.00	0.00	0.00
3	35	0	0	-0	0	0	0	--	0.00	0.00	0.00
4	35	0	-0	-0	0	0	0	--	0.00	0.00	0.00
5	35	0	0	-0	0	0	0	--	0.00	0.00	0.00
7	35	0	0	-0	0	0	0	--	0.00	0.00	0.00
20	35	0	0	0	0	0	0	--	0.00	0.00	0.00
22	35	-0	0	-0	0	0	0	--	0.00	0.00	0.00

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	$\gamma_{min.}$	ky	kz	kLT	χ_{LT}	I.S.n.	I.S.m.	I.S.	Nota
--	kg	kg*m											
1A	-2	39	-101	3	1.0000	1.0000	1.0000	--	--	0.00	--	0.00	Snell. 'zx'= 5
1B	-2	39	-102	3	1.0000	1.0000	1.0000	--	--	0.00	--	0.00	Snell. 'zx'= 5
1C	-2	-39	-101	3	1.0000	1.0000	1.0000	--	--	0.00	--	0.00	Snell. 'zx'= 5
1D	-2	-39	-102	3	1.0000	1.0000	1.0000	--	--	0.00	--	0.00	Snell. 'zx'= 5
1I	-8	12	-101	3	1.0000	1.0000	1.0000	--	--	0.00	--	0.00	Snell. 'zx'= 5
1J	-8	12	-102	3	1.0000	1.0000	1.0000	--	--	0.00	--	0.00	Snell. 'zx'= 5
1K	-8	-12	-101	3	1.0000	1.0000	1.0000	--	--	0.00	--	0.00	Snell. 'zx'= 5
1L	-8	-12	-102	3	1.0000	1.0000	1.0000	--	--	0.00	--	0.00	Snell. 'zx'= 5
1Q	-2	12	-101	3	1.0000	1.0000	1.0000	--	--	0.00	--	0.00	Snell. 'zx'= 5
1R	-2	12	-102	3	1.0000	1.0000	1.0000	--	--	0.00	--	0.00	Snell. 'zx'= 5
1S	-2	-12	-101	3	1.0000	1.0000	1.0000	--	--	0.00	--	0.00	Snell. 'zx'= 5
1T	-2	-12	-102	3	1.0000	1.0000	1.0000	--	--	0.00	--	0.00	Snell. 'zx'= 5
22	-0	0	0	1	1.0000	0.0000	0.0000	--	--	--	--	--	Snell. 'zx'= 5

ASTA NUM. 11 NI 15 NF 10 Lungh. 245.0 cm SEZ. 1 Ps HEB 600

categoria: p.p. y Permanente Congresso Neve qy tot.
 qy medio: 211.95 1443.00 975.00 195.00 2824.95 kg/m
 Sollecitazioni di calcolo e di verifica

Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
--	cm	kg			kg*m							
1A	0	-17313	-57	1656	0	3487	46063	3	0.00	0.02	0.37	
1B	0	-17313	72	1656	0	3487	43757	3	0.00	0.02	0.35	
1C	0	-17313	-57	-1656	0	-3487	46063	3	0.00	0.02	0.37	
1D	0	-17313	72	-1656	0	-3487	43757	3	0.00	0.02	0.35	
1E	0	17313	-57	1656	0	3487	46063	1	0.00	0.02	0.21	
1F	0	17313	72	1656	0	3487	43757	1	0.00	0.02	0.20	
1G	0	17313	-57	-1656	0	-3487	46063	1	0.00	0.02	0.21	
1H	0	17313	72	-1656	0	-3487	43757	1	0.00	0.02	0.20	
1I	0	-13788	-57	533	0	1121	46063	3	0.00	0.01	0.29	
1J	0	-13788	72	533	0	1121	43757	3	0.00	0.01	0.27	
1K	0	-13788	-57	-533	0	-1121	46063	3	0.00	0.01	0.29	
1L	0	-13788	72	-533	0	-1121	43757	3	0.00	0.01	0.27	
1M	0	13788	-57	533	0	1121	46063	1	0.00	0.01	0.21	
1N	0	13788	72	533	0	1121	43757	1	0.00	0.01	0.20	
1O	0	13788	-57	-533	0	-1121	46063	1	0.00	0.01	0.21	
1P	0	13788	72	-533	0	-1121	43757	1	0.00	0.01	0.20	
1Q	0	-7177	-208	505	0	1063	48753	3	0.00	0.01	0.29	
1R	0	-7177	222	505	0	1063	41067	3	0.00	0.01	0.25	
1S	0	-7177	-208	-505	0	-1063	48753	3	0.00	0.01	0.29	
1T	0	-7177	222	-505	0	-1063	41067	3	0.00	0.01	0.25	
1U	0	7177	-208	505	0	1063	48753	1	0.00	0.01	0.22	
1V	0	7177	222	505	0	1063	41067	1	0.00	0.01	0.19	
1W	0	7177	-208	-505	0	-1063	48753	1	0.00	0.01	0.22	
1X	0	7177	222	-505	0	-1063	41067	1	0.00	0.01	0.19	
2	0	2572	7	-238	0	-425	44910	1	0.00	0.00	0.20	
3	0	1543	12	-143	0	-255	74020	1	0.00	0.00	0.33	
4	0	1543	17	-143	0	-255	105500	1	0.00	0.00	0.48	
5	0	2572	13	-238	0	-425	81900	1	0.00	0.00	0.37	
7	0	-6647	-2965	2	0	10	106400	3	0.01	0.01	0.55	
20	0	-9148	-421	5	0	17	69320	3	0.00	0.01	0.36	
22	0	6098	-288	-3	0	-11	2112	1	0.00	0.01	0.01	
1A	123	-17313	-2084	1656	0	1455	44762	3	0.01	0.02	0.29	
1B	123	-17313	-1956	1656	0	1455	42591	3	0.01	0.02	0.28	
1C	123	-17313	-2084	-1656	0	-1455	44762	3	0.01	0.02	0.29	
1D	123	-17313	-1956	-1656	0	-1455	42591	3	0.01	0.02	0.28	
1E	123	17313	-2084	1656	0	1455	44762	1	0.01	0.02	0.20	
1F	123	17313	-1956	1656	0	1455	42591	1	0.01	0.02	0.19	
1G	123	17313	-2084	-1656	0	-1455	44762	1	0.01	0.02	0.20	

1H	123	17313	-1956	-1656	0	-1455	42591	1	0.01	0.02	0.19	
1I	123	-13788	-2084	533	0	466	44762	3	0.01	0.01	0.26	
1J	123	-13788	-1956	533	0	466	42591	3	0.01	0.01	0.25	
1K	123	-13788	-2084	-533	0	-466	44762	3	0.01	0.01	0.26	
1L	123	-13788	-1956	-533	0	-466	42591	3	0.01	0.01	0.25	
1M	123	13788	-2084	533	0	466	44762	1	0.01	0.01	0.20	
1N	123	13788	-1956	533	0	466	42591	1	0.01	0.01	0.19	
1O	123	13788	-2084	-533	0	-466	44762	1	0.01	0.01	0.20	
1P	123	13788	-1956	-533	0	-466	42591	1	0.01	0.01	0.19	
1Q	123	-7177	-2235	505	0	443	47295	3	0.01	0.01	0.26	
1R	123	-7177	-1805	505	0	443	40059	3	0.01	0.01	0.23	
1S	123	-7177	-2235	-505	0	-443	47295	3	0.01	0.01	0.26	
1T	123	-7177	-1805	-505	0	-443	40059	3	0.01	0.01	0.23	
1U	123	7177	-2235	505	0	443	47295	1	0.01	0.01	0.21	
1V	123	7177	-1805	505	0	443	40059	1	0.01	0.01	0.18	
1W	123	7177	-2235	-505	0	-443	47295	1	0.01	0.01	0.21	
1X	123	7177	-1805	-505	0	-443	40059	1	0.01	0.01	0.18	
2	123	2572	-2020	-238	0	-134	43677	1	0.01	0.00	0.20	
3	123	1543	-3336	-143	0	-80	71985	1	0.02	0.00	0.33	
4	123	1543	-4764	-143	0	-80	102603	1	0.02	0.00	0.46	
5	123	2572	-3692	-238	0	-134	79645	1	0.02	0.00	0.36	
7	123	-6647	-5954	2	0	9	100936	3	0.03	0.01	0.52	
20	123	-9148	-3410	5	0	11	66971	3	0.02	0.01	0.35	
22	123	6098	-288	-3	0	-7	1760	1	0.00	0.01	0.01	
1A	245	-17313	-4111	1656	0	-577	40978	3	0.02	0.02	0.25	
1B	245	-17313	-3983	1656	0	-577	38942	3	0.02	0.02	0.24	
1C	245	-17313	-4111	-1656	0	577	40978	3	0.02	0.02	0.25	
1D	245	-17313	-3983	-1656	0	577	38942	3	0.02	0.02	0.24	
1E	245	17313	-4111	1656	0	-577	40978	1	0.02	0.02	0.19	
1F	245	17313	-3983	1656	0	-577	38942	1	0.02	0.02	0.18	
1G	245	17313	-4111	-1656	0	577	40978	1	0.02	0.02	0.19	
1H	245	17313	-3983	-1656	0	577	38942	1	0.02	0.02	0.18	
1I	245	-13788	-4111	533	0	-190	40978	3	0.02	0.01	0.23	
1J	245	-13788	-3983	533	0	-190	38942	3	0.02	0.01	0.22	
1K	245	-13788	-4111	-533	0	190	40978	3	0.02	0.01	0.23	
1L	245	-13788	-3983	-533	0	190	38942	3	0.02	0.01	0.22	
1M	245	13788	-4111	533	0	-190	40978	1	0.02	0.01	0.19	
1N	245	13788	-3983	533	0	-190	38942	1	0.02	0.01	0.18	
1O	245	13788	-4111	-533	0	190	40978	1	0.02	0.01	0.19	
1P	245	13788	-3983	-533	0	190	38942	1	0.02	0.01	0.18	
1Q	245	-7177	-4262	505	0	-177	43353	3	0.02	0.01	0.23	
1R	245	-7177	-3832	505	0	-177	36567	3	0.02	0.01	0.20	
1S	245	-7177	-4262	-505	0	177	43353	3	0.02	0.01	0.23	
1T	245	-7177	-3832	-505	0	177	36567	3	0.02	0.01	0.20	
1U	245	7177	-4262	505	0	-177	43353	1	0.02	0.01	0.20	
1V	245	7177	-3832	505	0	-177	36567	1	0.02	0.01	0.17	
1W	245	7177	-4262	-505	0	177	43353	1	0.02	0.01	0.20	
1X	245	7177	-3832	-505	0	177	36567	1	0.02	0.01	0.17	
2	245	2572	-4047	-238	0	157	39960	1	0.02	0.00	0.18	
3	245	1543	-6683	-143	0	94	65850	1	0.03	0.00	0.30	
4	245	1543	-9544	-143	0	94	93850	1	0.04	0.00	0.42	
5	245	2572	-7398	-238	0	157	72850	1	0.03	0.00	0.33	
7	245	-6647	-8943	2	0	7	91810	3	0.04	0.01	0.47	
20	245	-9148	-6399	5	0	5	60960	3	0.03	0.01	0.32	
22	245	6098	-288	-3	0	-4	1408	1	0.00	0.01	0.01	

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	$\gamma_{min.}$	ky	kz	kLT	χ_{LT}	I.S.n.	I.S.m.	I.S.	Nota
	kg	kg*m											
1A	-17313	3487	46063	3	0.9027	1.0015	1.0037	--	--	0.02	--	0.37	Snell. 'zx'= 35
1B	-17313	3487	43757	3	0.9027	1.0015	1.0037	--	--	0.02	--	0.36	Snell. 'zx'= 35
1C	-17313	-3487	46063	3	0.9027	1.0015	1.0037	--	--	0.02	--	0.37	Snell. 'zx'= 35
1D	-17313	-3487	43757	3	0.9027	1.0015	1.0037	--	--	0.02	--	0.36	Snell. 'zx'= 35
1I	-13788	1121	46063	3	0.9027	1.0012	1.0030	--	--	0.02	--	0.29	Snell. 'zx'= 35
1J	-13788	1121	43757	3	0.9027	1.0012	1.0030	--	--	0.02	--	0.28	Snell. 'zx'= 35
1K	-13788	-1121	46063	3	0.9027	1.0012	1.0030	--	--	0.02	--	0.29	Snell. 'zx'= 35
1L	-13788	-1121	43757	3	0.9027	1.0012	1.0030	--	--	0.02	--	0.28	Snell. 'zx'= 35
1Q	-7177	1063	48753	3	0.9027	1.0006	1.0015	--	--	0.01	--	0.29	Snell. 'zx'= 35
1R	-7177	1063	41067	3	0.9027	1.0006	1.0015	--	--	0.01	--	0.25	Snell. 'zx'= 35
1S	-7177	-1063	48753	3	0.9027	1.0006	1.0015	--	--	0.01	--	0.29	Snell. 'zx'= 35
1T	-7177	-1063	41067	3	0.9027	1.0006	1.0015	--	--	0.01	--	0.25	Snell. 'zx'= 35
7	-6647	10	106400	3	0.9027	1.0045	1.0014	--	--	0.01	--	0.55	Snell. 'zx'= 35
20	-9148	17	69320	3	0.9027	1.0040	1.0020	--	--	0.01	--	0.36	Snell. 'zx'= 35

ASTA NUM. 12 NI 16 NF 5 Lungh. 435.0 cm SEZ. 1 Ps HEB 600

categoria: p.p. y Permanente Congresso Neve qy tot.
qy medio: 211.95 1443.00 975.00 195.00 2824.95 kg/m

Sollecitazioni di calcolo e di verifica

Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	cm	kg			kg*m							
1A	0	-12034	-5250	163	0	765	38392	3	0.02	0.01	0.23	
1B	0	-12034	-4812	163	0	765	36488	3	0.02	0.01	0.22	
1C	0	-12034	-5250	-163	0	-765	38392	3	0.02	0.01	0.23	
1D	0	-12034	-4812	-163	0	-765	36488	3	0.02	0.01	0.22	
1E	0	12034	-5250	163	0	765	38392	1	0.02	0.01	0.17	
1F	0	12034	-4812	163	0	765	36488	1	0.02	0.01	0.16	
1G	0	12034	-5250	-163	0	-765	38392	1	0.02	0.01	0.17	
1H	0	12034	-4812	-163	0	-765	36488	1	0.02	0.01	0.16	

1I	0	-16878	-5250	72	0	259	38392	3	0.02	0.02	0.22	
1J	0	-16878	-4812	72	0	259	36488	3	0.02	0.02	0.21	
1K	0	-16878	-5250	-72	0	-259	38392	3	0.02	0.02	0.22	
1L	0	-16878	-4812	-72	0	-259	36488	3	0.02	0.02	0.21	
1M	0	16878	-5250	72	0	259	38392	1	0.02	0.02	0.17	
1N	0	16878	-4812	72	0	259	36488	1	0.02	0.02	0.16	
1O	0	16878	-5250	-72	0	-259	38392	1	0.02	0.02	0.17	
1P	0	16878	-4812	-72	0	-259	36488	1	0.02	0.02	0.16	
1Q	0	-6672	-5760	54	0	236	40612	3	0.03	0.01	0.22	
1R	0	-6672	-4302	54	0	236	34268	3	0.02	0.01	0.19	
1S	0	-6672	-5760	-54	0	-236	40612	3	0.03	0.01	0.22	
1T	0	-6672	-4302	-54	0	-236	34268	3	0.02	0.01	0.19	
1U	0	6672	-5760	54	0	236	40612	1	0.03	0.01	0.18	
1V	0	6672	-4302	54	0	236	34268	1	0.02	0.01	0.15	
1W	0	6672	-5760	-54	0	-236	40612	1	0.03	0.01	0.18	
1X	0	6672	-4302	-54	0	-236	34268	1	0.02	0.01	0.15	
2	0	1325	-5031	-85	0	-359	37440	1	0.02	0.00	0.17	
3	0	795	-8281	-51	0	-215	61710	1	0.04	0.00	0.28	
4	0	795	-11790	-51	0	-215	87950	1	0.05	0.00	0.40	
5	0	1325	-9158	-85	0	-359	68270	1	0.04	0.00	0.31	
7	0	-10210	-14610	4	0	12	86500	3	0.07	0.01	0.45	
20	0	-10200	-7836	5	0	14	57020	3	0.04	0.01	0.30	
22	0	6803	-288	-3	0	-10	1251	1	0.00	0.01	0.01	
1A	217	-12034	-8849	163	0	445	23060	3	0.04	0.01	0.14	
1B	217	-12034	-8412	163	0	445	22108	3	0.04	0.01	0.14	
1C	217	-12034	-8849	-163	0	-445	23060	3	0.04	0.01	0.14	
1D	217	-12034	-8412	-163	0	-445	22108	3	0.04	0.01	0.14	
1E	217	12034	-8849	163	0	445	23060	1	0.04	0.01	0.10	
1F	217	12034	-8412	163	0	445	22108	1	0.04	0.01	0.10	
1G	217	12034	-8849	-163	0	-445	23060	1	0.04	0.01	0.10	
1H	217	12034	-8412	-163	0	-445	22108	1	0.04	0.01	0.10	
1I	217	-16878	-8849	72	0	69	23060	3	0.04	0.02	0.14	
1J	217	-16878	-8412	72	0	69	22108	3	0.04	0.02	0.13	
1K	217	-16878	-8849	-72	0	-69	23060	3	0.04	0.02	0.14	
1L	217	-16878	-8412	-72	0	-69	22108	3	0.04	0.02	0.13	
1M	217	16878	-8849	72	0	69	23060	1	0.04	0.02	0.10	
1N	217	16878	-8412	72	0	69	22108	1	0.04	0.02	0.10	
1O	217	16878	-8849	-72	0	-69	23060	1	0.04	0.02	0.10	
1P	217	16878	-8412	-72	0	-69	22108	1	0.04	0.02	0.10	
1Q	217	-6672	-9360	54	0	90	24170	3	0.04	0.01	0.13	
1R	217	-6672	-7901	54	0	90	20997	3	0.04	0.01	0.12	
1S	217	-6672	-9360	-54	0	-90	24170	3	0.04	0.01	0.13	
1T	217	-6672	-7901	-54	0	-90	20997	3	0.04	0.01	0.12	
1U	217	6672	-9360	54	0	90	24170	1	0.04	0.01	0.11	
1V	217	6672	-7901	54	0	90	20997	1	0.04	0.01	0.09	
1W	217	6672	-9360	-54	0	-90	24170	1	0.04	0.01	0.11	
1X	217	6672	-7901	-54	0	-90	20997	1	0.04	0.01	0.09	
2	217	1325	-8630	-85	0	-174	22584	1	0.04	0.00	0.10	
3	217	795	-14225	-51	0	-104	37235	1	0.06	0.00	0.17	
4	217	795	-20275	-51	0	-104	53086	1	0.09	0.00	0.24	
5	217	1325	-15739	-85	0	-174	41197	1	0.07	0.00	0.19	
7	217	-10210	-19920	4	0	2	48946	3	0.09	0.01	0.26	
20	217	-10200	-13143	5	0	3	34207	3	0.06	0.01	0.19	
22	217	6803	-288	-3	0	-2	625	1	0.00	0.01	0.00	
1A	435	-12034	-12449	163	0	126	-101	3	0.06	0.01	0.02	
1B	435	-12034	-12011	163	0	126	-102	3	0.05	0.01	0.02	
1C	435	-12034	-12449	-163	0	-126	-101	3	0.06	0.01	0.02	
1D	435	-12034	-12011	-163	0	-126	-102	3	0.05	0.01	0.02	
1E	435	12034	-12449	163	0	126	-101	1	0.06	0.01	0.00	
1F	435	12034	-12011	163	0	126	-102	1	0.05	0.01	0.00	
1G	435	12034	-12449	-163	0	-126	-101	1	0.06	0.01	0.00	
1H	435	12034	-12011	-163	0	-126	-102	1	0.05	0.01	0.00	
1I	435	-16878	-12449	72	0	-121	-101	3	0.06	0.02	0.02	
1J	435	-16878	-12011	72	0	-121	-102	3	0.05	0.02	0.02	
1K	435	-16878	-12449	-72	0	121	-101	3	0.06	0.02	0.02	
1L	435	-16878	-12011	-72	0	121	-102	3	0.05	0.02	0.02	
1M	435	16878	-12449	72	0	-121	-101	1	0.06	0.02	0.00	
1N	435	16878	-12011	72	0	-121	-102	1	0.05	0.02	0.00	
1O	435	16878	-12449	-72	0	121	-101	1	0.06	0.02	0.00	
1P	435	16878	-12011	-72	0	121	-102	1	0.05	0.02	0.00	
1Q	435	-6672	-12959	54	0	-57	-101	3	0.06	0.01	0.01	
1R	435	-6672	-11501	54	0	-57	-102	3	0.05	0.01	0.01	
1S	435	-6672	-12959	-54	0	57	-101	3	0.06	0.01	0.01	
1T	435	-6672	-11501	-54	0	57	-102	3	0.05	0.01	0.01	
1U	435	6672	-12959	54	0	-57	-101	1	0.06	0.01	0.00	
1V	435	6672	-11501	54	0	-57	-102	1	0.05	0.01	0.00	
1W	435	6672	-12959	-54	0	57	-101	1	0.06	0.01	0.00	
1X	435	6672	-11501	-54	0	57	-102	1	0.05	0.01	0.00	
2	435	1325	-12230	-85	0	10	-101	1	0.06	0.00	0.00	
3	435	795	-20170	-51	0	6	-167	1	0.09	0.00	0.00	
4	435	795	-28760	-51	0	6	-239	1	0.13	0.00	0.00	
5	435	1325	-22320	-85	0	10	-185	1	0.10	0.00	0.00	
7	435	-10210	-25230	4	0	-7	-150	3	0.11	0.01	0.01	
20	435	-10200	-18450	5	0	-7	-150	3	0.08	0.01	0.01	
22	435	6803	-288	-3	0	5	-0	1	0.00	0.01	0.00	

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	$\gamma_{min.}$	ky	kz	kLT	χ_{LT}	I.S.n.	I.S.m.	I.S.	Nota
	kg	kg*m											
1A	-12034	765	38392	3	0.7170	1.0088	1.0018	--	--	0.02	--	0.24	Snell. 'zx'= 61
1B	-12034	765	36488	3	0.7170	1.0088	1.0018	--	--	0.02	--	0.23	Snell. 'zx'= 61
1C	-12034	-765	38392	3	0.7170	1.0088	1.0018	--	--	0.02	--	0.24	Snell. 'zx'= 61

1D	-12034	-765	36488	3	0.7170	1.0088	1.0018	--	--	0.02	--	0.23	Snell.	'zx'='	61
1I	-16878	259	38392	3	0.7170	0.9950	1.0025	--	--	0.03	--	0.23	Snell.	'zx'='	61
1J	-16878	259	36488	3	0.7170	0.9950	1.0026	--	--	0.03	--	0.22	Snell.	'zx'='	61
1K	-16878	-259	38392	3	0.7170	0.9950	1.0025	--	--	0.03	--	0.23	Snell.	'zx'='	61
1L	-16878	-259	36488	3	0.7170	0.9950	1.0026	--	--	0.03	--	0.22	Snell.	'zx'='	61
1Q	-6672	236	40612	3	0.7170	1.0005	1.0010	--	--	0.01	--	0.22	Snell.	'zx'='	61
1R	-6672	236	34268	3	0.7170	1.0005	1.0010	--	--	0.01	--	0.19	Snell.	'zx'='	61
1S	-6672	-236	40612	3	0.7170	1.0005	1.0010	--	--	0.01	--	0.22	Snell.	'zx'='	61
1T	-6672	-236	34268	3	0.7170	1.0005	1.0010	--	--	0.01	--	0.19	Snell.	'zx'='	61
7	-10210	12	86500	3	0.7170	0.9944	1.0012	--	--	0.02	--	0.46	Snell.	'zx'='	61
20	-10200	14	57020	3	0.7170	0.9962	1.0013	--	--	0.02	--	0.31	Snell.	'zx'='	61

ASTA NUM. 13 NI 19 NF 6 Lungh. 435.0 cm SEZ. 1 Ps HEB 600

categoria: p.p. y Permanente Congresso Neve qy tot.
 qy medio: 211.95 1443.00 975.00 195.00 2824.95 kg/m

Sollecitazioni di calcolo e di verifica Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
--	cm	kg			kg*m							
1A	0	-7049	-5250	149	0	701	38392	3	0.02	0.01	0.23	
1B	0	-7049	-4812	149	0	701	36488	3	0.02	0.01	0.22	
1C	0	-7049	-5250	-149	0	-701	38392	3	0.02	0.01	0.23	
1D	0	-7049	-4812	-149	0	-701	36488	3	0.02	0.01	0.22	
1E	0	7049	-5250	149	0	701	38392	1	0.02	0.01	0.17	
1F	0	7049	-4812	149	0	701	36488	1	0.02	0.01	0.16	
1G	0	7049	-5250	-149	0	-701	38392	1	0.02	0.01	0.17	
1H	0	7049	-4812	-149	0	-701	36488	1	0.02	0.01	0.16	
1I	0	-2260	-5250	71	0	250	38392	3	0.02	0.00	0.21	
1J	0	-2260	-4812	71	0	250	36488	3	0.02	0.00	0.20	
1K	0	-2260	-5250	-71	0	-250	38392	3	0.02	0.00	0.21	
1L	0	-2260	-4812	-71	0	-250	36488	3	0.02	0.00	0.20	
1M	0	2260	-5250	71	0	250	38392	1	0.02	0.00	0.17	
1N	0	2260	-4812	71	0	250	36488	1	0.02	0.00	0.16	
1O	0	2260	-5250	-71	0	-250	38392	1	0.02	0.00	0.17	
1P	0	2260	-4812	-71	0	-250	36488	1	0.02	0.00	0.16	
1Q	0	-2148	-5760	51	0	220	40612	3	0.03	0.00	0.22	
1R	0	-2148	-4302	51	0	220	34268	3	0.02	0.00	0.18	
1S	0	-2148	-5760	-51	0	-220	40612	3	0.03	0.00	0.22	
1T	0	-2148	-4302	-51	0	-220	34268	3	0.02	0.00	0.18	
1U	0	2148	-5760	51	0	220	40612	1	0.03	0.00	0.18	
1V	0	2148	-4302	51	0	220	34268	1	0.02	0.00	0.15	
1W	0	2148	-5760	-51	0	-220	40612	1	0.03	0.00	0.18	
1X	0	2148	-4302	-51	0	-220	34268	1	0.02	0.00	0.15	
2	0	-1262	-5031	943	0	404	37440	3	0.02	0.00	0.20	
3	0	-757	-8281	566	0	243	61710	3	0.04	0.00	0.32	
4	0	-757	-11790	566	0	243	87950	3	0.05	0.00	0.46	
5	0	-1262	-9158	943	0	404	68270	3	0.04	0.00	0.36	
7	0	-472	-10420	4	0	12	68280	3	0.05	0.00	0.35	
20	0	-470	-7586	4	0	12	55930	3	0.03	0.00	0.29	
22	0	314	-121	-3	0	-8	524	1	0.00	0.00	0.00	
1A	217	-7049	-8849	149	0	415	23060	3	0.04	0.01	0.14	
1B	217	-7049	-8412	149	0	415	22108	3	0.04	0.01	0.13	
1C	217	-7049	-8849	-149	0	-415	23060	3	0.04	0.01	0.14	
1D	217	-7049	-8412	-149	0	-415	22108	3	0.04	0.01	0.13	
1E	217	7049	-8849	149	0	415	23060	1	0.04	0.01	0.10	
1F	217	7049	-8412	149	0	415	22108	1	0.04	0.01	0.10	
1G	217	7049	-8849	-149	0	-415	23060	1	0.04	0.01	0.10	
1H	217	7049	-8412	-149	0	-415	22108	1	0.04	0.01	0.10	
1I	217	-2260	-8849	71	0	65	23060	3	0.04	0.00	0.12	
1J	217	-2260	-8412	71	0	65	22108	3	0.04	0.00	0.12	
1K	217	-2260	-8849	-71	0	-65	23060	3	0.04	0.00	0.12	
1L	217	-2260	-8412	-71	0	-65	22108	3	0.04	0.00	0.12	
1M	217	2260	-8849	71	0	65	23060	1	0.04	0.00	0.10	
1N	217	2260	-8412	71	0	65	22108	1	0.04	0.00	0.10	
1O	217	2260	-8849	-71	0	-65	23060	1	0.04	0.00	0.10	
1P	217	2260	-8412	-71	0	-65	22108	1	0.04	0.00	0.10	
1Q	217	-2148	-9360	51	0	81	24170	3	0.04	0.00	0.13	
1R	217	-2148	-7901	51	0	81	20997	3	0.04	0.00	0.11	
1S	217	-2148	-9360	-51	0	-81	24170	3	0.04	0.00	0.13	
1T	217	-2148	-7901	-51	0	-81	20997	3	0.04	0.00	0.11	
1U	217	2148	-9360	51	0	81	24170	1	0.04	0.00	0.11	
1V	217	2148	-7901	51	0	81	20997	1	0.04	0.00	0.09	
1W	217	2148	-9360	-51	0	-81	24170	1	0.04	0.00	0.11	
1X	217	2148	-7901	-51	0	-81	20997	1	0.04	0.00	0.09	
2	217	-1262	-8630	82	0	-710	22584	3	0.04	0.00	0.14	
3	217	-757	-14225	49	0	-426	37235	3	0.06	0.00	0.20	
4	217	-757	-20275	49	0	-426	53086	3	0.09	0.00	0.28	
5	217	-1262	-15739	82	0	-710	41197	3	0.07	0.00	0.23	
7	217	-472	-15730	4	0	2	39837	3	0.07	0.00	0.20	
20	217	-470	-12893	4	0	2	33662	3	0.06	0.00	0.17	
22	217	314	-121	-3	0	-1	262	1	0.00	0.00	0.00	
1A	435	-7049	-12449	149	0	128	-101	3	0.06	0.01	0.01	
1B	435	-7049	-12011	149	0	128	-102	3	0.05	0.01	0.01	
1C	435	-7049	-12449	-149	0	-128	-101	3	0.06	0.01	0.01	
1D	435	-7049	-12011	-149	0	-128	-102	3	0.05	0.01	0.01	
1E	435	7049	-12449	149	0	128	-101	1	0.06	0.01	0.00	
1F	435	7049	-12011	149	0	128	-102	1	0.05	0.01	0.00	
1G	435	7049	-12449	-149	0	-128	-101	1	0.06	0.01	0.00	
1H	435	7049	-12011	-149	0	-128	-102	1	0.05	0.01	0.00	
1I	435	-2260	-12449	71	0	-121	-101	3	0.06	0.00	0.01	
1J	435	-2260	-12011	71	0	-121	-102	3	0.05	0.00	0.01	
1K	435	-2260	-12449	-71	0	121	-101	3	0.06	0.00	0.01	
1L	435	-2260	-12011	-71	0	121	-102	3	0.05	0.00	0.01	
1M	435	2260	-12449	71	0	-121	-101	1	0.06	0.00	0.00	

1N	435	2260	-12011	71	0	-121	-102	1	0.05	0.00	0.00	
1O	435	2260	-12449	-71	0	121	-101	1	0.06	0.00	0.00	
1P	435	2260	-12011	-71	0	121	-102	1	0.05	0.00	0.00	
1Q	435	-2148	-12959	51	0	-57	-101	3	0.06	0.00	0.00	
1R	435	-2148	-11501	51	0	-57	-102	3	0.05	0.00	0.00	
1S	435	-2148	-12959	-51	0	57	-101	3	0.06	0.00	0.00	
1T	435	-2148	-11501	-51	0	57	-102	3	0.05	0.00	0.00	
1U	435	2148	-12959	51	0	-57	-101	1	0.06	0.00	0.00	
1V	435	2148	-11501	51	0	-57	-102	1	0.05	0.00	0.00	
1W	435	2148	-12959	-51	0	57	-101	1	0.06	0.00	0.00	
1X	435	2148	-11501	-51	0	57	-102	1	0.05	0.00	0.00	
2	435	-1262	-12230	-779	0	48	-101	3	0.06	0.00	0.00	
3	435	-757	-20170	-468	0	29	-167	3	0.09	0.00	0.00	
4	435	-757	-28760	-468	0	29	-239	3	0.13	0.00	0.00	
5	435	-1262	-22320	-779	0	48	-185	3	0.10	0.00	0.00	
7	435	-472	-21040	4	0	-7	-149	3	0.10	0.00	0.00	
20	435	-470	-18200	4	0	-8	-149	3	0.08	0.00	0.00	
22	435	314	-121	-3	0	5	0	1	0.00	0.00	0.00	

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	$\gamma_{min.}$	ky	kz	kLT	χ_{LT}	I.S.n.	I.S.m.	I.S.	Nota
	kg	kg*m											
1A	-7049	701	38392	3	0.7170	1.0135	1.0011	--	--	0.01	--	0.23	Snell. 'zx'= 61
1B	-7049	701	36488	3	0.7170	1.0135	1.0011	--	--	0.01	--	0.22	Snell. 'zx'= 61
1C	-7049	-701	38392	3	0.7170	1.0135	1.0011	--	--	0.01	--	0.23	Snell. 'zx'= 61
1D	-7049	-701	36488	3	0.7170	1.0135	1.0011	--	--	0.01	--	0.22	Snell. 'zx'= 61
1I	-2260	250	38392	3	0.7170	1.0104	1.0003	--	--	0.00	--	0.21	Snell. 'zx'= 61
1J	-2260	250	36488	3	0.7170	1.0104	1.0003	--	--	0.00	--	0.20	Snell. 'zx'= 61
1K	-2260	-250	38392	3	0.7170	1.0104	1.0003	--	--	0.00	--	0.21	Snell. 'zx'= 61
1L	-2260	-250	36488	3	0.7170	1.0104	1.0003	--	--	0.00	--	0.20	Snell. 'zx'= 61
1Q	-2148	220	40612	3	0.7170	1.0116	1.0003	--	--	0.00	--	0.22	Snell. 'zx'= 61
1R	-2148	220	34268	3	0.7170	1.0116	1.0003	--	--	0.00	--	0.18	Snell. 'zx'= 61
1S	-2148	-220	40612	3	0.7170	1.0116	1.0003	--	--	0.00	--	0.22	Snell. 'zx'= 61
1T	-2148	-220	34268	3	0.7170	1.0116	1.0003	--	--	0.00	--	0.18	Snell. 'zx'= 61
2	-1262	-710	37440	3	0.7170	1.0019	1.0002	--	--	0.00	--	0.22	Snell. 'zx'= 61
3	-757	-426	61710	3	0.7170	1.0015	1.0001	--	--	0.00	--	0.33	Snell. 'zx'= 61
4	-757	-426	87950	3	0.7170	1.0015	1.0001	--	--	0.00	--	0.46	Snell. 'zx'= 61
5	-1262	-710	68270	3	0.7170	1.0019	1.0002	--	--	0.00	--	0.37	Snell. 'zx'= 61
7	-472	12	68280	3	0.7170	1.0505	1.0001	--	--	0.00	--	0.35	Snell. 'zx'= 61
20	-470	12	55930	3	0.7170	1.0490	1.0001	--	--	0.00	--	0.29	Snell. 'zx'= 61

ASTA NUM. 14 NI 20 NF 8 Lungh. 245.0 cm SEZ. 1 Ps HEB 600

categoria: p.p. y Permanente Congresso Neve qy tot.
qy medio: 211.95 1443.00 975.00 195.00 2824.95 kg/m

Sollecitazioni di calcolo e di verifica

Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	cm	kg			kg*m							
1A	0	-14598	-57	1663	0	3479	46063	3	0.00	0.02	0.36	
1B	0	-14598	72	1663	0	3479	43757	3	0.00	0.02	0.35	
1C	0	-14598	-57	-1663	0	-3479	46063	3	0.00	0.02	0.36	
1D	0	-14598	72	-1663	0	-3479	43757	3	0.00	0.02	0.35	
1E	0	14598	-57	1663	0	3479	46063	1	0.00	0.02	0.21	
1F	0	14598	72	1663	0	3479	43757	1	0.00	0.02	0.20	
1G	0	14598	-57	-1663	0	-3479	46063	1	0.00	0.02	0.21	
1H	0	14598	72	-1663	0	-3479	43757	1	0.00	0.02	0.20	
1I	0	-5617	-57	539	0	1119	46063	3	0.00	0.01	0.28	
1J	0	-5617	72	539	0	1119	43757	3	0.00	0.01	0.26	
1K	0	-5617	-57	-539	0	-1119	46063	3	0.00	0.01	0.28	
1L	0	-5617	72	-539	0	-1119	43757	3	0.00	0.01	0.26	
1M	0	5617	-57	539	0	1119	46063	1	0.00	0.01	0.21	
1N	0	5617	72	539	0	1119	43757	1	0.00	0.01	0.20	
1O	0	5617	-57	-539	0	-1119	46063	1	0.00	0.01	0.21	
1P	0	5617	72	-539	0	-1119	43757	1	0.00	0.01	0.20	
1Q	0	-4665	-208	508	0	1061	48753	3	0.00	0.01	0.29	
1R	0	-4665	222	508	0	1061	41067	3	0.00	0.01	0.25	
1S	0	-4665	-208	-508	0	-1061	48753	3	0.00	0.01	0.29	
1T	0	-4665	222	-508	0	-1061	41067	3	0.00	0.01	0.25	
1U	0	4665	-208	508	0	1061	48753	1	0.00	0.01	0.22	
1V	0	4665	222	508	0	1061	41067	1	0.00	0.01	0.19	
1W	0	4665	-208	-508	0	-1061	48753	1	0.00	0.01	0.22	
1X	0	4665	222	-508	0	-1061	41067	1	0.00	0.01	0.19	
2	0	-2566	7	247	0	-215	44910	3	0.00	0.00	0.24	
3	0	-1540	12	148	0	-129	74020	3	0.00	0.00	0.38	
4	0	-1540	17	148	0	-129	105500	3	0.00	0.00	0.54	
5	0	-2566	13	247	0	-215	81900	3	0.00	0.00	0.43	
7	0	-516	-1238	-6	0	4	83050	3	0.01	0.00	0.42	
20	0	-1543	-170	-8	0	5	67480	3	0.00	0.00	0.35	
22	0	1029	-121	5	0	-3	888	1	0.00	0.00	0.00	
1A	123	-14598	-2084	1663	0	1438	44762	3	0.01	0.02	0.29	
1B	123	-14598	-1956	1663	0	1438	42591	3	0.01	0.02	0.28	
1C	123	-14598	-2084	-1663	0	-1438	44762	3	0.01	0.02	0.29	
1D	123	-14598	-1956	-1663	0	-1438	42591	3	0.01	0.02	0.28	
1E	123	14598	-2084	1663	0	1438	44762	1	0.01	0.02	0.20	
1F	123	14598	-1956	1663	0	1438	42591	1	0.01	0.02	0.19	
1G	123	14598	-2084	-1663	0	-1438	44762	1	0.01	0.02	0.20	
1H	123	14598	-1956	-1663	0	-1438	42591	1	0.01	0.02	0.19	
1I	123	-5617	-2084	539	0	453	44762	3	0.01	0.01	0.25	
1J	123	-5617	-1956	539	0	453	42591	3	0.01	0.01	0.24	

1K	123	-5617	-2084	-539	0	-453	44762	3	0.01	0.01	0.25	
1L	123	-5617	-1956	-539	0	-453	42591	3	0.01	0.01	0.24	
1M	123	5617	-2084	539	0	453	44762	1	0.01	0.01	0.20	
1N	123	5617	-1956	539	0	453	42591	1	0.01	0.01	0.19	
1O	123	5617	-2084	-539	0	-453	44762	1	0.01	0.01	0.20	
1P	123	5617	-1956	-539	0	-453	42591	1	0.01	0.01	0.19	
1Q	123	-4665	-2235	508	0	436	47295	3	0.01	0.01	0.26	
1R	123	-4665	-1805	508	0	436	40059	3	0.01	0.01	0.22	
1S	123	-4665	-2235	-508	0	-436	47295	3	0.01	0.01	0.26	
1T	123	-4665	-1805	-508	0	-436	40059	3	0.01	0.01	0.22	
1U	123	4665	-2235	508	0	436	47295	1	0.01	0.01	0.21	
1V	123	4665	-1805	508	0	436	40059	1	0.01	0.01	0.18	
1W	123	4665	-2235	-508	0	-436	47295	1	0.01	0.01	0.21	
1X	123	4665	-1805	-508	0	-436	40059	1	0.01	0.01	0.18	
2	123	-2566	-2020	-238	0	-220	43677	3	0.01	0.00	0.23	
3	123	-1540	-3336	-143	0	-132	71985	3	0.02	0.00	0.37	
4	123	-1540	-4764	-143	0	-132	102603	3	0.02	0.00	0.53	
5	123	-2566	-3692	-238	0	-220	79645	3	0.02	0.00	0.42	
7	123	-516	-4227	-6	0	12	79701	3	0.02	0.00	0.41	
20	123	-1543	-3159	-8	0	15	65441	3	0.01	0.00	0.34	
22	123	1029	-121	5	0	-10	740	1	0.00	0.00	0.00	

1A	245	-14598	-4111	1663	0	-604	40978	3	0.02	0.02	0.24	
1B	245	-14598	-3983	1663	0	-604	38942	3	0.02	0.02	0.23	
1C	245	-14598	-4111	-1663	0	604	40978	3	0.02	0.02	0.24	
1D	245	-14598	-3983	-1663	0	604	38942	3	0.02	0.02	0.23	
1E	245	14598	-4111	1663	0	-604	40978	1	0.02	0.02	0.19	
1F	245	14598	-3983	1663	0	-604	38942	1	0.02	0.02	0.18	
1G	245	14598	-4111	-1663	0	604	40978	1	0.02	0.02	0.19	
1H	245	14598	-3983	-1663	0	604	38942	1	0.02	0.02	0.18	
1I	245	-5617	-4111	539	0	-214	40978	3	0.02	0.01	0.22	
1J	245	-5617	-3983	539	0	-214	38942	3	0.02	0.01	0.21	
1K	245	-5617	-4111	-539	0	214	40978	3	0.02	0.01	0.22	
1L	245	-5617	-3983	-539	0	214	38942	3	0.02	0.01	0.21	
1M	245	5617	-4111	539	0	-214	40978	1	0.02	0.01	0.19	
1N	245	5617	-3983	539	0	-214	38942	1	0.02	0.01	0.18	
1O	245	5617	-4111	-539	0	214	40978	1	0.02	0.01	0.19	
1P	245	5617	-3983	-539	0	214	38942	1	0.02	0.01	0.18	
1Q	245	-4665	-4262	508	0	-189	43353	3	0.02	0.01	0.23	
1R	245	-4665	-3832	508	0	-189	36567	3	0.02	0.01	0.20	
1S	245	-4665	-4262	-508	0	189	43353	3	0.02	0.01	0.23	
1T	245	-4665	-3832	-508	0	189	36567	3	0.02	0.01	0.20	
1U	245	4665	-4262	508	0	-189	43353	1	0.02	0.01	0.20	
1V	245	4665	-3832	508	0	-189	36567	1	0.02	0.01	0.17	
1W	245	4665	-4262	-508	0	189	43353	1	0.02	0.01	0.20	
1X	245	4665	-3832	-508	0	189	36567	1	0.02	0.01	0.17	
2	245	-2566	-4047	-724	0	369	39960	3	0.02	0.00	0.22	
3	245	-1540	-6683	-434	0	222	65850	3	0.03	0.00	0.34	
4	245	-1540	-9544	-434	0	222	93850	3	0.04	0.00	0.49	
5	245	-2566	-7398	-724	0	369	72850	3	0.03	0.00	0.39	
7	245	-516	-7216	-6	0	20	72690	3	0.03	0.00	0.37	
20	245	-1543	-6148	-8	0	25	59740	3	0.03	0.00	0.31	
22	245	1029	-121	5	0	-16	592	1	0.00	0.00	0.00	

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	$\gamma_{min.}$	ky	kz	kLT	χ_{LT}	I.S.n.	I.S.m.	I.S.	Nota
--	kg	kg*m	kg*m										
1A	-14598	3479	46063	3	0.9027	1.0019	1.0031	--	--	0.02	--	0.36	Snell. 'zx'= 35
1B	-14598	3479	43757	3	0.9027	1.0019	1.0031	--	--	0.02	--	0.35	Snell. 'zx'= 35
1C	-14598	-3479	46063	3	0.9027	1.0019	1.0031	--	--	0.02	--	0.36	Snell. 'zx'= 35
1D	-14598	-3479	43757	3	0.9027	1.0019	1.0031	--	--	0.02	--	0.35	Snell. 'zx'= 35
1I	-5617	1119	46063	3	0.9027	1.0012	1.0012	--	--	0.01	--	0.28	Snell. 'zx'= 35
1J	-5617	1119	43757	3	0.9027	1.0012	1.0012	--	--	0.01	--	0.27	Snell. 'zx'= 35
1K	-5617	-1119	46063	3	0.9027	1.0012	1.0012	--	--	0.01	--	0.28	Snell. 'zx'= 35
1L	-5617	-1119	43757	3	0.9027	1.0012	1.0012	--	--	0.01	--	0.27	Snell. 'zx'= 35
1Q	-4665	1061	48753	3	0.9027	1.0011	1.0010	--	--	0.01	--	0.29	Snell. 'zx'= 35
1R	-4665	1061	41067	3	0.9027	1.0011	1.0010	--	--	0.01	--	0.25	Snell. 'zx'= 35
1S	-4665	-1061	48753	3	0.9027	1.0011	1.0010	--	--	0.01	--	0.29	Snell. 'zx'= 35
1T	-4665	-1061	41067	3	0.9027	1.0011	1.0010	--	--	0.01	--	0.25	Snell. 'zx'= 35
2	-2566	369	44910	3	0.9027	1.0007	1.0006	--	--	0.00	--	0.24	Snell. 'zx'= 35
3	-1540	222	74020	3	0.9027	1.0009	1.0003	--	--	0.00	--	0.39	Snell. 'zx'= 35
4	-1540	222	105500	3	0.9027	1.0009	1.0003	--	--	0.00	--	0.55	Snell. 'zx'= 35
5	-2566	369	81900	3	0.9027	1.0007	1.0006	--	--	0.00	--	0.43	Snell. 'zx'= 35
7	-516	20	83050	3	0.9027	1.0031	1.0001	--	--	0.00	--	0.42	Snell. 'zx'= 35
20	-1543	25	67480	3	0.9027	1.0074	1.0003	--	--	0.00	--	0.35	Snell. 'zx'= 35

ASTA NUM. 15 NI 22 NF 7 Lungh. 240.0 cm SEZ. 1 Ps HEB 600

categoria: p.p. y Permanente Congresso Neve qy tot.
qy medio: 211.95 1443.00 975.00 195.00 2824.95 kg/m

Sollecitazioni di calcolo e di verifica

Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
--	cm	kg	kg	kg	kg*m	kg*m	kg*m					
1A	0	-7504	7934	949	0	1587	25815	3	0.04	0.01	0.19	
1B	0	-7504	8280	949	0	1587	24645	3	0.04	0.01	0.18	
1C	0	-7504	7934	-949	0	-1587	25815	3	0.04	0.01	0.19	
1D	0	-7504	8280	-949	0	-1587	24645	3	0.04	0.01	0.18	
1E	0	7504	7934	949	0	1587	25815	1	0.04	0.01	0.12	
1F	0	7504	8280	949	0	1587	24645	1	0.04	0.01	0.11	
1G	0	7504	7934	-949	0	-1587	25815	1	0.04	0.01	0.12	

1H	0	7504	8280	-949	0	-1587	24645	1	0.04	0.01	0.11	
1J	0	-3716	7934	361	0	601	25815	3	0.04	0.00	0.15	
1K	0	-3716	8280	361	0	601	24645	3	0.04	0.00	0.15	
1L	0	-3716	7934	-361	0	-601	25815	3	0.04	0.00	0.15	
1M	0	-3716	8280	-361	0	-601	24645	3	0.04	0.00	0.15	
1N	0	3716	7934	361	0	601	25815	1	0.04	0.00	0.12	
1O	0	3716	8280	361	0	601	24645	1	0.04	0.00	0.11	
1P	0	3716	7934	-361	0	-601	25815	1	0.04	0.00	0.12	
1Q	0	3716	8280	-361	0	-601	24645	1	0.04	0.00	0.11	
1R	0	-2589	7532	302	0	505	27181	3	0.03	0.00	0.16	
1S	0	-2589	8682	302	0	505	23279	3	0.04	0.00	0.14	
1T	0	-2589	7532	-302	0	-505	27181	3	0.03	0.00	0.16	
1U	0	-2589	8682	-302	0	-505	23279	3	0.04	0.00	0.14	
1V	0	2589	7532	302	0	505	27181	1	0.03	0.00	0.12	
1W	0	2589	8682	302	0	505	23279	1	0.04	0.00	0.11	
1X	0	2589	7532	-302	0	-505	27181	1	0.03	0.00	0.12	
2	0	2589	8682	-302	0	-505	23279	1	0.04	0.00	0.11	
3	0	-1262	8107	246	0	-236	25230	3	0.04	0.00	0.14	
4	0	-757	13360	147	0	-141	41600	3	0.06	0.00	0.22	
5	0	-757	19040	147	0	-141	59310	3	0.09	0.00	0.31	
7	0	-1262	14780	246	0	-236	46030	3	0.07	0.00	0.24	
20	0	527	14230	-14	0	-18	42960	1	0.06	0.00	0.19	
22	0	-2614	11760	-17	0	-18	39380	3	0.05	0.00	0.20	
		1743	-121	11	0	12	1473	1	0.00	0.00	0.01	
1A	120	-7504	5948	949	0	435	34555	3	0.03	0.01	0.20	
1B	120	-7504	6294	949	0	435	32978	3	0.03	0.01	0.19	
1C	120	-7504	5948	-949	0	-435	34555	3	0.03	0.01	0.20	
1D	120	-7504	6294	-949	0	-435	32978	3	0.03	0.01	0.19	
1E	120	7504	5948	949	0	435	34555	1	0.03	0.01	0.16	
1F	120	7504	6294	949	0	435	32978	1	0.03	0.01	0.15	
1G	120	7504	5948	-949	0	-435	34555	1	0.03	0.01	0.16	
1H	120	7504	6294	-949	0	-435	32978	1	0.03	0.01	0.15	
1I	120	-3716	5948	361	0	163	34555	3	0.03	0.00	0.19	
1J	120	-3716	6294	361	0	163	32978	3	0.03	0.00	0.18	
1K	120	-3716	5948	-361	0	-163	34555	3	0.03	0.00	0.19	
1L	120	-3716	6294	-361	0	-163	32978	3	0.03	0.00	0.18	
1M	120	-3716	5948	361	0	163	34555	1	0.03	0.00	0.16	
1N	120	-3716	6294	361	0	163	32978	1	0.03	0.00	0.15	
1O	120	-3716	5948	-361	0	-163	34555	1	0.03	0.00	0.16	
1P	120	-3716	6294	-361	0	-163	32978	1	0.03	0.00	0.15	
1Q	120	-2589	5546	302	0	138	36396	3	0.03	0.00	0.19	
1R	120	-2589	6696	302	0	138	31137	3	0.03	0.00	0.17	
1S	120	-2589	5546	-302	0	-138	36396	3	0.03	0.00	0.19	
1T	120	-2589	6696	-302	0	-138	31137	3	0.03	0.00	0.17	
1U	120	2589	5546	302	0	138	36396	1	0.03	0.00	0.16	
1V	120	2589	6696	302	0	138	31137	1	0.03	0.00	0.14	
1W	120	2589	5546	-302	0	-138	36396	1	0.03	0.00	0.16	
1X	120	2589	6696	-302	0	-138	31137	1	0.03	0.00	0.14	
2	120	-1262	6121	-230	0	-245	33767	3	0.03	0.00	0.18	
3	120	-757	10081	-138	0	-147	55662	3	0.05	0.00	0.29	
4	120	-757	14357	-138	0	-147	79345	3	0.07	0.00	0.41	
5	120	-1262	11150	-230	0	-245	61588	3	0.05	0.00	0.32	
7	120	527	11302	-14	0	-2	58282	1	0.05	0.00	0.26	
20	120	-2614	8832	-17	0	2	51737	3	0.04	0.00	0.27	
22	120	1743	-121	11	0	-1	1328	1	0.00	0.00	0.01	
1A	240	-7504	3962	949	0	-718	40912	3	0.02	0.01	0.24	
1B	240	-7504	4308	949	0	-718	38928	3	0.02	0.01	0.23	
1C	240	-7504	3962	-949	0	718	40912	3	0.02	0.01	0.24	
1D	240	-7504	4308	-949	0	718	38928	3	0.02	0.01	0.23	
1E	240	7504	3962	949	0	-718	40912	1	0.02	0.01	0.18	
1F	240	7504	4308	949	0	-718	38928	1	0.02	0.01	0.18	
1G	240	7504	3962	-949	0	718	40912	1	0.02	0.01	0.18	
1H	240	7504	4308	-949	0	718	38928	1	0.02	0.01	0.18	
1I	240	-3716	3962	361	0	-275	40912	3	0.02	0.00	0.22	
1J	240	-3716	4308	361	0	-275	38928	3	0.02	0.00	0.21	
1K	240	-3716	3962	-361	0	275	40912	3	0.02	0.00	0.22	
1L	240	-3716	4308	-361	0	275	38928	3	0.02	0.00	0.21	
1M	240	-3716	3962	361	0	-275	40912	1	0.02	0.00	0.18	
1N	240	-3716	4308	361	0	-275	38928	1	0.02	0.00	0.18	
1O	240	-3716	3962	-361	0	275	40912	1	0.02	0.00	0.18	
1P	240	-3716	4308	-361	0	275	38928	1	0.02	0.00	0.18	
1Q	240	-2589	3560	302	0	-229	43228	3	0.02	0.00	0.23	
1R	240	-2589	4710	302	0	-229	36612	3	0.02	0.00	0.20	
1S	240	-2589	3560	-302	0	229	43228	3	0.02	0.00	0.23	
1T	240	-2589	4710	-302	0	229	36612	3	0.02	0.00	0.20	
1U	240	2589	3560	302	0	-229	43228	1	0.02	0.00	0.20	
1V	240	2589	4710	302	0	-229	36612	1	0.02	0.00	0.17	
1W	240	2589	3560	-302	0	229	43228	1	0.02	0.00	0.20	
1X	240	2589	4710	-302	0	229	36612	1	0.02	0.00	0.17	
2	240	-1262	4135	-705	0	316	39920	3	0.02	0.00	0.21	
3	240	-757	6802	-423	0	190	65790	3	0.03	0.00	0.34	
4	240	-757	9674	-423	0	190	93760	3	0.04	0.00	0.48	
5	240	-1262	7520	-705	0	316	72790	3	0.03	0.00	0.38	
7	240	527	8374	-14	0	14	70090	1	0.04	0.00	0.32	
20	240	-2614	5903	-17	0	23	60580	3	0.03	0.00	0.31	
22	240	1743	-121	11	0	-15	1184	1	0.00	0.00	0.01	

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	γ_{min}	ky	kz	kLT	χ_{LT}	I.S.n.	I.S.m.	I.S.	Nota
	kg	kg*m											
1A	-7504	1587	40912	3	0.9066	0.9999	1.0012	--	--	0.01	--	0.27	Snell. 'zx' = 34
1B	-7504	1587	38928	3	0.9066	0.9999	1.0013	--	--	0.01	--	0.26	Snell. 'zx' = 34

1C	-7504	-1587	40912	3	0.9066	0.9999	1.0012	--	--	0.01	--	0.27	Snell.	'zx'=' 34
1D	-7504	-1587	38928	3	0.9066	0.9999	1.0013	--	--	0.01	--	0.26	Snell.	'zx'=' 34
1I	-3716	601	40912	3	0.9066	1.0006	1.0006	--	--	0.00	--	0.23	Snell.	'zx'=' 34
1J	-3716	601	38928	3	0.9066	1.0006	1.0006	--	--	0.00	--	0.22	Snell.	'zx'=' 34
1K	-3716	-601	40912	3	0.9066	1.0006	1.0006	--	--	0.00	--	0.23	Snell.	'zx'=' 34
1L	-3716	-601	38928	3	0.9066	1.0006	1.0006	--	--	0.00	--	0.22	Snell.	'zx'=' 34
1Q	-2589	505	43228	3	0.9066	1.0005	1.0004	--	--	0.00	--	0.24	Snell.	'zx'=' 34
1R	-2589	505	36612	3	0.9066	1.0005	1.0004	--	--	0.00	--	0.21	Snell.	'zx'=' 34
1S	-2589	-505	43228	3	0.9066	1.0005	1.0004	--	--	0.00	--	0.24	Snell.	'zx'=' 34
1T	-2589	-505	36612	3	0.9066	1.0005	1.0004	--	--	0.00	--	0.21	Snell.	'zx'=' 34
2	-1262	316	39920	3	0.9066	1.0003	1.0002	--	--	0.00	--	0.21	Snell.	'zx'=' 34
3	-757	190	65790	3	0.9066	1.0004	1.0001	--	--	0.00	--	0.34	Snell.	'zx'=' 34
4	-757	190	93760	3	0.9066	1.0004	1.0001	--	--	0.00	--	0.48	Snell.	'zx'=' 34
5	-1262	316	72790	3	0.9066	1.0003	1.0002	--	--	0.00	--	0.38	Snell.	'zx'=' 34
20	-2614	23	60580	3	0.9066	1.0188	1.0004	--	--	0.00	--	0.31	Snell.	'zx'=' 34

ASTA NUM. 16 NI 25 NF 9 Lunghezza 240.0 cm SEZ. 1 Ps HEB 600

categoria: p.p. y Permanente Congresso Neve qy tot.
 qy medio: 211.95 1443.00 975.00 195.00 2824.95 kg/m

Sollecitazioni di calcolo e di verifica Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
--	cm	kg			kg*m							
1A	0	-8492	7934	1152	0	1983	25815	3	0.04	0.01	0.20	
1B	0	-8492	8280	1152	0	1983	24645	3	0.04	0.01	0.20	
1C	0	-8492	7934	-1152	0	-1983	25815	3	0.04	0.01	0.20	
1D	0	-8492	8280	-1152	0	-1983	24645	3	0.04	0.01	0.20	
1E	0	8492	7934	1152	0	1983	25815	1	0.04	0.01	0.12	
1F	0	8492	8280	1152	0	1983	24645	1	0.04	0.01	0.11	
1G	0	8492	7934	-1152	0	-1983	25815	1	0.04	0.01	0.12	
1H	0	8492	8280	-1152	0	-1983	24645	1	0.04	0.01	0.11	
1I	0	-6081	7934	372	0	644	25815	3	0.04	0.01	0.16	
1J	0	-6081	8280	372	0	644	24645	3	0.04	0.01	0.15	
1K	0	-6081	7934	-372	0	-644	25815	3	0.04	0.01	0.16	
1L	0	-6081	8280	-372	0	-644	24645	3	0.04	0.01	0.15	
1M	0	6081	7934	372	0	644	25815	1	0.04	0.01	0.12	
1N	0	6081	8280	372	0	644	24645	1	0.04	0.01	0.11	
1O	0	6081	7934	-372	0	-644	25815	1	0.04	0.01	0.12	
1P	0	6081	8280	-372	0	-644	24645	1	0.04	0.01	0.11	
1Q	0	-3363	7532	352	0	606	27181	3	0.03	0.00	0.16	
1R	0	-3363	8682	352	0	606	23279	3	0.04	0.00	0.14	
1S	0	-3363	7532	-352	0	-606	27181	3	0.03	0.00	0.16	
1T	0	-3363	8682	-352	0	-606	23279	3	0.04	0.00	0.14	
1U	0	3363	7532	352	0	606	27181	1	0.03	0.00	0.12	
1V	0	3363	8682	352	0	606	23279	1	0.04	0.00	0.11	
1W	0	3363	7532	-352	0	-606	27181	1	0.03	0.00	0.12	
1X	0	3363	8682	-352	0	-606	23279	1	0.04	0.00	0.11	
2	0	1331	8107	-326	0	-601	25230	1	0.04	0.00	0.11	
3	0	799	13360	-196	0	-360	41600	1	0.06	0.00	0.19	
4	0	799	19040	-196	0	-360	59310	1	0.09	0.00	0.27	
5	0	1331	14780	-326	0	-601	46030	1	0.07	0.00	0.21	
7	0	-538	17430	3	0	13	50820	3	0.08	0.00	0.26	
20	0	-8106	11510	4	0	18	42430	3	0.05	0.01	0.23	
22	0	5404	-288	-3	0	-12	3507	1	0.00	0.01	0.02	
1A	120	-8492	5948	1152	0	589	34555	3	0.03	0.01	0.20	
1B	120	-8492	6294	1152	0	589	32978	3	0.03	0.01	0.20	
1C	120	-8492	5948	-1152	0	-589	34555	3	0.03	0.01	0.20	
1D	120	-8492	6294	-1152	0	-589	32978	3	0.03	0.01	0.20	
1E	120	8492	5948	1152	0	589	34555	1	0.03	0.01	0.16	
1F	120	8492	6294	1152	0	589	32978	1	0.03	0.01	0.15	
1G	120	8492	5948	-1152	0	-589	34555	1	0.03	0.01	0.16	
1H	120	8492	6294	-1152	0	-589	32978	1	0.03	0.01	0.15	
1I	120	-6081	5948	372	0	186	34555	3	0.03	0.01	0.19	
1J	120	-6081	6294	372	0	186	32978	3	0.03	0.01	0.18	
1K	120	-6081	5948	-372	0	-186	34555	3	0.03	0.01	0.19	
1L	120	-6081	6294	-372	0	-186	32978	3	0.03	0.01	0.18	
1M	120	6081	5948	372	0	186	34555	1	0.03	0.01	0.16	
1N	120	6081	6294	372	0	186	32978	1	0.03	0.01	0.15	
1O	120	6081	5948	-372	0	-186	34555	1	0.03	0.01	0.16	
1P	120	6081	6294	-372	0	-186	32978	1	0.03	0.01	0.15	
1Q	120	-3363	5546	352	0	179	36396	3	0.03	0.00	0.19	
1R	120	-3363	6696	352	0	179	31137	3	0.03	0.00	0.17	
1S	120	-3363	5546	-352	0	-179	36396	3	0.03	0.00	0.19	
1T	120	-3363	6696	-352	0	-179	31137	3	0.03	0.00	0.17	
1U	120	3363	5546	352	0	179	36396	1	0.03	0.00	0.16	
1V	120	3363	6696	352	0	179	31137	1	0.03	0.00	0.14	
1W	120	3363	5546	-352	0	-179	36396	1	0.03	0.00	0.16	
1X	120	3363	6696	-352	0	-179	31137	1	0.03	0.00	0.14	
2	120	1331	6121	-326	0	-209	33767	1	0.03	0.00	0.15	
3	120	799	10081	-196	0	-126	55662	1	0.05	0.00	0.25	
4	120	799	14357	-196	0	-126	79345	1	0.07	0.00	0.36	
5	120	1331	11150	-326	0	-209	61588	1	0.05	0.00	0.28	
7	120	-538	14500	3	0	9	69972	3	0.07	0.00	0.36	
20	120	-8106	8582	4	0	13	54482	3	0.04	0.01	0.29	
22	120	5404	-288	-3	0	-9	3162	1	0.00	0.01	0.01	
1A	240	-8492	3962	1152	0	-805	40912	3	0.02	0.01	0.24	
1B	240	-8492	4308	1152	0	-805	38928	3	0.02	0.01	0.23	
1C	240	-8492	3962	-1152	0	805	40912	3	0.02	0.01	0.24	
1D	240	-8492	4308	-1152	0	805	38928	3	0.02	0.01	0.23	
1E	240	8492	3962	1152	0	-805	40912	1	0.02	0.01	0.18	
1F	240	8492	4308	1152	0	-805	38928	1	0.02	0.01	0.18	
1G	240	8492	3962	-1152	0	805	40912	1	0.02	0.01	0.18	
1H	240	8492	4308	-1152	0	805	38928	1	0.02	0.01	0.18	
1I	240	-6081	3962	372	0	-272	40912	3	0.02	0.01	0.22	

1J	240	-6081	4308	372	0	-272	38928	3	0.02	0.01	0.21	
1K	240	-6081	3962	-372	0	272	40912	3	0.02	0.01	0.22	
1L	240	-6081	4308	-372	0	272	38928	3	0.02	0.01	0.21	
1M	240	6081	3962	372	0	-272	40912	1	0.02	0.01	0.18	
1N	240	6081	4308	372	0	-272	38928	1	0.02	0.01	0.18	
1O	240	6081	3962	-372	0	272	40912	1	0.02	0.01	0.18	
1P	240	6081	4308	-372	0	272	38928	1	0.02	0.01	0.18	
1Q	240	-3363	3560	352	0	-248	43228	3	0.02	0.00	0.23	
1R	240	-3363	4710	352	0	-248	36612	3	0.02	0.00	0.20	
1S	240	-3363	3560	-352	0	248	43228	3	0.02	0.00	0.23	
1T	240	-3363	4710	-352	0	248	36612	3	0.02	0.00	0.20	
1U	240	3363	3560	352	0	-248	43228	1	0.02	0.00	0.20	
1V	240	3363	4710	352	0	-248	36612	1	0.02	0.00	0.17	
1W	240	3363	3560	-352	0	248	43228	1	0.02	0.00	0.20	
1X	240	3363	4710	-352	0	248	36612	1	0.02	0.00	0.17	
2	240	1331	4135	-326	0	182	39920	1	0.02	0.00	0.18	
3	240	799	6802	-196	0	109	65790	1	0.03	0.00	0.30	
4	240	799	9674	-196	0	109	93760	1	0.04	0.00	0.42	
5	240	1331	7520	-326	0	182	72790	1	0.03	0.00	0.33	
7	240	-538	11570	3	0	5	85610	3	0.05	0.00	0.44	
20	240	-8106	5653	4	0	8	63020	3	0.03	0.01	0.33	
22	240	5404	-288	-3	0	-5	2816	1	0.00	0.01	0.01	

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	$\gamma_{min.}$	ky	kz	kLT	χ_{LT}	I.S.n.	I.S.m.	I.S.	Nota
	kg	kg*m											
1A	-8492	1983	40912	3	0.9066	0.9993	1.0014	--	--	0.01	--	0.28	Snell. 'zx'= 34
1B	-8492	1983	38928	3	0.9066	0.9993	1.0014	--	--	0.01	--	0.27	Snell. 'zx'= 34
1C	-8492	-1983	40912	3	0.9066	0.9993	1.0014	--	--	0.01	--	0.28	Snell. 'zx'= 34
1D	-8492	-1983	38928	3	0.9066	0.9993	1.0014	--	--	0.01	--	0.27	Snell. 'zx'= 34
1I	-6081	644	40912	3	0.9066	0.9994	1.0010	--	--	0.01	--	0.24	Snell. 'zx'= 34
1J	-6081	644	38928	3	0.9066	0.9994	1.0010	--	--	0.01	--	0.23	Snell. 'zx'= 34
1K	-6081	-644	40912	3	0.9066	0.9994	1.0010	--	--	0.01	--	0.24	Snell. 'zx'= 34
1L	-6081	-644	38928	3	0.9066	0.9994	1.0010	--	--	0.01	--	0.23	Snell. 'zx'= 34
1Q	-3363	606	43228	3	0.9066	0.9997	1.0006	--	--	0.00	--	0.24	Snell. 'zx'= 34
1R	-3363	606	36612	3	0.9066	0.9997	1.0006	--	--	0.00	--	0.21	Snell. 'zx'= 34
1S	-3363	-606	43228	3	0.9066	0.9997	1.0006	--	--	0.00	--	0.24	Snell. 'zx'= 34
1T	-3363	-606	36612	3	0.9066	0.9997	1.0006	--	--	0.00	--	0.21	Snell. 'zx'= 34
7	-538	13	85610	3	0.9066	1.0003	1.0001	--	--	0.00	--	0.44	Snell. 'zx'= 34
20	-8106	18	63020	3	0.9066	1.0041	1.0014	--	--	0.01	--	0.33	Snell. 'zx'= 34

AMV s.r.l.
Via San Lorenzo, 106 Tel. 0481/779903
34077 Ronchi dei Legionari (GO)

Lavoro: **Struttura R01** Intestazione lavoro:
Elemento: **TRAVE** Metodo di verifica: **Eurocodice 3 - NTC 2018**
Gruppo: **2** Descrizione: **Controventi di piano**
Tabella: **Controventi** Struttura: **Nuova**
Tipo acciaio: **S 355**
Tipologia sismica: **Senza prescrizioni aggiuntive**
 γ_{M0} : **1.050** γ_{M1} : **1.050** γ_{M1} ': **1.050** γ_{M2} : **1.250** γ_{rv} : **0.000** γ_{M0} Pf: **1.000** γ_{M1} Pf: **1.000**
Tipo collegamento: **saldato** Connessione su un solo lato Connessione sul lato corto (solo 'L')

ASTA NUM. 1 NI 1 NF 9 Lungh. 626.3 cm SEZ. 3 Rp B= 0.060 H= 0.010 m
Sollecitazioni di calcolo e di verifica Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
--	cm	kg			kg*m							
1A	0	-9682	0	0	0	0	0	1	0.00	0.50	0.00	
1B	0	-9682	0	0	0	0	0	1	0.00	0.50	0.00	
1C	0	-9682	0	-0	0	-0	0	1	0.00	0.50	0.00	
1D	0	-9682	0	-0	0	-0	0	1	0.00	0.50	0.00	
1E	0	9682	0	0	0	0	0	1	0.00	0.50	0.00	
1F	0	9682	0	0	0	0	0	1	0.00	0.50	0.00	
1G	0	9682	0	-0	0	-0	0	1	0.00	0.50	0.00	
1H	0	9682	0	-0	0	-0	0	1	0.00	0.50	0.00	
1I	0	-5689	0	0	0	0	0	1	0.00	0.29	0.00	
1J	0	-5689	0	0	0	0	0	1	0.00	0.29	0.00	
1K	0	-5689	0	-0	0	-0	0	1	0.00	0.29	0.00	
1L	0	-5689	0	-0	0	-0	0	1	0.00	0.29	0.00	
1M	0	5689	0	0	0	0	0	1	0.00	0.29	0.00	
1N	0	5689	0	0	0	0	0	1	0.00	0.29	0.00	
1O	0	5689	0	-0	0	-0	0	1	0.00	0.29	0.00	
1P	0	5689	0	-0	0	-0	0	1	0.00	0.29	0.00	
1Q	0	-3547	0	0	0	0	0	1	0.00	0.18	0.00	
1R	0	-3547	0	0	0	0	0	1	0.00	0.18	0.00	
1S	0	-3547	0	-0	0	-0	0	1	0.00	0.18	0.00	
1T	0	-3547	0	-0	0	-0	0	1	0.00	0.18	0.00	
1U	0	3547	0	0	0	0	0	1	0.00	0.18	0.00	
1V	0	3547	0	0	0	0	0	1	0.00	0.18	0.00	
1W	0	3547	0	-0	0	-0	0	1	0.00	0.18	0.00	
1X	0	3547	0	-0	0	-0	0	1	0.00	0.18	0.00	
2	0	1564	0	0	0	0	0	1	0.00	0.08	0.00	
3	0	938	0	0	0	0	0	1	0.00	0.05	0.00	
4	0	938	0	0	0	0	0	1	0.00	0.05	0.00	
5	0	1564	0	0	0	0	0	1	0.00	0.08	0.00	
7	0	-662	0	0	0	0	0	1	0.00	0.03	0.00	
20	0	-719	0	0	0	0	0	1	0.00	0.04	0.00	
22	0	479	0	-0	0	0	0	1	0.00	0.02	0.00	
1A	313	-9682	0	0	0	0	-0	1	0.00	0.50	0.00	
1B	313	-9682	0	0	0	0	0	1	0.00	0.50	0.00	
1C	313	-9682	0	-0	0	-0	-0	1	0.00	0.50	0.00	
1D	313	-9682	0	-0	0	-0	0	1	0.00	0.50	0.00	
1E	313	9682	0	0	0	0	-0	1	0.00	0.50	0.00	
1F	313	9682	0	0	0	0	0	1	0.00	0.50	0.00	
1G	313	9682	0	-0	0	-0	-0	1	0.00	0.50	0.00	
1H	313	9682	0	-0	0	-0	0	1	0.00	0.50	0.00	
1I	313	-5689	0	0	0	0	-0	1	0.00	0.29	0.00	
1J	313	-5689	0	0	0	0	0	1	0.00	0.29	0.00	
1K	313	-5689	0	-0	0	-0	-0	1	0.00	0.29	0.00	
1L	313	-5689	0	-0	0	-0	0	1	0.00	0.29	0.00	
1M	313	5689	0	0	0	0	-0	1	0.00	0.29	0.00	
1N	313	5689	0	0	0	0	0	1	0.00	0.29	0.00	
1O	313	5689	0	-0	0	-0	-0	1	0.00	0.29	0.00	
1P	313	5689	0	-0	0	-0	0	1	0.00	0.29	0.00	
1Q	313	-3547	0	0	0	0	-0	1	0.00	0.18	0.00	
1R	313	-3547	0	0	0	0	0	1	0.00	0.18	0.00	
1S	313	-3547	0	-0	0	-0	-0	1	0.00	0.18	0.00	
1T	313	-3547	0	-0	0	-0	0	1	0.00	0.18	0.00	
1U	313	3547	0	0	0	0	-0	1	0.00	0.18	0.00	
1V	313	3547	0	0	0	0	0	1	0.00	0.18	0.00	
1W	313	3547	0	-0	0	-0	-0	1	0.00	0.18	0.00	
1X	313	3547	0	-0	0	-0	0	1	0.00	0.18	0.00	
2	313	1564	0	0	0	0	0	1	0.00	0.08	0.00	
3	313	938	0	0	0	0	0	1	0.00	0.05	0.00	
4	313	938	0	0	0	0	0	1	0.00	0.05	0.00	
5	313	1564	0	0	0	0	0	1	0.00	0.08	0.00	
7	313	-662	0	0	0	0	0	1	0.00	0.03	0.00	
20	313	-719	0	0	0	0	0	1	0.00	0.04	0.00	
22	313	479	0	-0	0	0	0	1	0.00	0.02	0.00	
1A	626	-9682	0	0	0	0	-0	1	0.00	0.50	0.00	
1B	626	-9682	0	0	0	0	0	1	0.00	0.50	0.00	
1C	626	-9682	0	-0	0	0	-0	1	0.00	0.50	0.00	
1D	626	-9682	0	-0	0	0	0	1	0.00	0.50	0.00	
1E	626	9682	0	0	0	0	-0	1	0.00	0.50	0.00	
1F	626	9682	0	0	0	0	0	1	0.00	0.50	0.00	
1G	626	9682	0	-0	0	0	-0	1	0.00	0.50	0.00	
1H	626	9682	0	-0	0	0	0	1	0.00	0.50	0.00	
1I	626	-5689	0	0	0	0	-0	1	0.00	0.29	0.00	
1J	626	-5689	0	0	0	0	0	1	0.00	0.29	0.00	
1K	626	-5689	0	-0	0	0	-0	1	0.00	0.29	0.00	
1L	626	-5689	0	-0	0	0	0	1	0.00	0.29	0.00	
1M	626	5689	0	0	0	0	-0	1	0.00	0.29	0.00	

1N	626	5689	0	0	0	0	0	1	0.00	0.29	0.00
1O	626	5689	0	-0	0	0	-0	1	0.00	0.29	0.00
1P	626	5689	0	-0	0	0	0	1	0.00	0.29	0.00
1Q	626	-3547	0	0	0	0	-0	1	0.00	0.18	0.00
1R	626	-3547	0	0	0	0	0	1	0.00	0.18	0.00
1S	626	-3547	0	-0	0	0	-0	1	0.00	0.18	0.00
1T	626	-3547	0	-0	0	0	0	1	0.00	0.18	0.00
1U	626	3547	0	0	0	0	-0	1	0.00	0.18	0.00
1V	626	3547	0	0	0	0	0	1	0.00	0.18	0.00
1W	626	3547	0	-0	0	0	-0	1	0.00	0.18	0.00
1X	626	3547	0	-0	0	0	0	1	0.00	0.18	0.00
2	626	1564	0	0	0	0	0	1	0.00	0.08	0.00
3	626	938	0	0	0	0	0	1	0.00	0.05	0.00
4	626	938	0	0	0	0	0	1	0.00	0.05	0.00
5	626	1564	0	0	0	0	0	1	0.00	0.08	0.00
7	626	-662	0	0	0	0	0	1	0.00	0.03	0.00
20	626	-719	0	0	0	0	0	1	0.00	0.04	0.00
22	626	479	0	-0	0	0	0	1	0.00	0.02	0.00

ASTA NUM. 2 NI 9 NF 8 Lungh. 626.3 cm SEZ. 3 Rp B= 0.060 H= 0.010 m
Sollecitazioni di calcolo e di verifica Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
---	---	---	---	---	---	---	---	---	---	---	---	---
	cm	kg			kg*m							
1A	0	-1520	-0	0	0	0	0	1	0.00	0.08	0.00	
1B	0	-1520	0	0	0	0	0	1	0.00	0.08	0.00	
1C	0	-1520	-0	-0	0	-0	0	1	0.00	0.08	0.00	
1D	0	-1520	0	-0	0	0	-0	1	0.00	0.08	0.00	
1E	0	1520	-0	0	0	0	0	1	0.00	0.08	0.00	
1F	0	1520	0	0	0	0	0	1	0.00	0.08	0.00	
1G	0	1520	-0	-0	0	-0	0	1	0.00	0.08	0.00	
1H	0	1520	0	-0	0	-0	0	1	0.00	0.08	0.00	
1I	0	-3295	-0	0	0	0	0	1	0.00	0.17	0.00	
1J	0	-3295	0	0	0	0	0	1	0.00	0.17	0.00	
1K	0	-3295	-0	-0	0	-0	0	1	0.00	0.17	0.00	
1L	0	-3295	0	-0	0	-0	0	1	0.00	0.17	0.00	
1M	0	3295	-0	0	0	0	0	1	0.00	0.17	0.00	
1N	0	3295	0	0	0	0	0	1	0.00	0.17	0.00	
1O	0	3295	-0	-0	0	-0	0	1	0.00	0.17	0.00	
1P	0	3295	0	-0	0	-0	0	1	0.00	0.17	0.00	
1Q	0	-1111	-0	0	0	0	0	1	0.00	0.06	0.00	
1R	0	-1111	0	0	0	0	0	1	0.00	0.06	0.00	
1S	0	-1111	-0	-0	0	-0	0	1	0.00	0.06	0.00	
1T	0	-1111	0	-0	0	-0	0	1	0.00	0.06	0.00	
1U	0	1111	-0	0	0	0	0	1	0.00	0.06	0.00	
1V	0	1111	0	0	0	0	0	1	0.00	0.06	0.00	
1W	0	1111	-0	-0	0	-0	0	1	0.00	0.06	0.00	
1X	0	1111	0	-0	0	-0	0	1	0.00	0.06	0.00	
2	0	2	0	0	0	0	0	1	0.00	0.00	0.00	
3	0	1	0	0	0	0	0	1	0.00	0.00	0.00	
4	0	1	0	0	0	0	0	1	0.00	0.00	0.00	
5	0	2	0	0	0	0	0	1	0.00	0.00	0.00	
7	0	651	-0	0	0	0	0	1	0.00	0.03	0.00	
20	0	606	-0	0	0	0	0	1	0.00	0.03	0.00	
22	0	-404	-0	-0	0	0	0	1	0.00	0.02	0.00	
1A	313	-1520	-0	0	0	0	-0	1	0.00	0.08	0.00	
1B	313	-1520	0	0	0	0	0	1	0.00	0.08	0.00	
1C	313	-1520	-0	-0	0	-0	-0	1	0.00	0.08	0.00	
1D	313	-1520	0	-0	0	-0	0	1	0.00	0.08	0.00	
1E	313	1520	-0	0	0	0	-0	1	0.00	0.08	0.00	
1F	313	1520	0	0	0	0	0	1	0.00	0.08	0.00	
1G	313	1520	-0	-0	0	-0	-0	1	0.00	0.08	0.00	
1H	313	1520	0	-0	0	-0	0	1	0.00	0.08	0.00	
1I	313	-3295	-0	0	0	0	-0	1	0.00	0.17	0.00	
1J	313	-3295	0	0	0	0	0	1	0.00	0.17	0.00	
1K	313	-3295	-0	-0	0	-0	-0	1	0.00	0.17	0.00	
1L	313	-3295	0	-0	0	-0	0	1	0.00	0.17	0.00	
1M	313	3295	-0	0	0	0	-0	1	0.00	0.17	0.00	
1N	313	3295	0	0	0	0	0	1	0.00	0.17	0.00	
1O	313	3295	-0	-0	0	-0	-0	1	0.00	0.17	0.00	
1P	313	3295	0	-0	0	-0	0	1	0.00	0.17	0.00	
1Q	313	-1111	-0	0	0	0	-0	1	0.00	0.06	0.00	
1R	313	-1111	0	0	0	0	0	1	0.00	0.06	0.00	
1S	313	-1111	-0	-0	0	-0	-0	1	0.00	0.06	0.00	
1T	313	-1111	0	-0	0	-0	0	1	0.00	0.06	0.00	
1U	313	1111	-0	0	0	0	-0	1	0.00	0.06	0.00	
1V	313	1111	0	0	0	0	0	1	0.00	0.06	0.00	
1W	313	1111	-0	-0	0	-0	-0	1	0.00	0.06	0.00	
1X	313	1111	0	-0	0	-0	0	1	0.00	0.06	0.00	
2	313	2	0	0	0	0	0	1	0.00	0.00	0.00	
3	313	1	0	0	0	0	0	1	0.00	0.00	0.00	
4	313	1	0	0	0	0	0	1	0.00	0.00	0.00	
5	313	2	0	0	0	0	0	1	0.00	0.00	0.00	
7	313	651	-0	0	0	0	0	1	0.00	0.03	0.00	
20	313	606	-0	0	0	0	0	1	0.00	0.03	0.00	
22	313	-404	-0	-0	0	0	0	1	0.00	0.02	0.00	
1A	626	-1520	-0	0	0	0	-0	1	0.00	0.08	0.00	
1B	626	-1520	0	0	0	0	0	1	0.00	0.08	0.00	
1C	626	-1520	-0	-0	0	0	-0	1	0.00	0.08	0.00	
1D	626	-1520	0	-0	0	0	0	1	0.00	0.08	0.00	
1E	626	1520	-0	0	0	0	-0	1	0.00	0.08	0.00	
1F	626	1520	0	0	0	0	0	1	0.00	0.08	0.00	
1G	626	1520	-0	-0	0	0	-0	1	0.00	0.08	0.00	
1H	626	1520	0	-0	0	0	0	1	0.00	0.08	0.00	
1I	626	-3295	-0	0	0	0	-0	1	0.00	0.17	0.00	

1J	626	-3295	0	0	0	0	0	1	0.00	0.17	0.00
1K	626	-3295	-0	-0	0	0	-0	1	0.00	0.17	0.00
1L	626	-3295	0	-0	0	0	0	1	0.00	0.17	0.00
1M	626	3295	-0	0	0	0	-0	1	0.00	0.17	0.00
1N	626	3295	0	0	0	0	0	1	0.00	0.17	0.00
1O	626	3295	-0	-0	0	0	-0	1	0.00	0.17	0.00
1P	626	3295	0	-0	0	0	0	1	0.00	0.17	0.00
1Q	626	-1111	-0	0	0	0	-0	1	0.00	0.06	0.00
1R	626	-1111	0	0	0	0	0	1	0.00	0.06	0.00
1S	626	-1111	-0	-0	0	0	-0	1	0.00	0.06	0.00
1T	626	-1111	0	-0	0	0	0	1	0.00	0.06	0.00
1U	626	1111	-0	0	0	0	-0	1	0.00	0.06	0.00
1V	626	1111	0	0	0	0	0	1	0.00	0.06	0.00
1W	626	1111	-0	-0	0	0	-0	1	0.00	0.06	0.00
1X	626	1111	0	-0	0	0	0	1	0.00	0.06	0.00
2	626	2	0	0	0	0	0	1	0.00	0.00	0.00
3	626	1	0	0	0	0	0	1	0.00	0.00	0.00
4	626	1	0	0	0	0	0	1	0.00	0.00	0.00
5	626	2	0	0	0	0	0	1	0.00	0.00	0.00
7	626	651	-0	0	0	0	0	1	0.00	0.03	0.00
20	626	606	-0	0	0	0	0	1	0.00	0.03	0.00
22	626	-404	-0	-0	0	0	0	1	0.00	0.02	0.00

ASTA NUM. 3 NI 8 NF 5 Lungh. 626.3 cm SEZ. 3 Rp B= 0.060 H= 0.010 m
 Sollecitazioni di calcolo e di verifica Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	cm	kg			kg*m							
1A	0	-10192	-0	0	0	0	0	1	0.00	0.52	0.00	
1B	0	-10192	0	0	0	0	-0	1	0.00	0.52	0.00	
1C	0	-10192	-0	-0	0	0	0	1	0.00	0.52	0.00	
1D	0	-10192	0	-0	0	0	-0	1	0.00	0.52	0.00	
1E	0	10192	-0	0	0	0	0	1	0.00	0.52	0.00	
1F	0	10192	0	0	0	0	-0	1	0.00	0.52	0.00	
1G	0	10192	-0	-0	0	0	0	1	0.00	0.52	0.00	
1H	0	10192	0	-0	0	0	-0	1	0.00	0.52	0.00	
1I	0	-6188	-0	0	0	0	0	1	0.00	0.32	0.00	
1J	0	-6188	0	0	0	0	-0	1	0.00	0.32	0.00	
1K	0	-6188	-0	-0	0	0	0	1	0.00	0.32	0.00	
1L	0	-6188	0	-0	0	0	-0	1	0.00	0.32	0.00	
1M	0	6188	-0	0	0	0	0	1	0.00	0.32	0.00	
1N	0	6188	0	0	0	0	-0	1	0.00	0.32	0.00	
1O	0	6188	-0	-0	0	0	0	1	0.00	0.32	0.00	
1P	0	6188	0	-0	0	0	-0	1	0.00	0.32	0.00	
1Q	0	-3780	-0	0	0	0	0	1	0.00	0.19	0.00	
1R	0	-3780	0	0	0	0	-0	1	0.00	0.19	0.00	
1S	0	-3780	-0	-0	0	0	0	1	0.00	0.19	0.00	
1T	0	-3780	0	-0	0	0	-0	1	0.00	0.19	0.00	
1U	0	3780	-0	0	0	0	0	1	0.00	0.19	0.00	
1V	0	3780	0	0	0	0	-0	1	0.00	0.19	0.00	
1W	0	3780	-0	-0	0	0	0	1	0.00	0.19	0.00	
1X	0	3780	0	-0	0	0	-0	1	0.00	0.19	0.00	
2	0	-1682	-0	0	0	0	0	1	0.00	0.09	0.00	
3	0	-1009	-0	0	0	0	0	1	0.00	0.05	0.00	
4	0	-1009	-0	0	0	0	0	1	0.00	0.05	0.00	
5	0	-1682	-0	0	0	0	0	1	0.00	0.09	0.00	
7	0	-763	-0	-0	0	0	0	1	0.00	0.04	0.00	
20	0	-766	-0	-0	0	0	0	1	0.00	0.04	0.00	
22	0	511	0	0	0	0	0	1	0.00	0.03	0.00	
1A	313	-10192	-0	0	0	-0	0	1	0.00	0.52	0.00	
1B	313	-10192	0	0	0	-0	-0	1	0.00	0.52	0.00	
1C	313	-10192	-0	-0	0	0	0	1	0.00	0.52	0.00	
1D	313	-10192	0	-0	0	0	-0	1	0.00	0.52	0.00	
1E	313	10192	-0	0	0	-0	0	1	0.00	0.52	0.00	
1F	313	10192	0	0	0	-0	-0	1	0.00	0.52	0.00	
1G	313	10192	-0	-0	0	0	0	1	0.00	0.52	0.00	
1H	313	10192	0	-0	0	0	-0	1	0.00	0.52	0.00	
1I	313	-6188	-0	0	0	-0	0	1	0.00	0.32	0.00	
1J	313	-6188	0	0	0	-0	-0	1	0.00	0.32	0.00	
1K	313	-6188	-0	-0	0	0	0	1	0.00	0.32	0.00	
1L	313	-6188	0	-0	0	0	-0	1	0.00	0.32	0.00	
1M	313	6188	-0	0	0	-0	0	1	0.00	0.32	0.00	
1N	313	6188	0	0	0	-0	-0	1	0.00	0.32	0.00	
1O	313	6188	-0	-0	0	0	0	1	0.00	0.32	0.00	
1P	313	6188	0	-0	0	0	-0	1	0.00	0.32	0.00	
1Q	313	-3780	-0	0	0	-0	0	1	0.00	0.19	0.00	
1R	313	-3780	0	0	0	-0	-0	1	0.00	0.19	0.00	
1S	313	-3780	-0	-0	0	0	0	1	0.00	0.19	0.00	
1T	313	-3780	0	-0	0	0	-0	1	0.00	0.19	0.00	
1U	313	3780	-0	0	0	-0	0	1	0.00	0.19	0.00	
1V	313	3780	0	0	0	-0	-0	1	0.00	0.19	0.00	
1W	313	3780	-0	-0	0	0	0	1	0.00	0.19	0.00	
1X	313	3780	0	-0	0	0	-0	1	0.00	0.19	0.00	
2	313	-1682	-0	0	0	0	0	1	0.00	0.09	0.00	
3	313	-1009	-0	0	0	0	0	1	0.00	0.05	0.00	
4	313	-1009	-0	0	0	0	0	1	0.00	0.05	0.00	
5	313	-1682	-0	0	0	0	0	1	0.00	0.09	0.00	
7	313	-763	-0	-0	0	0	0	1	0.00	0.04	0.00	
20	313	-766	-0	-0	0	0	0	1	0.00	0.04	0.00	
22	313	511	0	0	0	0	0	1	0.00	0.03	0.00	
1A	626	-10192	-0	0	0	-0	0	1	0.00	0.52	0.00	
1B	626	-10192	0	0	0	-0	0	1	0.00	0.52	0.00	
1C	626	-10192	-0	-0	0	0	0	1	0.00	0.52	0.00	
1D	626	-10192	0	-0	0	0	0	1	0.00	0.52	0.00	
1E	626	10192	-0	0	0	-0	0	1	0.00	0.52	0.00	

1F	626	10192	0	0	0	-0	0	1	0.00	0.52	0.00
1G	626	10192	-0	-0	0	0	0	1	0.00	0.52	0.00
1H	626	10192	0	-0	0	0	0	1	0.00	0.52	0.00
1I	626	-6188	-0	0	0	-0	0	1	0.00	0.32	0.00
1J	626	-6188	0	0	0	-0	0	1	0.00	0.32	0.00
1K	626	-6188	-0	-0	0	0	0	1	0.00	0.32	0.00
1L	626	-6188	0	-0	0	0	0	1	0.00	0.32	0.00
1M	626	6188	-0	0	0	-0	0	1	0.00	0.32	0.00
1N	626	6188	0	0	0	-0	0	1	0.00	0.32	0.00
1O	626	6188	-0	-0	0	0	0	1	0.00	0.32	0.00
1P	626	6188	0	-0	0	0	0	1	0.00	0.32	0.00
1Q	626	-3780	-0	0	0	-0	0	1	0.00	0.19	0.00
1R	626	-3780	0	0	0	-0	0	1	0.00	0.19	0.00
1S	626	-3780	-0	-0	0	0	0	1	0.00	0.19	0.00
1T	626	-3780	0	-0	0	0	0	1	0.00	0.19	0.00
1U	626	3780	-0	0	0	-0	0	1	0.00	0.19	0.00
1V	626	3780	0	0	0	-0	0	1	0.00	0.19	0.00
1W	626	3780	-0	-0	0	0	0	1	0.00	0.19	0.00
1X	626	3780	0	-0	0	0	0	1	0.00	0.19	0.00
2	626	-1682	-0	0	0	0	0	1	0.00	0.09	0.00
3	626	-1009	-0	0	0	0	0	1	0.00	0.05	0.00
4	626	-1009	-0	0	0	0	0	1	0.00	0.05	0.00
5	626	-1682	-0	0	0	0	0	1	0.00	0.09	0.00
7	626	-763	-0	-0	0	0	0	1	0.00	0.04	0.00
20	626	-766	-0	-0	0	0	0	1	0.00	0.04	0.00
22	626	511	0	0	0	0	0	1	0.00	0.03	0.00

ASTA NUM. 4 NI 6 NF 10 Lungh. 626.3 cm SEZ. 3 Rp B= 0.060 H= 0.010 m
Sollecitazioni di calcolo e di verifica Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
---	---	---	---	---	---	---	---	---	---	---	---	---
	cm	kg			kg*m							
1A	0	-9847	-0	0	0	0	0	1	0.00	0.50	0.00	
1B	0	-9847	0	0	0	0	-0	1	0.00	0.50	0.00	
1C	0	-9847	-0	-0	0	0	0	1	0.00	0.50	0.00	
1D	0	-9847	0	-0	0	0	-0	1	0.00	0.50	0.00	
1E	0	9847	-0	0	0	0	0	1	0.00	0.50	0.00	
1F	0	9847	0	0	0	0	-0	1	0.00	0.50	0.00	
1G	0	9847	-0	-0	0	0	0	1	0.00	0.50	0.00	
1H	0	9847	0	-0	0	0	-0	1	0.00	0.50	0.00	
1I	0	-5840	-0	0	0	0	0	1	0.00	0.30	0.00	
1J	0	-5840	0	0	0	0	-0	1	0.00	0.30	0.00	
1K	0	-5840	-0	-0	0	0	0	1	0.00	0.30	0.00	
1L	0	-5840	0	-0	0	0	-0	1	0.00	0.30	0.00	
1M	0	5840	-0	0	0	0	0	1	0.00	0.30	0.00	
1N	0	5840	0	0	0	0	-0	1	0.00	0.30	0.00	
1O	0	5840	-0	-0	0	0	0	1	0.00	0.30	0.00	
1P	0	5840	0	-0	0	0	-0	1	0.00	0.30	0.00	
1Q	0	-3620	-0	0	0	0	0	1	0.00	0.19	0.00	
1R	0	-3620	0	0	0	0	-0	1	0.00	0.19	0.00	
1S	0	-3620	-0	-0	0	0	0	1	0.00	0.19	0.00	
1T	0	-3620	0	-0	0	0	-0	1	0.00	0.19	0.00	
1U	0	3620	-0	0	0	0	0	1	0.00	0.19	0.00	
1V	0	3620	0	0	0	0	-0	1	0.00	0.19	0.00	
1W	0	3620	-0	-0	0	0	0	1	0.00	0.19	0.00	
1X	0	3620	0	-0	0	0	-0	1	0.00	0.19	0.00	
2	0	1601	-0	0	0	0	0	1	0.00	0.08	0.00	
3	0	961	-0	0	0	0	0	1	0.00	0.05	0.00	
4	0	961	-0	0	0	0	0	1	0.00	0.05	0.00	
5	0	1601	-0	0	0	0	0	1	0.00	0.08	0.00	
7	0	608	-0	-0	0	0	0	1	0.00	0.03	0.00	
20	0	606	-0	-0	0	0	0	1	0.00	0.03	0.00	
22	0	-404	0	0	0	0	0	1	0.00	0.02	0.00	
1A	313	-9847	-0	0	0	-0	0	1	0.00	0.50	0.00	
1B	313	-9847	0	0	0	-0	-0	1	0.00	0.50	0.00	
1C	313	-9847	-0	-0	0	0	0	1	0.00	0.50	0.00	
1D	313	-9847	0	-0	0	0	-0	1	0.00	0.50	0.00	
1E	313	9847	-0	0	0	-0	0	1	0.00	0.50	0.00	
1F	313	9847	0	0	0	-0	-0	1	0.00	0.50	0.00	
1G	313	9847	-0	-0	0	0	0	1	0.00	0.50	0.00	
1H	313	9847	0	-0	0	0	-0	1	0.00	0.50	0.00	
1I	313	-5840	-0	0	0	-0	0	1	0.00	0.30	0.00	
1J	313	-5840	0	0	0	-0	-0	1	0.00	0.30	0.00	
1K	313	-5840	-0	-0	0	0	0	1	0.00	0.30	0.00	
1L	313	-5840	0	-0	0	0	-0	1	0.00	0.30	0.00	
1M	313	5840	-0	0	0	-0	0	1	0.00	0.30	0.00	
1N	313	5840	0	0	0	-0	-0	1	0.00	0.30	0.00	
1O	313	5840	-0	-0	0	0	0	1	0.00	0.30	0.00	
1P	313	5840	0	-0	0	0	-0	1	0.00	0.30	0.00	
1Q	313	-3620	-0	0	0	-0	0	1	0.00	0.19	0.00	
1R	313	-3620	0	0	0	-0	-0	1	0.00	0.19	0.00	
1S	313	-3620	-0	-0	0	0	0	1	0.00	0.19	0.00	
1T	313	-3620	0	-0	0	0	-0	1	0.00	0.19	0.00	
1U	313	3620	-0	0	0	-0	0	1	0.00	0.19	0.00	
1V	313	3620	0	0	0	-0	-0	1	0.00	0.19	0.00	
1W	313	3620	-0	-0	0	0	0	1	0.00	0.19	0.00	
1X	313	3620	0	-0	0	0	-0	1	0.00	0.19	0.00	
2	313	1601	-0	0	0	0	0	1	0.00	0.08	0.00	
3	313	961	-0	0	0	0	0	1	0.00	0.05	0.00	
4	313	961	-0	0	0	0	0	1	0.00	0.05	0.00	
5	313	1601	-0	0	0	0	0	1	0.00	0.08	0.00	
7	313	608	-0	-0	0	0	0	1	0.00	0.03	0.00	
20	313	606	-0	-0	0	-0	0	1	0.00	0.03	0.00	
22	313	-404	0	0	0	0	0	1	0.00	0.02	0.00	
1A	626	-9847	-0	0	0	-0	0	1	0.00	0.50	0.00	

1B	626	-9847	0	0	0	-0	0	1	0.00	0.50	0.00
1C	626	-9847	-0	-0	0	0	0	1	0.00	0.50	0.00
1D	626	-9847	0	-0	0	0	0	1	0.00	0.50	0.00
1E	626	9847	-0	0	0	-0	0	1	0.00	0.50	0.00
1F	626	9847	0	0	0	0	0	1	0.00	0.50	0.00
1G	626	9847	-0	-0	0	0	0	1	0.00	0.50	0.00
1H	626	9847	0	-0	0	0	0	1	0.00	0.50	0.00
1I	626	-5840	-0	0	0	-0	0	1	0.00	0.30	0.00
1J	626	-5840	0	0	0	-0	0	1	0.00	0.30	0.00
1K	626	-5840	-0	-0	0	0	0	1	0.00	0.30	0.00
1L	626	-5840	0	-0	0	0	0	1	0.00	0.30	0.00
1M	626	5840	-0	0	0	-0	0	1	0.00	0.30	0.00
1N	626	5840	0	0	0	-0	0	1	0.00	0.30	0.00
1O	626	5840	-0	-0	0	0	0	1	0.00	0.30	0.00
1P	626	5840	0	-0	0	0	0	1	0.00	0.30	0.00
1Q	626	-3620	-0	0	0	-0	0	1	0.00	0.19	0.00
1R	626	-3620	0	0	0	-0	0	1	0.00	0.19	0.00
1S	626	-3620	-0	-0	0	0	0	1	0.00	0.19	0.00
1T	626	-3620	0	-0	0	0	0	1	0.00	0.19	0.00
1U	626	3620	-0	0	0	-0	0	1	0.00	0.19	0.00
1V	626	3620	0	0	0	-0	0	1	0.00	0.19	0.00
1W	626	3620	-0	-0	0	0	0	1	0.00	0.19	0.00
1X	626	3620	0	-0	0	0	0	1	0.00	0.19	0.00
2	626	1601	-0	0	0	0	0	1	0.00	0.08	0.00
3	626	961	-0	0	0	0	0	1	0.00	0.05	0.00
4	626	961	-0	0	0	0	0	1	0.00	0.05	0.00
5	626	1601	-0	0	0	0	0	1	0.00	0.08	0.00
7	626	608	-0	-0	0	0	0	1	0.00	0.03	0.00
20	626	606	-0	-0	0	-0	0	1	0.00	0.03	0.00
22	626	-404	0	0	0	0	0	1	0.00	0.02	0.00

ASTA NUM. 5 NI 10 NF 7 Lungh. 626.3 cm SEZ. 3 Rp B= 0.060 H= 0.010 m
Sollecitazioni di calcolo e di verifica Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	cm	kg			kg*m							
1A	0	-1555	-0	0	0	0	0	1	0.00	0.08	0.00	
1B	0	-1555	0	0	0	0	0	1	0.00	0.08	0.00	
1C	0	-1555	-0	-0	0	-0	0	1	0.00	0.08	0.00	
1D	0	-1555	0	-0	0	-0	0	1	0.00	0.08	0.00	
1E	0	1555	-0	0	0	0	0	1	0.00	0.08	0.00	
1F	0	1555	0	0	0	0	0	1	0.00	0.08	0.00	
1G	0	1555	-0	-0	0	-0	0	1	0.00	0.08	0.00	
1H	0	1555	0	-0	0	-0	0	1	0.00	0.08	0.00	
1I	0	-3401	-0	0	0	0	0	1	0.00	0.17	0.00	
1J	0	-3401	0	0	0	0	0	1	0.00	0.17	0.00	
1K	0	-3401	-0	-0	0	-0	0	1	0.00	0.17	0.00	
1L	0	-3401	0	-0	0	-0	0	1	0.00	0.17	0.00	
1M	0	3401	-0	0	0	0	0	1	0.00	0.17	0.00	
1N	0	3401	0	0	0	0	0	1	0.00	0.17	0.00	
1O	0	3401	-0	-0	0	-0	0	1	0.00	0.17	0.00	
1P	0	3401	0	-0	0	-0	0	1	0.00	0.17	0.00	
1Q	0	-1144	-0	0	0	0	0	1	0.00	0.06	0.00	
1R	0	-1144	0	0	0	0	0	1	0.00	0.06	0.00	
1S	0	-1144	-0	-0	0	-0	0	1	0.00	0.06	0.00	
1T	0	-1144	0	-0	0	-0	0	1	0.00	0.06	0.00	
1U	0	1144	-0	0	0	0	0	1	0.00	0.06	0.00	
1V	0	1144	0	0	0	0	0	1	0.00	0.06	0.00	
1W	0	1144	-0	-0	0	-0	0	1	0.00	0.06	0.00	
1X	0	1144	0	-0	0	-0	0	1	0.00	0.06	0.00	
2	0	-10	-0	-0	0	0	0	1	0.00	0.00	0.00	
3	0	-6	-0	-0	0	0	0	1	0.00	0.00	0.00	
4	0	-6	-0	-0	0	0	0	1	0.00	0.00	0.00	
5	0	-10	-0	-0	0	0	0	1	0.00	0.00	0.00	
7	0	-698	-0	0	0	0	0	1	0.00	0.04	0.00	
20	0	-745	-0	0	0	0	0	1	0.00	0.04	0.00	
22	0	497	-0	-0	0	0	0	1	0.00	0.03	0.00	
1A	313	-1555	-0	0	0	0	-0	1	0.00	0.08	0.00	
1B	313	-1555	0	0	0	0	0	1	0.00	0.08	0.00	
1C	313	-1555	-0	-0	0	-0	-0	1	0.00	0.08	0.00	
1D	313	-1555	0	-0	0	-0	0	1	0.00	0.08	0.00	
1E	313	1555	-0	0	0	0	-0	1	0.00	0.08	0.00	
1F	313	1555	0	0	0	0	0	1	0.00	0.08	0.00	
1G	313	1555	-0	-0	0	-0	-0	1	0.00	0.08	0.00	
1H	313	1555	0	-0	0	-0	0	1	0.00	0.08	0.00	
1I	313	-3401	-0	0	0	0	-0	1	0.00	0.17	0.00	
1J	313	-3401	0	0	0	0	0	1	0.00	0.17	0.00	
1K	313	-3401	-0	-0	0	-0	-0	1	0.00	0.17	0.00	
1L	313	-3401	0	-0	0	-0	0	1	0.00	0.17	0.00	
1M	313	3401	-0	0	0	0	-0	1	0.00	0.17	0.00	
1N	313	3401	0	0	0	0	0	1	0.00	0.17	0.00	
1O	313	3401	-0	-0	0	-0	-0	1	0.00	0.17	0.00	
1P	313	3401	0	-0	0	-0	0	1	0.00	0.17	0.00	
1Q	313	-1144	-0	0	0	0	-0	1	0.00	0.06	0.00	
1R	313	-1144	0	0	0	0	0	1	0.00	0.06	0.00	
1S	313	-1144	-0	-0	0	-0	-0	1	0.00	0.06	0.00	
1T	313	-1144	0	-0	0	-0	0	1	0.00	0.06	0.00	
1U	313	1144	-0	0	0	0	-0	1	0.00	0.06	0.00	
1V	313	1144	0	0	0	0	0	1	0.00	0.06	0.00	
1W	313	1144	-0	-0	0	-0	-0	1	0.00	0.06	0.00	
1X	313	1144	0	-0	0	-0	0	1	0.00	0.06	0.00	
2	313	-10	-0	-0	0	0	0	1	0.00	0.00	0.00	
3	313	-6	-0	-0	0	0	0	1	0.00	0.00	0.00	
4	313	-6	-0	-0	0	0	0	1	0.00	0.00	0.00	
5	313	-10	-0	-0	0	0	0	1	0.00	0.00	0.00	
7	313	-698	-0	0	0	0	0	1	0.00	0.04	0.00	

20	313	-745	-0	0	0	-0	0	1	0.00	0.04	0.00
22	313	497	-0	-0	0	0	0	1	0.00	0.03	0.00
1A	626	-1555	-0	0	0	0	-0	1	0.00	0.08	0.00
1B	626	-1555	0	0	0	0	0	1	0.00	0.08	0.00
1C	626	-1555	-0	-0	0	0	-0	1	0.00	0.08	0.00
1D	626	-1555	0	-0	0	0	0	1	0.00	0.08	0.00
1E	626	1555	-0	0	0	0	-0	1	0.00	0.08	0.00
1F	626	1555	0	0	0	0	0	1	0.00	0.08	0.00
1G	626	1555	-0	-0	0	0	-0	1	0.00	0.08	0.00
1H	626	1555	0	-0	0	0	0	1	0.00	0.08	0.00
1I	626	-3401	-0	0	0	0	-0	1	0.00	0.17	0.00
1J	626	-3401	0	0	0	0	0	1	0.00	0.17	0.00
1K	626	-3401	-0	-0	0	0	-0	1	0.00	0.17	0.00
1L	626	-3401	0	-0	0	0	0	1	0.00	0.17	0.00
1M	626	3401	-0	0	0	0	-0	1	0.00	0.17	0.00
1N	626	3401	0	0	0	0	0	1	0.00	0.17	0.00
1O	626	3401	-0	-0	0	0	-0	1	0.00	0.17	0.00
1P	626	3401	0	-0	0	0	0	1	0.00	0.17	0.00
1Q	626	-1144	-0	0	0	0	-0	1	0.00	0.06	0.00
1R	626	-1144	0	0	0	0	0	1	0.00	0.06	0.00
1S	626	-1144	-0	-0	0	0	-0	1	0.00	0.06	0.00
1T	626	-1144	0	-0	0	0	0	1	0.00	0.06	0.00
1U	626	1144	-0	0	0	0	-0	1	0.00	0.06	0.00
1V	626	1144	0	0	0	0	0	1	0.00	0.06	0.00
1W	626	1144	-0	-0	0	0	-0	1	0.00	0.06	0.00
1X	626	1144	0	-0	0	0	0	1	0.00	0.06	0.00
2	626	-10	-0	-0	0	0	0	1	0.00	0.00	0.00
3	626	-6	-0	-0	0	0	0	1	0.00	0.00	0.00
4	626	-6	-0	-0	0	0	0	1	0.00	0.00	0.00
5	626	-10	-0	-0	0	0	0	1	0.00	0.00	0.00
7	626	-698	-0	0	0	0	0	1	0.00	0.04	0.00
20	626	-745	-0	0	0	-0	0	1	0.00	0.04	0.00
22	626	497	-0	-0	0	0	0	1	0.00	0.03	0.00

ASTA NUM. 6 NI 7 NF 2 Lungh. 626.3 cm SEZ. 3 Rp B= 0.060 H= 0.010 m
Sollecitazioni di calcolo e di verifica Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	cm	kg			kg*m							
1A	0	-9900	-0	0	0	0	0	1	0.00	0.51	0.00	
1B	0	-9900	-0	0	0	0	0	1	0.00	0.51	0.00	
1C	0	-9900	-0	-0	0	-0	0	1	0.00	0.51	0.00	
1D	0	-9900	-0	-0	0	-0	0	1	0.00	0.51	0.00	
1E	0	9900	-0	0	0	0	0	1	0.00	0.51	0.00	
1F	0	9900	-0	0	0	0	0	1	0.00	0.51	0.00	
1G	0	9900	-0	-0	0	-0	0	1	0.00	0.51	0.00	
1H	0	9900	-0	-0	0	-0	0	1	0.00	0.51	0.00	
1I	0	-5779	-0	0	0	0	0	1	0.00	0.30	0.00	
1J	0	-5779	-0	0	0	0	0	1	0.00	0.30	0.00	
1K	0	-5779	-0	-0	0	-0	0	1	0.00	0.30	0.00	
1L	0	-5779	-0	-0	0	-0	0	1	0.00	0.30	0.00	
1M	0	5779	-0	0	0	0	0	1	0.00	0.30	0.00	
1N	0	5779	-0	0	0	0	0	1	0.00	0.30	0.00	
1O	0	5779	-0	-0	0	-0	0	1	0.00	0.30	0.00	
1P	0	5779	-0	-0	0	-0	0	1	0.00	0.30	0.00	
1Q	0	-3618	-0	0	0	0	0	1	0.00	0.19	0.00	
1R	0	-3618	-0	0	0	0	0	1	0.00	0.19	0.00	
1S	0	-3618	-0	-0	0	-0	0	1	0.00	0.19	0.00	
1T	0	-3618	-0	-0	0	-0	0	1	0.00	0.19	0.00	
1U	0	3618	-0	0	0	0	0	1	0.00	0.19	0.00	
1V	0	3618	-0	0	0	0	0	1	0.00	0.19	0.00	
1W	0	3618	-0	-0	0	-0	0	1	0.00	0.19	0.00	
1X	0	3618	-0	-0	0	-0	0	1	0.00	0.19	0.00	
2	0	-1653	-0	0	0	0	0	1	0.00	0.08	0.00	
3	0	-992	-0	0	0	0	0	1	0.00	0.05	0.00	
4	0	-992	-0	0	0	0	0	1	0.00	0.05	0.00	
5	0	-1653	-0	0	0	0	0	1	0.00	0.08	0.00	
7	0	677	-0	0	0	0	0	1	0.00	0.03	0.00	
20	0	617	-0	0	0	0	0	1	0.00	0.03	0.00	
22	0	-412	-0	-0	0	0	0	1	0.00	0.02	0.00	
1A	313	-9900	-0	0	0	0	-0	1	0.00	0.51	0.00	
1B	313	-9900	-0	0	0	0	0	1	0.00	0.51	0.00	
1C	313	-9900	-0	-0	0	-0	-0	1	0.00	0.51	0.00	
1D	313	-9900	-0	-0	0	-0	0	1	0.00	0.51	0.00	
1E	313	9900	-0	0	0	0	-0	1	0.00	0.51	0.00	
1F	313	9900	-0	0	0	0	0	1	0.00	0.51	0.00	
1G	313	9900	-0	-0	0	-0	-0	1	0.00	0.51	0.00	
1H	313	9900	-0	-0	0	-0	0	1	0.00	0.51	0.00	
1I	313	-5779	-0	0	0	0	-0	1	0.00	0.30	0.00	
1J	313	-5779	-0	0	0	0	0	1	0.00	0.30	0.00	
1K	313	-5779	-0	-0	0	-0	-0	1	0.00	0.30	0.00	
1L	313	-5779	-0	-0	0	-0	0	1	0.00	0.30	0.00	
1M	313	5779	-0	0	0	0	-0	1	0.00	0.30	0.00	
1N	313	5779	-0	0	0	0	0	1	0.00	0.30	0.00	
1O	313	5779	-0	-0	0	-0	-0	1	0.00	0.30	0.00	
1P	313	5779	-0	-0	0	-0	0	1	0.00	0.30	0.00	
1Q	313	-3618	-0	0	0	0	-0	1	0.00	0.19	0.00	
1R	313	-3618	-0	0	0	0	0	1	0.00	0.19	0.00	
1S	313	-3618	-0	-0	0	-0	-0	1	0.00	0.19	0.00	
1T	313	-3618	-0	-0	0	-0	0	1	0.00	0.19	0.00	
1U	313	3618	-0	0	0	0	-0	1	0.00	0.19	0.00	
1V	313	3618	-0	0	0	0	0	1	0.00	0.19	0.00	
1W	313	3618	-0	-0	0	-0	-0	1	0.00	0.19	0.00	
1X	313	3618	-0	-0	0	-0	0	1	0.00	0.19	0.00	
2	313	-1653	-0	0	0	0	0	1	0.00	0.08	0.00	

3	313	-992	-0	0	0	0	0	1	0.00	0.05	0.00
4	313	-992	-0	0	0	0	0	1	0.00	0.05	0.00
5	313	-1653	-0	0	0	0	0	1	0.00	0.08	0.00
7	313	677	-0	0	0	0	0	1	0.00	0.03	0.00
20	313	617	-0	0	0	0	0	1	0.00	0.03	0.00
22	313	-412	-0	-0	0	0	0	1	0.00	0.02	0.00
1A	626	-9900	-0	0	0	0	-0	1	0.00	0.51	0.00
1B	626	-9900	-0	0	0	0	0	1	0.00	0.51	0.00
1C	626	-9900	-0	-0	0	0	-0	1	0.00	0.51	0.00
1D	626	-9900	-0	-0	0	0	0	1	0.00	0.51	0.00
1E	626	9900	-0	0	0	0	-0	1	0.00	0.51	0.00
1F	626	9900	-0	0	0	0	0	1	0.00	0.51	0.00
1G	626	9900	-0	-0	0	0	-0	1	0.00	0.51	0.00
1H	626	9900	-0	-0	0	0	0	1	0.00	0.51	0.00
1I	626	-5779	-0	0	0	0	-0	1	0.00	0.30	0.00
1J	626	-5779	-0	0	0	0	0	1	0.00	0.30	0.00
1K	626	-5779	-0	-0	0	0	-0	1	0.00	0.30	0.00
1L	626	-5779	-0	-0	0	0	0	1	0.00	0.30	0.00
1M	626	5779	-0	0	0	0	-0	1	0.00	0.30	0.00
1N	626	5779	-0	0	0	0	0	1	0.00	0.30	0.00
1O	626	5779	-0	-0	0	0	-0	1	0.00	0.30	0.00
1P	626	5779	-0	-0	0	0	0	1	0.00	0.30	0.00
1Q	626	-3618	-0	0	0	0	-0	1	0.00	0.19	0.00
1R	626	-3618	-0	0	0	0	0	1	0.00	0.19	0.00
1S	626	-3618	-0	-0	0	0	-0	1	0.00	0.19	0.00
1T	626	-3618	-0	-0	0	0	0	1	0.00	0.19	0.00
1U	626	3618	-0	0	0	0	-0	1	0.00	0.19	0.00
1V	626	3618	-0	0	0	0	0	1	0.00	0.19	0.00
1W	626	3618	-0	-0	0	0	-0	1	0.00	0.19	0.00
1X	626	3618	-0	-0	0	0	0	1	0.00	0.19	0.00
2	626	-1653	-0	0	0	0	0	1	0.00	0.08	0.00
3	626	-992	-0	0	0	0	0	1	0.00	0.05	0.00
4	626	-992	-0	0	0	0	0	1	0.00	0.05	0.00
5	626	-1653	-0	0	0	0	0	1	0.00	0.08	0.00
7	626	677	-0	0	0	0	0	1	0.00	0.03	0.00
20	626	617	-0	0	0	0	0	1	0.00	0.03	0.00
22	626	-412	-0	-0	0	0	0	1	0.00	0.02	0.00

AMV s.r.l.
Via San Lorenzo, 106 Tel. 0481/779903
34077 Ronchi dei Legionari (GO)

Lavoro: **Struttura R01** Intestazione lavoro:
Elemento: **TRAVE** Metodo di verifica: **Eurocodice 3 - NTC 2018**
Gruppo: **3** Descrizione: **Travi di collegamento trasversali**
Tabella: **Tabella travi** Struttura: **Nuova**
Tipo acciaio: **S 355** Beta piano 'yx': **1.000** Beta piano 'zx': **1.000**
Tipologia sismica: **Senza prescrizioni aggiuntive**
 $\gamma M0$: **1.050** $\gamma M1$: **1.050** $\gamma M2$: **1.250** γ_{rv} : **0.000** $\gamma M0$ Pf: **1.000** $\gamma M1$ Pf: **1.000**
Tipo collegamento: **saldato** Connessione su un solo lato Connessione sul lato corto (solo 'L')

ASTA NUM. 1 NI 1 NF 2 Lungh. 390.0 cm SEZ. 2 Pd UNP 160 Dist.= 0.015 m ali esterne

categoria: p.p. y qy tot.

qy medio: 37.68 37.68 kg/m

Sollecitazioni di calcolo e di verifica

Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
---	---	---	---	---	---	---	---	---	---	---	---	---
	cm	kg			kg*m							
1A	0	-5102	73	172	0	342	0	1	0.00	0.03	0.11	
1B	0	-5102	73	172	0	342	-0	1	0.00	0.03	0.11	
1C	0	-5102	73	-172	0	-342	0	1	0.00	0.03	0.11	
1D	0	-5102	73	-172	0	-342	-0	1	0.00	0.03	0.11	
1E	0	5102	73	172	0	342	0	1	0.00	0.03	0.11	
1F	0	5102	73	172	0	342	-0	1	0.00	0.03	0.11	
1G	0	5102	73	-172	0	-342	0	1	0.00	0.03	0.11	
1H	0	5102	73	-172	0	-342	-0	1	0.00	0.03	0.11	
1I	0	-2849	73	85	0	169	0	1	0.00	0.02	0.06	
1J	0	-2849	73	85	0	169	-0	1	0.00	0.02	0.06	
1K	0	-2849	73	-85	0	-169	0	1	0.00	0.02	0.06	
1L	0	-2849	73	-85	0	-169	-0	1	0.00	0.02	0.06	
1M	0	2849	73	85	0	169	0	1	0.00	0.02	0.06	
1N	0	2849	73	85	0	169	-0	1	0.00	0.02	0.06	
1O	0	2849	73	-85	0	-169	0	1	0.00	0.02	0.06	
1P	0	2849	73	-85	0	-169	-0	1	0.00	0.02	0.06	
1Q	0	-1835	73	59	0	118	0	1	0.00	0.01	0.04	
1R	0	-1835	73	59	0	118	-0	1	0.00	0.01	0.04	
1S	0	-1835	73	-59	0	-118	0	1	0.00	0.01	0.04	
1T	0	-1835	73	-59	0	-118	-0	1	0.00	0.01	0.04	
1U	0	1835	73	59	0	118	0	1	0.00	0.01	0.04	
1V	0	1835	73	59	0	118	-0	1	0.00	0.01	0.04	
1W	0	1835	73	-59	0	-118	0	1	0.00	0.01	0.04	
1X	0	1835	73	-59	0	-118	-0	1	0.00	0.01	0.04	
2	0	-1457	73	-38	0	-77	0	1	0.00	0.01	0.03	
3	0	-874	96	-23	0	-46	0	1	0.00	0.01	0.02	
4	0	-874	96	-23	0	-46	0	1	0.00	0.01	0.02	
5	0	-1457	96	-38	0	-77	0	1	0.00	0.01	0.03	
7	0	308	96	8	0	16	0	1	0.00	0.00	0.01	
20	0	334	96	8	0	16	0	1	0.00	0.00	0.01	
22	0	-222	0	-5	0	-11	0	1	0.00	0.00	0.00	
1A	195	-5102	-0	172	0	7	72	1	0.00	0.03	0.04	
1B	195	-5102	0	172	0	7	72	1	0.00	0.03	0.04	
1C	195	-5102	-0	-172	0	-7	72	1	0.00	0.03	0.04	
1D	195	-5102	0	-172	0	-7	72	1	0.00	0.03	0.04	
1E	195	5102	-0	172	0	7	72	1	0.00	0.03	0.04	
1F	195	5102	0	172	0	7	72	1	0.00	0.03	0.04	
1G	195	5102	-0	-172	0	-7	72	1	0.00	0.03	0.04	
1H	195	5102	0	-172	0	-7	72	1	0.00	0.03	0.04	
1I	195	-2849	-0	85	0	4	72	1	0.00	0.02	0.03	
1J	195	-2849	0	85	0	4	72	1	0.00	0.02	0.03	
1K	195	-2849	-0	-85	0	-4	72	1	0.00	0.02	0.03	
1L	195	-2849	0	-85	0	-4	72	1	0.00	0.02	0.03	
1M	195	2849	-0	85	0	4	72	1	0.00	0.02	0.03	
1N	195	2849	0	85	0	4	72	1	0.00	0.02	0.03	
1O	195	2849	-0	-85	0	-4	72	1	0.00	0.02	0.03	
1P	195	2849	0	-85	0	-4	72	1	0.00	0.02	0.03	
1Q	195	-1835	-0	59	0	3	72	1	0.00	0.01	0.02	
1R	195	-1835	0	59	0	3	72	1	0.00	0.01	0.02	
1S	195	-1835	-0	-59	0	-3	72	1	0.00	0.01	0.02	
1T	195	-1835	0	-59	0	-3	72	1	0.00	0.01	0.02	
1U	195	1835	-0	59	0	3	72	1	0.00	0.01	0.02	
1V	195	1835	0	59	0	3	72	1	0.00	0.01	0.02	
1W	195	1835	-0	-59	0	-3	72	1	0.00	0.01	0.02	
1X	195	1835	0	-59	0	-3	72	1	0.00	0.01	0.02	
2	195	-1457	0	-38	0	-2	72	1	0.00	0.01	0.02	
3	195	-874	0	-23	0	-1	93	1	0.00	0.01	0.02	
4	195	-874	0	-23	0	-1	93	1	0.00	0.01	0.02	
5	195	-1457	0	-38	0	-2	93	1	0.00	0.01	0.02	
7	195	308	0	8	0	0	93	1	0.00	0.00	0.01	
20	195	334	0	8	0	0	93	1	0.00	0.00	0.01	
22	195	-222	0	-5	0	-0	0	1	0.00	0.00	0.00	
1A	390	-5102	-73	172	0	-328	0	1	0.00	0.03	0.11	
1B	390	-5102	-73	172	0	-328	-0	1	0.00	0.03	0.11	
1C	390	-5102	-73	-172	0	328	0	1	0.00	0.03	0.11	
1D	390	-5102	-73	-172	0	328	-0	1	0.00	0.03	0.11	
1E	390	5102	-73	172	0	-328	0	1	0.00	0.03	0.11	
1F	390	5102	-73	172	0	-328	-0	1	0.00	0.03	0.11	
1G	390	5102	-73	-172	0	328	0	1	0.00	0.03	0.11	
1H	390	5102	-73	-172	0	328	-0	1	0.00	0.03	0.11	
1I	390	-2849	-73	85	0	-162	0	1	0.00	0.02	0.05	
1J	390	-2849	-73	85	0	-162	0	1	0.00	0.02	0.05	

1K	390	-2849	-73	-85	0	162	0	1	0.00	0.02	0.05	
1L	390	-2849	-73	-85	0	162	0	1	0.00	0.02	0.05	
1M	390	2849	-73	85	0	-162	0	1	0.00	0.02	0.05	
1N	390	2849	-73	85	0	-162	0	1	0.00	0.02	0.05	
1O	390	2849	-73	-85	0	162	0	1	0.00	0.02	0.05	
1P	390	2849	-73	-85	0	162	0	1	0.00	0.02	0.05	
1Q	390	-1835	-73	59	0	-113	0	1	0.00	0.01	0.04	
1R	390	-1835	-73	59	0	-113	0	1	0.00	0.01	0.04	
1S	390	-1835	-73	-59	0	113	0	1	0.00	0.01	0.04	
1T	390	-1835	-73	-59	0	113	0	1	0.00	0.01	0.04	
1U	390	1835	-73	59	0	-113	0	1	0.00	0.01	0.04	
1V	390	1835	-73	59	0	-113	0	1	0.00	0.01	0.04	
1W	390	1835	-73	-59	0	113	0	1	0.00	0.01	0.04	
1X	390	1835	-73	-59	0	113	0	1	0.00	0.01	0.04	
2	390	-1457	-73	-38	0	72	0	1	0.00	0.01	0.03	
3	390	-874	-96	-23	0	43	0	1	0.00	0.01	0.02	
4	390	-874	-96	-23	0	43	0	1	0.00	0.01	0.02	
5	390	-1457	-96	-38	0	72	0	1	0.00	0.01	0.03	
7	390	308	-96	8	0	-16	0	1	0.00	0.00	0.01	
20	390	334	-96	8	0	-15	0	1	0.00	0.00	0.01	
22	390	-222	0	-5	0	10	0	1	0.00	0.00	0.00	

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	χ_{min}	ky	kz	kLT	χ_{LT}	I.S.n.	I.S.m.	I.S.	Nota
--	kg	kg*m	kg*m										
1A	-5102	342	72	1	0.2816	0.9061	1.0147	--	--	0.11	--	0.19	Snell. 'zx'= 122
1B	-5102	342	72	1	0.2816	0.9061	1.0147	--	--	0.11	--	0.19	Snell. 'zx'= 122
1C	-5102	-342	72	1	0.2816	0.9061	1.0147	--	--	0.11	--	0.19	Snell. 'zx'= 122
1D	-5102	-342	72	1	0.2816	0.9061	1.0147	--	--	0.11	--	0.19	Snell. 'zx'= 122
1I	-2849	169	72	1	0.2816	0.9476	1.0082	--	--	0.06	--	0.11	Snell. 'zx'= 122
1J	-2849	169	72	1	0.2816	0.9476	1.0082	--	--	0.06	--	0.11	Snell. 'zx'= 122
1K	-2849	-169	72	1	0.2816	0.9476	1.0082	--	--	0.06	--	0.11	Snell. 'zx'= 122
1L	-2849	-169	72	1	0.2816	0.9476	1.0082	--	--	0.06	--	0.11	Snell. 'zx'= 122
1Q	-1835	118	72	1	0.2816	0.9662	1.0053	--	--	0.04	--	0.07	Snell. 'zx'= 122
1R	-1835	118	72	1	0.2816	0.9662	1.0053	--	--	0.04	--	0.07	Snell. 'zx'= 122
1S	-1835	-118	72	1	0.2816	0.9662	1.0053	--	--	0.04	--	0.07	Snell. 'zx'= 122
1T	-1835	-118	72	1	0.2816	0.9662	1.0053	--	--	0.04	--	0.07	Snell. 'zx'= 122
2	-1457	-77	72	1	0.2816	0.9732	1.0042	--	--	0.03	--	0.06	Snell. 'zx'= 122
3	-874	-46	93	1	0.2816	0.9839	1.0076	--	--	0.02	--	0.04	Snell. 'zx'= 122
4	-874	-46	93	1	0.2816	0.9839	1.0076	--	--	0.02	--	0.04	Snell. 'zx'= 122
5	-1457	-77	93	1	0.2816	0.9732	1.0126	--	--	0.03	--	0.06	Snell. 'zx'= 122
22	-222	-11	0	1	0.2816	0.9959	1.0062	--	--	0.00	--	0.01	Snell. 'zx'= 122

ASTA NUM. 2 NI 7 NF 9 Lungh. 390.0 cm SEZ. 2 Pd UNP 160 Dist.= 0.015 m ali esterne

categoria: p.p. y qy tot.
qy medio: 37.68 37.68 kg/m

Sollecitazioni di calcolo e di verifica

Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
--	cm	kg	kg	kg	kg*m	kg*m	kg*m					
1A	0	-265	73	151	0	295	0	1	0.00	0.00	0.07	
1B	0	-265	73	151	0	295	-0	1	0.00	0.00	0.07	
1C	0	-265	73	-151	0	-295	0	1	0.00	0.00	0.07	
1D	0	-265	73	-151	0	-295	-0	1	0.00	0.00	0.07	
1E	0	265	73	151	0	295	0	1	0.00	0.00	0.07	
1F	0	265	73	151	0	295	-0	1	0.00	0.00	0.07	
1G	0	265	73	-151	0	-295	0	1	0.00	0.00	0.07	
1H	0	265	73	-151	0	-295	-0	1	0.00	0.00	0.07	
1I	0	-122	73	55	0	108	0	1	0.00	0.00	0.03	
1J	0	-122	73	55	0	108	-0	1	0.00	0.00	0.03	
1K	0	-122	73	-55	0	-108	0	1	0.00	0.00	0.03	
1L	0	-122	73	-55	0	-108	-0	1	0.00	0.00	0.03	
1M	0	122	73	55	0	108	0	1	0.00	0.00	0.03	
1N	0	122	73	55	0	108	-0	1	0.00	0.00	0.03	
1O	0	122	73	-55	0	-108	0	1	0.00	0.00	0.03	
1P	0	122	73	-55	0	-108	-0	1	0.00	0.00	0.03	
1Q	0	-89	73	47	0	93	0	1	0.00	0.00	0.02	
1R	0	-89	73	47	0	93	-0	1	0.00	0.00	0.02	
1S	0	-89	73	-47	0	-93	0	1	0.00	0.00	0.02	
1T	0	-89	73	-47	0	-93	-0	1	0.00	0.00	0.02	
1U	0	89	73	47	0	93	0	1	0.00	0.00	0.02	
1V	0	89	73	47	0	93	-0	1	0.00	0.00	0.02	
1W	0	89	73	-47	0	-93	0	1	0.00	0.00	0.02	
1X	0	89	73	-47	0	-93	-0	1	0.00	0.00	0.02	
2	0	-387	73	-19	0	-36	0	1	0.00	0.00	0.01	
3	0	-232	96	-11	0	-22	0	1	0.00	0.00	0.01	
4	0	-232	96	-11	0	-22	0	1	0.00	0.00	0.01	
5	0	-387	96	-19	0	-36	0	1	0.00	0.00	0.01	
7	0	-1	96	4	0	8	0	1	0.00	0.00	0.00	
20	0	59	96	4	0	8	0	1	0.00	0.00	0.00	
22	0	-39	0	-3	0	-6	0	1	0.00	0.00	0.00	
1A	195	-265	-0	151	0	1	72	1	0.00	0.00	0.01	
1B	195	-265	0	151	0	1	72	1	0.00	0.00	0.01	
1C	195	-265	-0	-151	0	-1	72	1	0.00	0.00	0.01	
1D	195	-265	0	-151	0	-1	72	1	0.00	0.00	0.01	
1E	195	265	-0	151	0	1	72	1	0.00	0.00	0.01	
1F	195	265	0	151	0	1	72	1	0.00	0.00	0.01	
1G	195	265	-0	-151	0	-1	72	1	0.00	0.00	0.01	
1H	195	265	0	-151	0	-1	72	1	0.00	0.00	0.01	

1I	195	-122	-0	55	0	0	72	1	0.00	0.00	0.01
1J	195	-122	0	55	0	0	72	1	0.00	0.00	0.01
1K	195	-122	-0	-55	0	-0	72	1	0.00	0.00	0.01
1L	195	-122	0	-55	0	-0	72	1	0.00	0.00	0.01
1M	195	122	-0	55	0	0	72	1	0.00	0.00	0.01
1N	195	122	0	55	0	0	72	1	0.00	0.00	0.01
1O	195	122	-0	-55	0	-0	72	1	0.00	0.00	0.01
1P	195	122	0	-55	0	-0	72	1	0.00	0.00	0.01
1Q	195	-89	-0	47	0	0	72	1	0.00	0.00	0.01
1R	195	-89	0	47	0	0	72	1	0.00	0.00	0.01
1S	195	-89	-0	-47	0	-0	72	1	0.00	0.00	0.01
1T	195	-89	0	-47	0	-0	72	1	0.00	0.00	0.01
1U	195	89	-0	47	0	0	72	1	0.00	0.00	0.01
1V	195	89	0	47	0	0	72	1	0.00	0.00	0.01
1W	195	89	-0	-47	0	-0	72	1	0.00	0.00	0.01
1X	195	89	0	-47	0	-0	72	1	0.00	0.00	0.01
2	195	-387	0	-19	0	-0	72	1	0.00	0.00	0.01
3	195	-232	0	-11	0	-0	93	1	0.00	0.00	0.01
4	195	-232	0	-11	0	-0	93	1	0.00	0.00	0.01
5	195	-387	0	-19	0	-0	93	1	0.00	0.00	0.01
7	195	-1	0	4	0	0	93	1	0.00	0.00	0.01
20	195	59	0	4	0	0	93	1	0.00	0.00	0.01
22	195	-39	0	-3	0	-0	0	1	0.00	0.00	0.00

1A	390	-265	-73	151	0	-293	0	1	0.00	0.00	0.07
1B	390	-265	-73	151	0	-293	0	1	0.00	0.00	0.07
1C	390	-265	-73	-151	0	293	0	1	0.00	0.00	0.07
1D	390	-265	-73	-151	0	293	0	1	0.00	0.00	0.07
1E	390	265	-73	151	0	-293	0	1	0.00	0.00	0.07
1F	390	265	-73	151	0	-293	0	1	0.00	0.00	0.07
1G	390	265	-73	-151	0	293	0	1	0.00	0.00	0.07
1H	390	265	-73	-151	0	293	0	1	0.00	0.00	0.07
1I	390	-122	-73	55	0	-107	0	1	0.00	0.00	0.03
1J	390	-122	-73	55	0	-107	0	1	0.00	0.00	0.03
1K	390	-122	-73	-55	0	107	0	1	0.00	0.00	0.03
1L	390	-122	-73	-55	0	107	0	1	0.00	0.00	0.03
1M	390	122	-73	55	0	-107	0	1	0.00	0.00	0.03
1N	390	122	-73	55	0	-107	0	1	0.00	0.00	0.03
1O	390	122	-73	-55	0	107	0	1	0.00	0.00	0.03
1P	390	122	-73	-55	0	107	0	1	0.00	0.00	0.03
1Q	390	-89	-73	47	0	-92	0	1	0.00	0.00	0.02
1R	390	-89	-73	47	0	-92	0	1	0.00	0.00	0.02
1S	390	-89	-73	-47	0	92	0	1	0.00	0.00	0.02
1T	390	-89	-73	-47	0	92	0	1	0.00	0.00	0.02
1U	390	89	-73	47	0	-92	0	1	0.00	0.00	0.02
1V	390	89	-73	47	0	-92	0	1	0.00	0.00	0.02
1W	390	89	-73	-47	0	92	0	1	0.00	0.00	0.02
1X	390	89	-73	-47	0	92	0	1	0.00	0.00	0.02
2	390	-387	-73	-19	0	36	0	1	0.00	0.00	0.01
3	390	-232	-96	-11	0	22	0	1	0.00	0.00	0.01
4	390	-232	-96	-11	0	22	0	1	0.00	0.00	0.01
5	390	-387	-96	-19	0	36	0	1	0.00	0.00	0.01
7	390	-1	-96	4	0	-8	0	1	0.00	0.00	0.00
20	390	59	-96	4	0	-8	0	1	0.00	0.00	0.00
22	390	-39	0	-3	0	6	0	1	0.00	0.00	0.00

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	$\gamma_{min.}$	ky	kz	kLT	χ_{LT}	I.S.n.	I.S.m.	I.S.	Nota
	kg	kg*m											
1A	-265	295	72	1	0.2816	0.9951	1.0008	--	--	0.01	--	0.08	Snell. 'zx'= 122
1B	-265	295	72	1	0.2816	0.9951	1.0008	--	--	0.01	--	0.08	Snell. 'zx'= 122
1C	-265	-295	72	1	0.2816	0.9951	1.0008	--	--	0.01	--	0.08	Snell. 'zx'= 122
1D	-265	-295	72	1	0.2816	0.9951	1.0008	--	--	0.01	--	0.08	Snell. 'zx'= 122
1I	-122	108	72	1	0.2816	0.9978	1.0003	--	--	0.00	--	0.04	Snell. 'zx'= 122
1J	-122	108	72	1	0.2816	0.9978	1.0003	--	--	0.00	--	0.04	Snell. 'zx'= 122
1K	-122	-108	72	1	0.2816	0.9978	1.0003	--	--	0.00	--	0.04	Snell. 'zx'= 122
1L	-122	-108	72	1	0.2816	0.9978	1.0003	--	--	0.00	--	0.04	Snell. 'zx'= 122
1Q	-89	93	72	1	0.2816	0.9984	1.0003	--	--	0.00	--	0.03	Snell. 'zx'= 122
1R	-89	93	72	1	0.2816	0.9984	1.0003	--	--	0.00	--	0.03	Snell. 'zx'= 122
1S	-89	-93	72	1	0.2816	0.9984	1.0003	--	--	0.00	--	0.03	Snell. 'zx'= 122
1T	-89	-93	72	1	0.2816	0.9984	1.0003	--	--	0.00	--	0.03	Snell. 'zx'= 122
2	-387	-36	72	1	0.2816	0.9929	1.0011	--	--	0.01	--	0.02	Snell. 'zx'= 122
3	-232	-22	93	1	0.2816	0.9957	1.0020	--	--	0.00	--	0.02	Snell. 'zx'= 122
4	-232	-22	93	1	0.2816	0.9957	1.0020	--	--	0.00	--	0.02	Snell. 'zx'= 122
5	-387	-36	93	1	0.2816	0.9929	1.0034	--	--	0.01	--	0.03	Snell. 'zx'= 122
7	-1	8	93	1	0.2816	1.0000	1.0000	--	--	0.00	--	0.01	Snell. 'zx'= 122
22	-39	-6	0	1	0.2816	0.9993	1.0011	--	--	0.00	--	0.00	Snell. 'zx'= 122

ASTA NUM. 3 NI 8 NF 10 Lungh. 390.0 cm SEZ. 2 Pd UNP 160 Dist.= 0.015 m ali esterne

categoria: p.p. y qy tot.
qy medio: 37.68 37.68 kg/m

Sollecitazioni di calcolo e di verifica

Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
	cm	kg			kg*m							
1A	0	-152	73	38	0	74	0	1	0.00	0.00	0.02	
1B	0	-152	73	38	0	74	-0	1	0.00	0.00	0.02	
1C	0	-152	73	-38	0	-74	0	1	0.00	0.00	0.02	
1D	0	-152	73	-38	0	-74	-0	1	0.00	0.00	0.02	
1E	0	152	73	38	0	74	0	1	0.00	0.00	0.02	

1F	0	152	73	38	0	74	-0	1	0.00	0.00	0.02
1G	0	152	73	-38	0	-74	0	1	0.00	0.00	0.02
1H	0	152	73	-38	0	-74	-0	1	0.00	0.00	0.02
1I	0	-141	73	31	0	60	0	1	0.00	0.00	0.01
1J	0	-141	73	31	0	60	-0	1	0.00	0.00	0.01
1K	0	-141	73	-31	0	-60	0	1	0.00	0.00	0.01
1L	0	-141	73	-31	0	-60	-0	1	0.00	0.00	0.01
1M	0	141	73	31	0	60	0	1	0.00	0.00	0.01
1N	0	141	73	31	0	60	-0	1	0.00	0.00	0.01
1O	0	141	73	-31	0	-60	0	1	0.00	0.00	0.01
1P	0	141	73	-31	0	-60	-0	1	0.00	0.00	0.01
1Q	0	-68	73	16	0	31	0	1	0.00	0.00	0.01
1R	0	-68	73	16	0	31	-0	1	0.00	0.00	0.01
1S	0	-68	73	-16	0	-31	0	1	0.00	0.00	0.01
1T	0	-68	73	-16	0	-31	-0	1	0.00	0.00	0.01
1U	0	68	73	16	0	31	0	1	0.00	0.00	0.01
1V	0	68	73	16	0	31	-0	1	0.00	0.00	0.01
1W	0	68	73	-16	0	-31	0	1	0.00	0.00	0.01
1X	0	68	73	-16	0	-31	-0	1	0.00	0.00	0.01
2	0	231	73	-13	0	-26	0	1	0.00	0.00	0.01
3	0	139	96	-8	0	-15	0	1	0.00	0.00	0.00
4	0	139	96	-8	0	-15	0	1	0.00	0.00	0.00
5	0	231	96	-13	0	-26	0	1	0.00	0.00	0.01
7	0	47	96	-0	0	-1	0	1	0.00	0.00	0.00
20	0	67	96	-0	0	-1	0	1	0.00	0.00	0.00
22	0	-45	0	0	0	1	0	1	0.00	0.00	0.00
1A	195	-152	-0	38	0	0	72	1	0.00	0.00	0.01
1B	195	-152	0	38	0	0	72	1	0.00	0.00	0.01
1C	195	-152	-0	-38	0	-0	72	1	0.00	0.00	0.01
1D	195	-152	0	-38	0	-0	72	1	0.00	0.00	0.01
1E	195	152	-0	38	0	0	72	1	0.00	0.00	0.01
1F	195	152	0	38	0	0	72	1	0.00	0.00	0.01
1G	195	152	-0	-38	0	-0	72	1	0.00	0.00	0.01
1H	195	152	0	-38	0	-0	72	1	0.00	0.00	0.01
1I	195	-141	-0	31	0	0	72	1	0.00	0.00	0.01
1J	195	-141	0	31	0	0	72	1	0.00	0.00	0.01
1K	195	-141	-0	-31	0	-0	72	1	0.00	0.00	0.01
1L	195	-141	0	-31	0	-0	72	1	0.00	0.00	0.01
1M	195	141	-0	31	0	0	72	1	0.00	0.00	0.01
1N	195	141	0	31	0	0	72	1	0.00	0.00	0.01
1O	195	141	-0	-31	0	-0	72	1	0.00	0.00	0.01
1P	195	141	0	-31	0	-0	72	1	0.00	0.00	0.01
1Q	195	-68	-0	16	0	0	72	1	0.00	0.00	0.01
1R	195	-68	0	16	0	0	72	1	0.00	0.00	0.01
1S	195	-68	-0	-16	0	-0	72	1	0.00	0.00	0.01
1T	195	-68	0	-16	0	-0	72	1	0.00	0.00	0.01
1U	195	68	-0	16	0	0	72	1	0.00	0.00	0.01
1V	195	68	0	16	0	0	72	1	0.00	0.00	0.01
1W	195	68	-0	-16	0	-0	72	1	0.00	0.00	0.01
1X	195	68	0	-16	0	-0	72	1	0.00	0.00	0.01
2	195	231	0	-13	0	-0	72	1	0.00	0.00	0.01
3	195	139	0	-8	0	-0	93	1	0.00	0.00	0.01
4	195	139	0	-8	0	-0	93	1	0.00	0.00	0.01
5	195	231	0	-13	0	-0	93	1	0.00	0.00	0.01
7	195	47	0	-0	0	-0	93	1	0.00	0.00	0.01
20	195	67	0	-0	0	-0	93	1	0.00	0.00	0.01
22	195	-45	0	0	0	0	0	1	0.00	0.00	0.00
1A	390	-152	-73	38	0	-73	0	1	0.00	0.00	0.02
1B	390	-152	-73	38	0	-73	0	1	0.00	0.00	0.02
1C	390	-152	-73	-38	0	73	0	1	0.00	0.00	0.02
1D	390	-152	-73	-38	0	73	0	1	0.00	0.00	0.02
1E	390	152	-73	38	0	-73	0	1	0.00	0.00	0.02
1F	390	152	-73	38	0	-73	0	1	0.00	0.00	0.02
1G	390	152	-73	-38	0	73	0	1	0.00	0.00	0.02
1H	390	152	-73	-38	0	73	0	1	0.00	0.00	0.02
1I	390	-141	-73	31	0	-60	0	1	0.00	0.00	0.01
1J	390	-141	-73	31	0	-60	0	1	0.00	0.00	0.01
1K	390	-141	-73	-31	0	60	0	1	0.00	0.00	0.01
1L	390	-141	-73	-31	0	60	0	1	0.00	0.00	0.01
1M	390	141	-73	31	0	-60	0	1	0.00	0.00	0.01
1N	390	141	-73	31	0	-60	0	1	0.00	0.00	0.01
1O	390	141	-73	-31	0	60	0	1	0.00	0.00	0.01
1P	390	141	-73	-31	0	60	0	1	0.00	0.00	0.01
1Q	390	-68	-73	16	0	-31	0	1	0.00	0.00	0.01
1R	390	-68	-73	16	0	-31	0	1	0.00	0.00	0.01
1S	390	-68	-73	-16	0	31	0	1	0.00	0.00	0.01
1T	390	-68	-73	-16	0	31	0	1	0.00	0.00	0.01
1U	390	68	-73	16	0	-31	0	1	0.00	0.00	0.01
1V	390	68	-73	16	0	-31	0	1	0.00	0.00	0.01
1W	390	68	-73	-16	0	31	0	1	0.00	0.00	0.01
1X	390	68	-73	-16	0	31	0	1	0.00	0.00	0.01
2	390	231	-73	-13	0	26	0	1	0.00	0.00	0.01
3	390	139	-96	-8	0	15	0	1	0.00	0.00	0.00
4	390	139	-96	-8	0	15	0	1	0.00	0.00	0.00
5	390	231	-96	-13	0	26	0	1	0.00	0.00	0.01
7	390	47	-96	-0	0	1	0	1	0.00	0.00	0.00
20	390	67	-96	-0	0	1	0	1	0.00	0.00	0.00
22	390	-45	0	0	0	-0	0	1	0.00	0.00	0.00

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx	My	Mz	Classe	γ_{min}	ky	kz	kLT	χ_{LT}	I.S.n.	I.S.m.	I.S.	Nota
	kg	kg*m											

1A	-152	74	72	1	0.2816	0.9972	1.0004	--	--	0.00	--	0.03	Snell.	'zx'=' 122
1B	-152	74	72	1	0.2816	0.9972	1.0004	--	--	0.00	--	0.03	Snell.	'zx'=' 122
1C	-152	-74	72	1	0.2816	0.9972	1.0004	--	--	0.00	--	0.03	Snell.	'zx'=' 122
1D	-152	-74	72	1	0.2816	0.9972	1.0004	--	--	0.00	--	0.03	Snell.	'zx'=' 122
1I	-141	60	72	1	0.2816	0.9974	1.0004	--	--	0.00	--	0.02	Snell.	'zx'=' 122
1J	-141	60	72	1	0.2816	0.9974	1.0004	--	--	0.00	--	0.02	Snell.	'zx'=' 122
1K	-141	-60	72	1	0.2816	0.9974	1.0004	--	--	0.00	--	0.02	Snell.	'zx'=' 122
1L	-141	-60	72	1	0.2816	0.9974	1.0004	--	--	0.00	--	0.02	Snell.	'zx'=' 122
1Q	-68	31	72	1	0.2816	0.9988	1.0002	--	--	0.00	--	0.02	Snell.	'zx'=' 122
1R	-68	31	72	1	0.2816	0.9988	1.0002	--	--	0.00	--	0.02	Snell.	'zx'=' 122
1S	-68	-31	72	1	0.2816	0.9988	1.0002	--	--	0.00	--	0.02	Snell.	'zx'=' 122
1T	-68	-31	72	1	0.2816	0.9988	1.0002	--	--	0.00	--	0.02	Snell.	'zx'=' 122
22	-45	1	0	1	0.2816	0.9992	1.0013	--	--	0.00	--	0.00	Snell.	'zx'=' 122

ASTA NUM. 4 NI 6 NF 5 Lungh. 390.0 cm SEZ. 2 Pd UNP 160 Dist.= 0.015 m ali esterne

categoria: p.p. y qy tot.

qy medio: 37.68 37.68 kg/m

Sollecitazioni di calcolo e di verifica

Indici <= 1 : VERIFICATO

NC	x	Fx	Fy	Fz	Mx	My	Mz	Classe	I.V.T.	I.R.n.	I.R.	Nota
--	cm	kg			kg*m							
1A	0	-6515	73	59	0	117	0	1	0.00	0.04	0.07	
1B	0	-6515	73	59	0	117	-0	1	0.00	0.04	0.07	
1C	0	-6515	73	-59	0	-117	0	1	0.00	0.04	0.07	
1D	0	-6515	73	-59	0	-117	-0	1	0.00	0.04	0.07	
1E	0	6515	73	59	0	117	0	1	0.00	0.04	0.07	
1F	0	6515	73	59	0	117	-0	1	0.00	0.04	0.07	
1G	0	6515	73	-59	0	-117	0	1	0.00	0.04	0.07	
1H	0	6515	73	-59	0	-117	-0	1	0.00	0.04	0.07	
1I	0	-3813	73	61	0	119	0	1	0.00	0.02	0.05	
1J	0	-3813	73	61	0	119	-0	1	0.00	0.02	0.05	
1K	0	-3813	73	-61	0	-119	0	1	0.00	0.02	0.05	
1L	0	-3813	73	-61	0	-119	-0	1	0.00	0.02	0.05	
1M	0	3813	73	61	0	119	0	1	0.00	0.02	0.05	
1N	0	3813	73	61	0	119	-0	1	0.00	0.02	0.05	
1O	0	3813	73	-61	0	-119	0	1	0.00	0.02	0.05	
1P	0	3813	73	-61	0	-119	-0	1	0.00	0.02	0.05	
1Q	0	-2383	73	28	0	54	0	1	0.00	0.01	0.03	
1R	0	-2383	73	28	0	54	-0	1	0.00	0.01	0.03	
1S	0	-2383	73	-28	0	-54	0	1	0.00	0.01	0.03	
1T	0	-2383	73	-28	0	-54	-0	1	0.00	0.01	0.03	
1U	0	2383	73	28	0	54	0	1	0.00	0.01	0.03	
1V	0	2383	73	28	0	54	-0	1	0.00	0.01	0.03	
1W	0	2383	73	-28	0	-54	0	1	0.00	0.01	0.03	
1X	0	2383	73	-28	0	-54	-0	1	0.00	0.01	0.03	
2	0	-1915	96	5	0	24	0	1	0.00	0.01	0.02	
3	0	-1149	96	5	0	14	0	1	0.00	0.01	0.01	
4	0	-1149	96	5	0	14	0	1	0.00	0.01	0.01	
5	0	-1915	96	9	0	24	0	1	0.00	0.01	0.02	
7	0	-374	96	-4	0	-7	0	1	0.00	0.00	0.00	
20	0	-373	96	-4	0	-8	0	1	0.00	0.00	0.00	
22	0	249	0	3	0	5	0	1	0.00	0.00	0.00	
1A	195	-6515	-0	59	0	2	72	1	0.00	0.04	0.05	
1B	195	-6515	0	59	0	2	72	1	0.00	0.04	0.05	
1C	195	-6515	-0	-59	0	-2	72	1	0.00	0.04	0.05	
1D	195	-6515	0	-59	0	-2	72	1	0.00	0.04	0.05	
1E	195	6515	-0	59	0	2	72	1	0.00	0.04	0.05	
1F	195	6515	0	59	0	2	72	1	0.00	0.04	0.05	
1G	195	6515	-0	-59	0	-2	72	1	0.00	0.04	0.05	
1H	195	6515	0	-59	0	-2	72	1	0.00	0.04	0.05	
1I	195	-3813	-0	61	0	1	72	1	0.00	0.02	0.03	
1J	195	-3813	0	61	0	1	72	1	0.00	0.02	0.03	
1K	195	-3813	-0	-61	0	-1	72	1	0.00	0.02	0.03	
1L	195	-3813	0	-61	0	-1	72	1	0.00	0.02	0.03	
1M	195	3813	-0	61	0	1	72	1	0.00	0.02	0.03	
1N	195	3813	0	61	0	1	72	1	0.00	0.02	0.03	
1O	195	3813	-0	-61	0	-1	72	1	0.00	0.02	0.03	
1P	195	3813	0	-61	0	-1	72	1	0.00	0.02	0.03	
1Q	195	-2383	-0	28	0	1	72	1	0.00	0.01	0.02	
1R	195	-2383	0	28	0	1	72	1	0.00	0.01	0.02	
1S	195	-2383	-0	-28	0	-1	72	1	0.00	0.01	0.02	
1T	195	-2383	0	-28	0	-1	72	1	0.00	0.01	0.02	
1U	195	2383	-0	28	0	1	72	1	0.00	0.01	0.02	
1V	195	2383	0	28	0	1	72	1	0.00	0.01	0.02	
1W	195	2383	-0	-28	0	-1	72	1	0.00	0.01	0.02	
1X	195	2383	0	-28	0	-1	72	1	0.00	0.01	0.02	
2	195	-1915	0	9	0	7	72	1	0.00	0.01	0.02	
3	195	-1149	0	5	0	4	93	1	0.00	0.01	0.02	
4	195	-1149	0	5	0	4	93	1	0.00	0.01	0.02	
5	195	-1915	0	9	0	7	93	1	0.00	0.01	0.02	
7	195	-374	0	-4	0	-0	93	1	0.00	0.00	0.01	
20	195	-373	0	-4	0	-0	93	1	0.00	0.00	0.01	
22	195	249	0	3	0	0	0	1	0.00	0.00	0.00	
1A	390	-6515	-73	59	0	-113	0	1	0.00	0.04	0.07	
1B	390	-6515	-73	59	0	-113	0	1	0.00	0.04	0.07	
1C	390	-6515	-73	-59	0	113	0	1	0.00	0.04	0.07	
1D	390	-6515	-73	-59	0	113	0	1	0.00	0.04	0.07	
1E	390	6515	-73	59	0	-113	0	1	0.00	0.04	0.07	
1F	390	6515	-73	59	0	-113	0	1	0.00	0.04	0.07	
1G	390	6515	-73	-59	0	113	0	1	0.00	0.04	0.07	
1H	390	6515	-73	-59	0	113	0	1	0.00	0.04	0.07	
1I	390	-3813	-73	61	0	-117	0	1	0.00	0.02	0.05	
1J	390	-3813	-73	61	0	-117	0	1	0.00	0.02	0.05	
1K	390	-3813	-73	-61	0	117	0	1	0.00	0.02	0.05	

1L	390	-3813	-73	-61	0	117	0	1	0.00	0.02	0.05	
1M	390	3813	-73	61	0	-117	0	1	0.00	0.02	0.05	
1N	390	3813	-73	61	0	-117	0	1	0.00	0.02	0.05	
1O	390	3813	-73	-61	0	117	0	1	0.00	0.02	0.05	
1P	390	3813	-73	-61	0	117	0	1	0.00	0.02	0.05	
1Q	390	-2383	-73	28	0	-53	0	1	0.00	0.01	0.03	
1R	390	-2383	-73	28	0	-53	0	1	0.00	0.01	0.03	
1S	390	-2383	-73	-28	0	53	0	1	0.00	0.01	0.03	
1T	390	-2383	-73	-28	0	53	0	1	0.00	0.01	0.03	
1U	390	2383	-73	28	0	-53	0	1	0.00	0.01	0.03	
1V	390	2383	-73	28	0	-53	0	1	0.00	0.01	0.03	
1W	390	2383	-73	-28	0	53	0	1	0.00	0.01	0.03	
1X	390	2383	-73	-28	0	53	0	1	0.00	0.01	0.03	
2	390	-1915	-73	9	0	-10	0	1	0.00	0.01	0.01	
3	390	-1149	-96	5	0	-6	0	1	0.00	0.01	0.01	
4	390	-1149	-96	5	0	-6	0	1	0.00	0.01	0.01	
5	390	-1915	-96	9	0	-10	0	1	0.00	0.01	0.01	
7	390	-374	-96	-4	0	7	0	1	0.00	0.00	0.00	
20	390	-373	-96	-4	0	7	0	1	0.00	0.00	0.00	
22	390	249	0	3	0	-5	0	1	0.00	0.00	0.00	

Verifica di STABILITA' e/o STABILITA' FLESSO TORSIONALE

NC	Fx -- kg	My ----- kg*m	Mz	Classe	$\gamma_{min.}$	ky	kz	kLT	χ_{LT}	I.S.n.	I.S.m.	I.S.	Nota
1A	-6515	117	72	1	0.2816	0.8801	1.0187	--	--	0.14	--	0.17	Snell. 'zx'= 122
1B	-6515	117	72	1	0.2816	0.8801	1.0187	--	--	0.14	--	0.17	Snell. 'zx'= 122
1C	-6515	-117	72	1	0.2816	0.8801	1.0187	--	--	0.14	--	0.17	Snell. 'zx'= 122
1D	-6515	-117	72	1	0.2816	0.8801	1.0187	--	--	0.14	--	0.17	Snell. 'zx'= 122
1I	-3813	119	72	1	0.2816	0.9298	1.0110	--	--	0.08	--	0.12	Snell. 'zx'= 122
1J	-3813	119	72	1	0.2816	0.9298	1.0110	--	--	0.08	--	0.12	Snell. 'zx'= 122
1K	-3813	-119	72	1	0.2816	0.9298	1.0110	--	--	0.08	--	0.12	Snell. 'zx'= 122
1L	-3813	-119	72	1	0.2816	0.9298	1.0110	--	--	0.08	--	0.12	Snell. 'zx'= 122
1Q	-2383	54	72	1	0.2816	0.9562	1.0068	--	--	0.05	--	0.07	Snell. 'zx'= 122
1R	-2383	54	72	1	0.2816	0.9562	1.0068	--	--	0.05	--	0.07	Snell. 'zx'= 122
1S	-2383	-54	72	1	0.2816	0.9562	1.0068	--	--	0.05	--	0.07	Snell. 'zx'= 122
1T	-2383	-54	72	1	0.2816	0.9562	1.0068	--	--	0.05	--	0.07	Snell. 'zx'= 122
2	-1915	24	72	1	0.2816	0.9648	1.0055	--	--	0.04	--	0.05	Snell. 'zx'= 122
3	-1149	14	93	1	0.2816	0.9789	1.0100	--	--	0.02	--	0.04	Snell. 'zx'= 122
4	-1149	14	93	1	0.2816	0.9789	1.0100	--	--	0.02	--	0.04	Snell. 'zx'= 122
5	-1915	24	93	1	0.2816	0.9648	1.0166	--	--	0.04	--	0.06	Snell. 'zx'= 122
7	-374	-7	93	1	0.2816	0.9931	1.0032	--	--	0.01	--	0.02	Snell. 'zx'= 122
20	-373	-8	93	1	0.2816	0.9931	1.0032	--	--	0.01	--	0.02	Snell. 'zx'= 122

Verifiche locali

Si riportano le verifiche degli elementi non contemplati nel modello.

VERIFICA GIUNTO DIAGONALE DI CONTROVENTO

I controventi sono stati previsti per stabilizzare le fasi di montaggio. Una volta gettate le lastre Predalles tali diagonali potrebbero essere anche smontate.

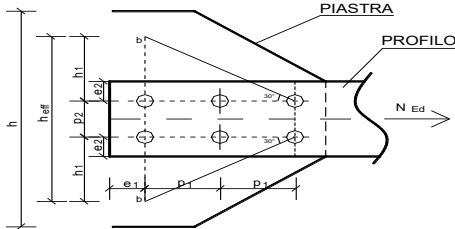
Il diagonale di controvento di piano (profilo ad L80x8) è collegato agli estremi mediante un piatto $s=15$ mm e 2 bulloni M16 Classe 8.8.

Il giunto maggiormente sollecitato è soggetto ad un'azione pari :

$$N = 2 \times 17 \approx 20 \text{ kN.}$$

DATI DI PROGETTO

R1



e ₁	=	50	mm
e ₂	=	40	mm
p ₂	=	0	mm
p ₁	=	65	mm

Sporgenza piatto rispetto al profilo	S _{sup}	=	0	mm
Sporgenza piatto rispetto al profilo	S _{inf}	=	0	mm
Spessore della piastra di collegamento	t _p	=	15	mm
Spessore del profilo collegato	t _{pr}	=	8	mm
Materiale della piastra			S355	
Numero colonne di bulloni	n ^o _{col}	=	2	
Numero di bulloni per colonna	n ^o _{b,col}	=	1	
Numero totale di bulloni	n ^o _{tot,b}	=	2	
Numero piani di taglio dei bulloni	n ^o _{p.taglio}	=	1	
Bulloni			20	
Classe			8.8	
Diametro nominale del gambo del bullone	d	=	16	mm
Diametro nominale del foro di alloggiamento del bullone	d _o	=	17	mm
Diametro della testa del dado	d _m	=	24	mm
Area resistente della vite	A _{res}	=	157	mm ²
Tensione di snervamento del materiale del bullone	f _{yb}	=	640	N/mm ²
Tensione di rottura del materiale del bullone	f _{tb}	=	800	N/mm ²
Tensione di rottura del materiale del piatto	f _{tk}	=	510	N/mm ²
Coefficienti di sicurezza (Tab. 4.2.XII- NTC 2008)	γ _{M2}	=	1.25	

VERIFICA BULLONI

Coefficiente k per bulloni di bordo	k	=	min(2,8e ₂ /d _o -1,7;2,5)=	2.50	
Coefficiente k per bulloni interni	k	=	min(1,4p ₂ /d _o -1,7;2,5)=		
Coefficiente α per bulloni di bordo	α	=	min(e ₁ /3d _o ;f _{tb} /f _{tk} ;1)=	0.98	
Coefficiente α per bulloni interni	α	=	min(p ₁ /3d _o -0,25;f _{tb} /f _{tk} ;1)=	1.00	
Resistenza di calcolo a taglio dei bulloni per piano di taglio	F _{v,Rd}	=	0.6 f _{tb} A _{res} /γ _{M2} =	60.29	kN
Resistenza di calcolo a taglio dei bulloni	F _{v,Rd,tot}	=	n ^o _{p.taglio} F _{v,Rd}	60.29	kN
Resistenza di calcolo a rifollamento per bulloni interni	F _{b,Rd}	=	kαf _{tk} dt/γ _{M2} =		kN
Resistenza di calcolo a rifollamento per bulloni di bordo	F _{b,Rd}	=	kαf _{tk} dt/γ _{M2} =	128.00	kN
Azione esterna agente	N _{Ed}	=		20	kN
Sforzo di taglio nel bullone più sollecitato	F _{v,Ed}	=	N _{Ed} /n ^o _{tot,b} =	10.0	kN
La resistenza complessiva della singola unione a taglio è data da	F _{v,Rd}	=	min(F _{v,Rd,tot} ;F _{b,Rd})=	60.29	kN
	F _{v,Ed} /F _{v,Rd}	=		0.17	< 1

Verificato

VERIFICA PIATTO

Altezza efficace	h ₁	=	(n ^o _{col} -1)p ₁ tan30°=	38	mm
	h _{eff}	=		75	mm
Area resistente netta	A _{netta}	=	(h _{eff} -n ^o _{b,col} d _o)t _p =	871	mm ²
Resistenza a rottura della sezione netta	N _{u,Rd}	=	0.9A _{netta} f _{tk} /γ _{M2} =	320	kN
	N _{Ed} /N _{u,Rd}	=		0.06	< 1

Verificato

VERIFICA APPOGGIO ESTREMITÀ "A"

L'appoggio all'estremità "A" ha le traslazioni impedito nelle 3 direzioni X, Y e Z. Il giunto è realizzato con quattro tirafondi M24 L=700 mm con piastrina di estremità 120x120x20 annegata nel cls.

Le massime azioni agenti si hanno per la combinazione sismica e valgono:

$$F_x = 8000 \text{ kg}$$

$$F_y = 17000 \text{ kg}$$

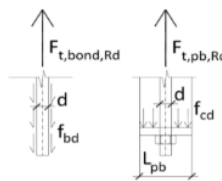
Non si hanno azioni a strappo.

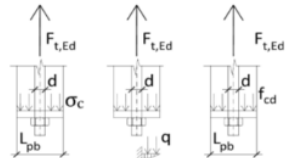
Il singolo tirafondo è soggetto ad un'azione di taglio pari a:

$$F_{v,Rd} = (F_x^2 + F_y^2)^{0.5} / 4 = 5000 \text{ kg}$$

VERIFICA TIRAFONDI			
Rif. UNI EN 1993 - 1 - 8			
DATI GEOMETRICI			
Materiali			
Acciaio da carpenteria			S 355
Tensione di snervamento	$f_y =$	355	N/mm ²
Tensione di rottura	$f_t =$	510	N/mm ²
Coefficiente di sicurezza parziale per l'acciaio (resistenza)	$\gamma_{M0} =$	1.05	-
Coefficiente di sicurezza parziale per l'acciaio (stabilità)	$\gamma_{M1} =$	1.05	-
Acciaio per tirafondi			8.8
Resistenza a snervamento	$f_{y0} =$	640	N/mm ²
Resistenza ultima	$f_{ub} =$	800	N/mm ²
Coefficiente di sicurezza parziale per l'acciaio (connessioni)	$\gamma_{M2} =$	1.25	-
Piastra di base			
Spessore	$t_p =$	30	mm
Piastra annegata			
Lato	$L_{pb} =$	120	mm
Spessore	$s_{pb} =$	20	mm
Tirafondi			
Diametro gambo tirafondo	$d =$	24	mm
Diametro del foro	$d_0 =$	26	mm
Diametro medio della testa del bullone	$d_m =$	36	mm
Area porzione filettata gambo	$A_{es} =$	353	mm ²
Lunghezza di ancoraggio	$L =$	500	mm
Spessore malta di allettamento	$s =$	50	mm
Area porzione non filettata gambo	$A = \pi d^2 / 4 =$	452	mm ²
	Nr. Tirafondi	p_2	
1° Riga	2	$e_1 = 100$	140 mm
2° Riga	2	$p_{1,1} = 300$	140 mm
3° Riga		$p_{1,2} =$	mm
4° Riga		$p_{1,3} =$	mm
5° Riga		$p_{1,4} =$	mm
Distanza tirafondi da bordo in direzione verticale		$e_2 =$	80 mm

Tirafondi: resistenza e sfilamento [rif. §6.2.6.12]



<p>Resistenza caratteristica cilindrica cls fondazione</p> <p>Lunghezza di ancoraggio</p> <p>Coefficiente che tiene conto del diametro del tirafondo</p> <p>Coefficiente di sicurezza parziale per il calcestruzzo</p> <p>Resistenza per aderenza di progetto relativa alle barre lisce</p> <p>Resistenza per aderenza acciaio-calcestruzzo del singolo tirafondo</p> <p>Area piastra annegata non forata</p> <p>Resistenza di progetto a compressione del cls fondazione</p> <p>Resistenza a trazione offerta dalla piastra annegata</p> <p>Resistenza a trazione del gambo filettato del tirafondo</p> <p>Resistenza a taglio del gambo filettato del tirafondo</p> <p>Coefficiente k per bulloni di bordo</p> <p>Coefficiente k per bulloni interni</p> <p>Coefficiente a per bulloni di bordo</p> <p>Coefficiente a per bulloni interni</p> <p>Resistenza di calcolo a rifollamento per bulloni interni</p> <p>Resistenza di calcolo a rifollamento per bulloni di bordo</p> <p>Resistenza di calcolo a punzonamento del piatto</p> <p>Resistenza di progetto a trazione dell'ancoraggio privo di piastra annegata</p> <p>Resistenza di progetto a trazione dell'ancoraggio con piastra annegata</p> <p>Resistenza di progetto a taglio del gambo filettato del tirafondo</p> <p>Numero totale di tirafondi</p> <p>Forza sollecitante a trazione sul singolo bullone</p> <p>Forza sollecitante a taglio</p>	<table border="0" style="width: 100%;"> <tr> <td>$f_{ck} =$</td> <td style="border: 1px solid black; padding: 2px;">25</td> <td>N/mm²</td> </tr> <tr> <td>$L_0 = L - s =$</td> <td style="border: 1px solid black; padding: 2px;">450</td> <td>mm</td> </tr> <tr> <td>$\eta = 1$ se $d \leq 32\text{mm}$</td> <td style="border: 1px solid black; padding: 2px;">1</td> <td>-</td> </tr> <tr> <td>$\eta = (132-d)/100$ se $d > 32\text{mm}$</td> <td></td> <td></td> </tr> <tr> <td>$\gamma_c =$</td> <td style="border: 1px solid black; padding: 2px;">1.5</td> <td>-</td> </tr> <tr> <td>$f_{bd} = \eta \cdot 0.7 \cdot (0.3 \cdot f_{ck}^{2/3}) \cdot \gamma_c$</td> <td style="border: 1px solid black; padding: 2px;">1.2</td> <td>N/mm²</td> </tr> <tr> <td>$F_{L,bond,Rd} = \pi \cdot d \cdot L_b \cdot f_{bd}$</td> <td style="border: 1px solid black; padding: 2px;">41</td> <td>kN</td> </tr> <tr> <td>$A_{CO,pb} = L_{pb} \cdot d$</td> <td style="border: 1px solid black; padding: 2px;">14400</td> <td>mm²</td> </tr> <tr> <td>$f_{cd} =$</td> <td style="border: 1px solid black; padding: 2px;">14.17</td> <td>N/mm²</td> </tr> <tr> <td>$F_{L,pb,Rd} = (A_{CO,pb} - \pi \cdot d^2/4) \cdot f_{cd}$</td> <td style="border: 1px solid black; padding: 2px;">198</td> <td>kN</td> </tr> <tr> <td>$F_{L,Rd} = 0.9 \cdot A_{res} \cdot f_{td} / \gamma_{M2}$</td> <td style="border: 1px solid black; padding: 2px;">203</td> <td>kN</td> </tr> <tr> <td>$F_{V,Rd} = 0.6 \cdot A \cdot f_{td} / \gamma_{M2}$</td> <td style="border: 1px solid black; padding: 2px;">174</td> <td>kN</td> </tr> <tr> <td>$k = \min(2.8e_2/d_0 - 1.7; 2.5)$</td> <td style="border: 1px solid black; padding: 2px;">2.5</td> <td>-</td> </tr> <tr> <td>$k = \min(1.4p_2/d_0 - 1.7; 2.5)$</td> <td style="border: 1px solid black; padding: 2px;">2.5</td> <td>-</td> </tr> <tr> <td>$\alpha = \min(e_1/3d_0; f_{td}/f_t; 1)$</td> <td style="border: 1px solid black; padding: 2px;">1.0</td> <td>-</td> </tr> <tr> <td>$\alpha = \min(p_1/3d_0 - 0.25; f_{td}/f_t; 1)$</td> <td style="border: 1px solid black; padding: 2px;">1.0</td> <td>-</td> </tr> <tr> <td>$F_{D,Rd} = k \cdot \alpha \cdot f_{tk} \cdot d \cdot t_p / \gamma_{M2}$</td> <td style="border: 1px solid black; padding: 2px;">734</td> <td>kN</td> </tr> <tr> <td>$F_{D,Rd} = k \cdot \alpha \cdot f_{tk} \cdot d \cdot t_p / \gamma_{M2}$</td> <td style="border: 1px solid black; padding: 2px;">734</td> <td>kN</td> </tr> <tr> <td>$B_{p,Rd} = 0.6 \cdot \pi \cdot f_{tk} \cdot d_{si} \cdot t_p / \gamma_{M2}$</td> <td style="border: 1px solid black; padding: 2px;">831</td> <td>kN</td> </tr> <tr> <td>$F_{L,anchor,Rd} = \min(F_{L,Rd}; B_{D,Rd}; F_{L,bond,Rd})$</td> <td style="border: 1px solid black; padding: 2px;">41</td> <td>kN</td> </tr> <tr> <td>$F_{L,anchor,Rd} = \min(F_{L,Rd}; B_{D,Rd}; F_{L,pb,Rd})$</td> <td style="border: 1px solid black; padding: 2px;">198</td> <td>kN</td> </tr> <tr> <td>$F_{V,anchor,Rd} = \min(F_{V,Rd}; F_{D,Rd})$</td> <td style="border: 1px solid black; padding: 2px;">174</td> <td>kN</td> </tr> <tr> <td>$n_b =$</td> <td style="border: 1px solid black; padding: 2px;">4</td> <td></td> </tr> <tr> <td>$F_{L,Ed} = \sigma_c \cdot A_{res}$</td> <td style="border: 1px solid black; padding: 2px;">0</td> <td>kN</td> </tr> <tr> <td>$F_{V,Ed} = V_{Ed} / n_b$</td> <td style="border: 1px solid black; padding: 2px;">50</td> <td>kN</td> </tr> <tr> <td>$F_{V,Ed} / F_{V,anchor,Rd} + F_{L,Ed} / 1.4 \cdot F_{L,anchor,Rd}$</td> <td style="border: 1px solid black; padding: 2px;">0.29</td> <td>≤ 1 VERIFICATO</td> </tr> <tr> <td>$F_{L,Ed} / F_{L,anchor,Rd}$</td> <td style="border: 1px solid black; padding: 2px;">0.00</td> <td>≤ 1 VERIFICATO</td> </tr> </table> <p style="text-align: center;">COMBINAZIONE DI TRAZIONE E TAGLIO</p> <div style="display: flex; justify-content: space-around; align-items: center;">  </div> <table border="0" style="width: 100%; border-collapse: collapse;"> <tr> <td style="width: 50%; vertical-align: top;"> <p>Carico sulla piastra annegata (schema a mensola)</p> <p>Luce mensola</p> <p>Momento sezione di incastro</p> <p>Momento d'inerzia</p> <p>Momento resistente</p> <p>Tensione tangenziale sulla sup. laterale del cilindro cls</p> <p>VERIFICA A COMPRESIONE CLS SOPRA LA PIASTRA ANNEGATA</p> <p>VERIFICA DI RESISTENZA PIASTRA ANNEGATA</p> <p>VERIFICA A SFILAMENTO DEL CILINDRO DI CALCESTRUZZO</p> </td> <td style="width: 50%; vertical-align: top;"> <table border="0" style="width: 100%;"> <tr> <td>$q = F_{L,Ed} / A_{CO,pb} \cdot 1\text{mm}$</td> <td style="border: 1px solid black; padding: 2px;">0.00</td> <td>N/mm</td> </tr> <tr> <td>$L = (L_{pb} - d)/2$</td> <td style="border: 1px solid black; padding: 2px;">48.00</td> <td>mm</td> </tr> <tr> <td>$M = qL^2/2$</td> <td style="border: 1px solid black; padding: 2px;">0</td> <td>Nmm</td> </tr> <tr> <td>$W = 1s_{pb}^2/6$</td> <td style="border: 1px solid black; padding: 2px;">66.67</td> <td>mm²</td> </tr> <tr> <td>$M_{Rd} = W \cdot f_{yd}$</td> <td style="border: 1px solid black; padding: 2px;">22540</td> <td>Nmm</td> </tr> <tr> <td>$\tau = F_{L,Ed} / (4L_{pb} \cdot L)$</td> <td style="border: 1px solid black; padding: 2px;">0.00</td> <td>N/mm²</td> </tr> <tr> <td>$F_{L,Ed} / F_{L,pb,Rd}$</td> <td style="border: 1px solid black; padding: 2px;">0.00</td> <td>≤ 1 VERIFICATO</td> </tr> <tr> <td>M_{Ed} / M_{Rd}</td> <td style="border: 1px solid black; padding: 2px;">0.00</td> <td>≤ 1 VERIFICATO</td> </tr> <tr> <td>τ / f_{bd}</td> <td style="border: 1px solid black; padding: 2px;">0.00</td> <td>≤ 1 VERIFICATO</td> </tr> </table> </td> </tr> </table> <p style="text-align: right;">Pag.2</p>	$f_{ck} =$	25	N/mm ²	$L_0 = L - s =$	450	mm	$\eta = 1$ se $d \leq 32\text{mm}$	1	-	$\eta = (132-d)/100$ se $d > 32\text{mm}$			$\gamma_c =$	1.5	-	$f_{bd} = \eta \cdot 0.7 \cdot (0.3 \cdot f_{ck}^{2/3}) \cdot \gamma_c$	1.2	N/mm ²	$F_{L,bond,Rd} = \pi \cdot d \cdot L_b \cdot f_{bd}$	41	kN	$A_{CO,pb} = L_{pb} \cdot d$	14400	mm ²	$f_{cd} =$	14.17	N/mm ²	$F_{L,pb,Rd} = (A_{CO,pb} - \pi \cdot d^2/4) \cdot f_{cd}$	198	kN	$F_{L,Rd} = 0.9 \cdot A_{res} \cdot f_{td} / \gamma_{M2}$	203	kN	$F_{V,Rd} = 0.6 \cdot A \cdot f_{td} / \gamma_{M2}$	174	kN	$k = \min(2.8e_2/d_0 - 1.7; 2.5)$	2.5	-	$k = \min(1.4p_2/d_0 - 1.7; 2.5)$	2.5	-	$\alpha = \min(e_1/3d_0; f_{td}/f_t; 1)$	1.0	-	$\alpha = \min(p_1/3d_0 - 0.25; f_{td}/f_t; 1)$	1.0	-	$F_{D,Rd} = k \cdot \alpha \cdot f_{tk} \cdot d \cdot t_p / \gamma_{M2}$	734	kN	$F_{D,Rd} = k \cdot \alpha \cdot f_{tk} \cdot d \cdot t_p / \gamma_{M2}$	734	kN	$B_{p,Rd} = 0.6 \cdot \pi \cdot f_{tk} \cdot d_{si} \cdot t_p / \gamma_{M2}$	831	kN	$F_{L,anchor,Rd} = \min(F_{L,Rd}; B_{D,Rd}; F_{L,bond,Rd})$	41	kN	$F_{L,anchor,Rd} = \min(F_{L,Rd}; B_{D,Rd}; F_{L,pb,Rd})$	198	kN	$F_{V,anchor,Rd} = \min(F_{V,Rd}; F_{D,Rd})$	174	kN	$n_b =$	4		$F_{L,Ed} = \sigma_c \cdot A_{res}$	0	kN	$F_{V,Ed} = V_{Ed} / n_b$	50	kN	$F_{V,Ed} / F_{V,anchor,Rd} + F_{L,Ed} / 1.4 \cdot F_{L,anchor,Rd}$	0.29	≤ 1 VERIFICATO	$F_{L,Ed} / F_{L,anchor,Rd}$	0.00	≤ 1 VERIFICATO	<p>Carico sulla piastra annegata (schema a mensola)</p> <p>Luce mensola</p> <p>Momento sezione di incastro</p> <p>Momento d'inerzia</p> <p>Momento resistente</p> <p>Tensione tangenziale sulla sup. laterale del cilindro cls</p> <p>VERIFICA A COMPRESIONE CLS SOPRA LA PIASTRA ANNEGATA</p> <p>VERIFICA DI RESISTENZA PIASTRA ANNEGATA</p> <p>VERIFICA A SFILAMENTO DEL CILINDRO DI CALCESTRUZZO</p>	<table border="0" style="width: 100%;"> <tr> <td>$q = F_{L,Ed} / A_{CO,pb} \cdot 1\text{mm}$</td> <td style="border: 1px solid black; padding: 2px;">0.00</td> <td>N/mm</td> </tr> <tr> <td>$L = (L_{pb} - d)/2$</td> <td style="border: 1px solid black; padding: 2px;">48.00</td> <td>mm</td> </tr> <tr> <td>$M = qL^2/2$</td> <td style="border: 1px solid black; padding: 2px;">0</td> <td>Nmm</td> </tr> <tr> <td>$W = 1s_{pb}^2/6$</td> <td style="border: 1px solid black; padding: 2px;">66.67</td> <td>mm²</td> </tr> <tr> <td>$M_{Rd} = W \cdot f_{yd}$</td> <td style="border: 1px solid black; padding: 2px;">22540</td> <td>Nmm</td> </tr> <tr> <td>$\tau = F_{L,Ed} / (4L_{pb} \cdot L)$</td> <td style="border: 1px solid black; padding: 2px;">0.00</td> <td>N/mm²</td> </tr> <tr> <td>$F_{L,Ed} / F_{L,pb,Rd}$</td> <td style="border: 1px solid black; padding: 2px;">0.00</td> <td>≤ 1 VERIFICATO</td> </tr> <tr> <td>M_{Ed} / M_{Rd}</td> <td style="border: 1px solid black; padding: 2px;">0.00</td> <td>≤ 1 VERIFICATO</td> </tr> <tr> <td>τ / f_{bd}</td> <td style="border: 1px solid black; padding: 2px;">0.00</td> <td>≤ 1 VERIFICATO</td> </tr> </table>	$q = F_{L,Ed} / A_{CO,pb} \cdot 1\text{mm}$	0.00	N/mm	$L = (L_{pb} - d)/2$	48.00	mm	$M = qL^2/2$	0	Nmm	$W = 1s_{pb}^2/6$	66.67	mm ²	$M_{Rd} = W \cdot f_{yd}$	22540	Nmm	$\tau = F_{L,Ed} / (4L_{pb} \cdot L)$	0.00	N/mm ²	$F_{L,Ed} / F_{L,pb,Rd}$	0.00	≤ 1 VERIFICATO	M_{Ed} / M_{Rd}	0.00	≤ 1 VERIFICATO	τ / f_{bd}	0.00	≤ 1 VERIFICATO
$f_{ck} =$	25	N/mm ²																																																																																																													
$L_0 = L - s =$	450	mm																																																																																																													
$\eta = 1$ se $d \leq 32\text{mm}$	1	-																																																																																																													
$\eta = (132-d)/100$ se $d > 32\text{mm}$																																																																																																															
$\gamma_c =$	1.5	-																																																																																																													
$f_{bd} = \eta \cdot 0.7 \cdot (0.3 \cdot f_{ck}^{2/3}) \cdot \gamma_c$	1.2	N/mm ²																																																																																																													
$F_{L,bond,Rd} = \pi \cdot d \cdot L_b \cdot f_{bd}$	41	kN																																																																																																													
$A_{CO,pb} = L_{pb} \cdot d$	14400	mm ²																																																																																																													
$f_{cd} =$	14.17	N/mm ²																																																																																																													
$F_{L,pb,Rd} = (A_{CO,pb} - \pi \cdot d^2/4) \cdot f_{cd}$	198	kN																																																																																																													
$F_{L,Rd} = 0.9 \cdot A_{res} \cdot f_{td} / \gamma_{M2}$	203	kN																																																																																																													
$F_{V,Rd} = 0.6 \cdot A \cdot f_{td} / \gamma_{M2}$	174	kN																																																																																																													
$k = \min(2.8e_2/d_0 - 1.7; 2.5)$	2.5	-																																																																																																													
$k = \min(1.4p_2/d_0 - 1.7; 2.5)$	2.5	-																																																																																																													
$\alpha = \min(e_1/3d_0; f_{td}/f_t; 1)$	1.0	-																																																																																																													
$\alpha = \min(p_1/3d_0 - 0.25; f_{td}/f_t; 1)$	1.0	-																																																																																																													
$F_{D,Rd} = k \cdot \alpha \cdot f_{tk} \cdot d \cdot t_p / \gamma_{M2}$	734	kN																																																																																																													
$F_{D,Rd} = k \cdot \alpha \cdot f_{tk} \cdot d \cdot t_p / \gamma_{M2}$	734	kN																																																																																																													
$B_{p,Rd} = 0.6 \cdot \pi \cdot f_{tk} \cdot d_{si} \cdot t_p / \gamma_{M2}$	831	kN																																																																																																													
$F_{L,anchor,Rd} = \min(F_{L,Rd}; B_{D,Rd}; F_{L,bond,Rd})$	41	kN																																																																																																													
$F_{L,anchor,Rd} = \min(F_{L,Rd}; B_{D,Rd}; F_{L,pb,Rd})$	198	kN																																																																																																													
$F_{V,anchor,Rd} = \min(F_{V,Rd}; F_{D,Rd})$	174	kN																																																																																																													
$n_b =$	4																																																																																																														
$F_{L,Ed} = \sigma_c \cdot A_{res}$	0	kN																																																																																																													
$F_{V,Ed} = V_{Ed} / n_b$	50	kN																																																																																																													
$F_{V,Ed} / F_{V,anchor,Rd} + F_{L,Ed} / 1.4 \cdot F_{L,anchor,Rd}$	0.29	≤ 1 VERIFICATO																																																																																																													
$F_{L,Ed} / F_{L,anchor,Rd}$	0.00	≤ 1 VERIFICATO																																																																																																													
<p>Carico sulla piastra annegata (schema a mensola)</p> <p>Luce mensola</p> <p>Momento sezione di incastro</p> <p>Momento d'inerzia</p> <p>Momento resistente</p> <p>Tensione tangenziale sulla sup. laterale del cilindro cls</p> <p>VERIFICA A COMPRESIONE CLS SOPRA LA PIASTRA ANNEGATA</p> <p>VERIFICA DI RESISTENZA PIASTRA ANNEGATA</p> <p>VERIFICA A SFILAMENTO DEL CILINDRO DI CALCESTRUZZO</p>	<table border="0" style="width: 100%;"> <tr> <td>$q = F_{L,Ed} / A_{CO,pb} \cdot 1\text{mm}$</td> <td style="border: 1px solid black; padding: 2px;">0.00</td> <td>N/mm</td> </tr> <tr> <td>$L = (L_{pb} - d)/2$</td> <td style="border: 1px solid black; padding: 2px;">48.00</td> <td>mm</td> </tr> <tr> <td>$M = qL^2/2$</td> <td style="border: 1px solid black; padding: 2px;">0</td> <td>Nmm</td> </tr> <tr> <td>$W = 1s_{pb}^2/6$</td> <td style="border: 1px solid black; padding: 2px;">66.67</td> <td>mm²</td> </tr> <tr> <td>$M_{Rd} = W \cdot f_{yd}$</td> <td style="border: 1px solid black; padding: 2px;">22540</td> <td>Nmm</td> </tr> <tr> <td>$\tau = F_{L,Ed} / (4L_{pb} \cdot L)$</td> <td style="border: 1px solid black; padding: 2px;">0.00</td> <td>N/mm²</td> </tr> <tr> <td>$F_{L,Ed} / F_{L,pb,Rd}$</td> <td style="border: 1px solid black; padding: 2px;">0.00</td> <td>≤ 1 VERIFICATO</td> </tr> <tr> <td>M_{Ed} / M_{Rd}</td> <td style="border: 1px solid black; padding: 2px;">0.00</td> <td>≤ 1 VERIFICATO</td> </tr> <tr> <td>τ / f_{bd}</td> <td style="border: 1px solid black; padding: 2px;">0.00</td> <td>≤ 1 VERIFICATO</td> </tr> </table>	$q = F_{L,Ed} / A_{CO,pb} \cdot 1\text{mm}$	0.00	N/mm	$L = (L_{pb} - d)/2$	48.00	mm	$M = qL^2/2$	0	Nmm	$W = 1s_{pb}^2/6$	66.67	mm ²	$M_{Rd} = W \cdot f_{yd}$	22540	Nmm	$\tau = F_{L,Ed} / (4L_{pb} \cdot L)$	0.00	N/mm ²	$F_{L,Ed} / F_{L,pb,Rd}$	0.00	≤ 1 VERIFICATO	M_{Ed} / M_{Rd}	0.00	≤ 1 VERIFICATO	τ / f_{bd}	0.00	≤ 1 VERIFICATO																																																																																			
$q = F_{L,Ed} / A_{CO,pb} \cdot 1\text{mm}$	0.00	N/mm																																																																																																													
$L = (L_{pb} - d)/2$	48.00	mm																																																																																																													
$M = qL^2/2$	0	Nmm																																																																																																													
$W = 1s_{pb}^2/6$	66.67	mm ²																																																																																																													
$M_{Rd} = W \cdot f_{yd}$	22540	Nmm																																																																																																													
$\tau = F_{L,Ed} / (4L_{pb} \cdot L)$	0.00	N/mm ²																																																																																																													
$F_{L,Ed} / F_{L,pb,Rd}$	0.00	≤ 1 VERIFICATO																																																																																																													
M_{Ed} / M_{Rd}	0.00	≤ 1 VERIFICATO																																																																																																													
τ / f_{bd}	0.00	≤ 1 VERIFICATO																																																																																																													

VERIFICA PARAPETTO

Per la verifica del parapetto si considera, in base al paragrafo 5.1.3.10 delle NTC 2018, un'azione orizzontale di 1,50 kN/m applicata alla quota del corrimano. L'altezza totale dei montanti principali del parapetto rispetto alla loro sezione di base è pari a 1,50 m, mentre l'interasse massimo è pari a 1.90 m. Quindi lo schema statico è quello di trave incastrata sottoposta a una forza ortogonale concentrata all'estremità libera.

Il montante di parapetto è costituito da doppio piatto in acciaio S355 di sezione 15x90, collegati ad un piatto di spessore pari a 25 mm mediante due bulloni M20 Classe 8.8.

Si riporta la verifica del parapetto e del giunto:

VERIFICA PARAPETTO

ANALISI DEI CARICHI

Spinta orizzontale sul parapetto Q	2.00 kN/m		
Interasse montanti i	0.95 m		
Forza orizzontale concentrata sul singolo montante P=Qxi	1.90 kN	γ_Q	1.5

CARATTERISTICHE DEL PROFILO

Tipo di acciaio	S355
Tensione di snervamento f_{yk}	355 N/mm ²
Tensione di rottura f_{tk}	510 N/mm ²
Modulo elastico E	210000 N/mm ²
Tipo di profilo	Piatto 15x90
Luce del montante L	1.60 m
Ipotesi schema di calcolo	Mensola
Area resistente a taglio A_v	1350 mm ²
Modulo resistente W	20.25 cm ³
Momento d'inerzia J	91.12 cm ⁴

VERIFICA DI RESISTENZA

Coefficiente di sicurezza γ_{M0} (tab. 4,2,V)	1.05		
Momento sollecitante M_{Ed}	$\gamma_Q PL = 4.56$ kNm	Taglio sollecitante V_{Ed}	$\gamma_Q P = 2.85$ kN
Momento resistente M_{c,Rd}	$W \cdot f_{yk} / g_{M0} = 6.85$ kNm	Taglio resistente V_{c,Rd}	$A_v \cdot f_{yk} / (30,5 \cdot g_{M0}) = #####$ kN
Coefficiente di sicurezza c_M	0.7	Coefficiente di sicurezza c_v	0.0

VERIFICATO

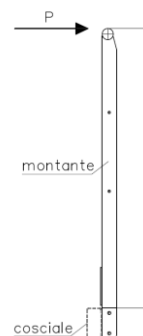
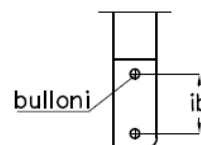
VERIFICATO

VERIFICA agli STATI LIMITE di ESERCIZIO

Freccia dovuta alla spinta sul parapetto	$(PL^3/3)/EJ = 14$ mm	
Limite superiore freccia	30 mm	
	0.45 < 1	VERIFICATO

VERIFICA COLLEGAMENTO bullonato

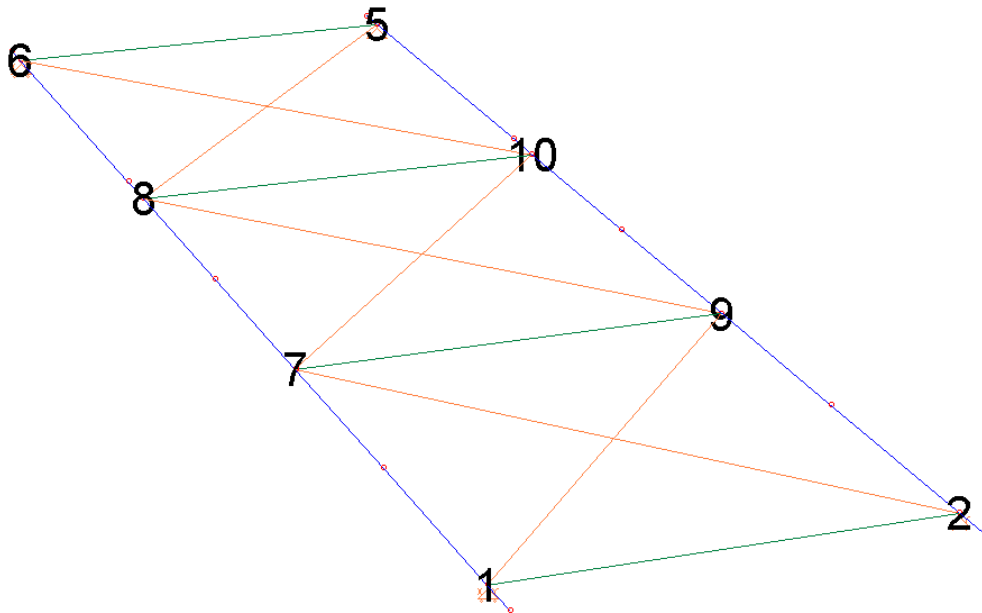
Spessore della piastra di collegamento	$t_p =$	12.5 mm
Bulloni		M20
Interasse bulloni	$i_b =$	120 mm
Numero bulloni	$n^{\circ}_b =$	1
Numero sezioni di taglio	$n^{\circ}_{st} =$	1
Classe		8.8
Diametro nominale del gambo del bullone	$d =$	20 mm
Diametro nominale del foro di alloggiamento del bullone	$d_o =$	22 mm
Area resistente della vite	$A_{res} =$	245 mm ²
Tensione di snervamento del materiale del bullone	$f_{yb} =$	640 N/mm ²
Tensione di rottura del materiale del bullone	$f_{tb} =$	800 N/mm ²



Tensione di rottura del materiale del piatto	f_{tk}	=	355	N/mm ²	
Coefficienti di sicurezza (Tab. 4.2.XII- NTC 2008)	γ_{M2}	=	1.25		
Resistenza di calcolo a taglio dei bulloni per piano di taglio	$F_{v,Rd}$	=	$0.6 f_{tb} A_{res} / \gamma_{M2} =$		94.08 kN
Resistenza di calcolo a rifollamento	$F_{b,Rd}$	=	$2.5 f_{tk} d t / \gamma_{M2} =$		177.50 kN
Resistenza complessiva della singola unione a taglio	$F_{v,Rd}$	=	$\min(F_{v,Rd}; F_{b,Rd}) =$		94.08 kN
Sollecitazione di taglio agente sul singolo bullone	$F_{v,Ed}$	=	$M_{Ed} / i_b / n^{\circ}_b / n^{\circ}_{st} =$		38.0 kN
	$F_{v,Ed} / F_{v,Rd}$	=	0.40	<	1 Verificato

Analogamente sono state calcolate le parti di minore importanza, le cui verifiche, per brevità di esposizione, vengono qui omesse.

Azioni agli appoggi



Si riportano le azioni trasmesse agli appoggi per le varie combinazioni di carico (forze in kg e momenti in kgm).

PROSPETTO DI STAMPA DELLE REAZIONI VINCOLARI

Nome progetto: Struttura R01
 Tipo analisi: dinamica
 Normativa: NTC 2018
 Numero frequenze: 30
 Sisma verticale: S1
 Modo in direzione X: 3
 Modo in direzione Y: 4
 Modo in direzione Z: 1
 λ : 0.3
 μ : 0.3
 Unità di misura delle forze: kg
 Unità di misura delle lunghezze: m

Stampa delle reazioni vincolari

Nodo	Comb	Descrizione	Azione sismica	FX	FY	FZ	MX	MY	MZ
1	1	Dinamica	EX + 0.3 EY + 0.3 EZ	0	0	13372.5	0	0	0
1	1	Dinamica	EX + 0.3 EY - 0.3 EZ	0	0	12907.5	0	0	0
1	1	Dinamica	EX - 0.3 EY + 0.3 EZ	0	0	13372.5	0	0	0
1	1	Dinamica	EX - 0.3 EY - 0.3 EZ	0	0	12907.5	0	0	0
1	1	Dinamica	-EX + 0.3 EY + 0.3 EZ	0	0	13372.5	0	0	0
1	1	Dinamica	-EX + 0.3 EY - 0.3 EZ	0	0	12907.5	0	0	0
1	1	Dinamica	-EX - 0.3 EY + 0.3 EZ	0	0	13372.5	0	0	0
1	1	Dinamica	-EX - 0.3 EY - 0.3 EZ	-0	-0	12907.5	-0	-0	-0
1	1	Dinamica	0.3 EX + EY + 0.3 EZ	0	0	13372.5	0	0	0
1	1	Dinamica	0.3 EX + EY - 0.3 EZ	0	0	12907.5	0	0	0
1	1	Dinamica	-0.3 EX + EY + 0.3 EZ	0	0	13372.5	0	0	0
1	1	Dinamica	-0.3 EX + EY - 0.3 EZ	0	0	12907.5	0	0	0
1	1	Dinamica	0.3 EX - EY + 0.3 EZ	0	0	13372.5	0	0	0
1	1	Dinamica	0.3 EX - EY - 0.3 EZ	0	0	12907.5	0	0	0
1	1	Dinamica	-0.3 EX - EY + 0.3 EZ	0	0	13372.5	0	0	0
1	1	Dinamica	-0.3 EX - EY - 0.3 EZ	-0	-0	12907.5	-0	-0	-0
1	1	Dinamica	0.3 EX + 0.3 EY + EZ	0	0	13915	0	0	0
1	1	Dinamica	0.3 EX - 0.3 EY + EZ	0	0	13915	0	0	0
1	1	Dinamica	-0.3 EX + 0.3 EY + EZ	0	0	13915	0	0	0
1	1	Dinamica	-0.3 EX - 0.3 EY + EZ	0	0	13915	0	0	0
1	1	Dinamica	0.3 EX + 0.3 EY - EZ	0	0	12365	0	0	0
1	1	Dinamica	0.3 EX - 0.3 EY - EZ	0	0	12365	0	0	0
1	1	Dinamica	-0.3 EX + 0.3 EY - EZ	0	0	12365	0	0	0
1	1	Dinamica	-0.3 EX - 0.3 EY - EZ	-0	-0	12365	-0	-0	-0
1	2	SLU1 - Statica solo Vento	--	-0	-0	13140	-0	-0	-0
1	3	SLU2 - Statica Neve dom	--	-0	-0	21650	-0	-0	-0
1	4	SLU3 - Statica Acc dom	--	-0	-0	30840	-0	-0	-0
1	5	SLU4 - Statica Vento dom	--	-0	-0	23950	-0	-0	-0
1	7	SLU5 - Statica soccorso POS.1	--	-0	-0	21650	-0	-0	-0
1	8	SLE1 - Rara Vento dom	--	-0	-0	16210	-0	-0	-0
1	9	SLE2 - Rara Solo Vento	--	-0	-0	13140	-0	-0	-0
1	10	SLE3 - Rara Acc dom	--	-0	-0	20800	-0	-0	-0
1	11	SLE4 - Neve dom	--	-0	-0	14680	-0	-0	-0
1	12	SLE 5 - Soccorso POS.1	--	-0	-0	14670	-0	-0	-0
1	13	Cond.1 - Solo P.P. Struttura	--	-0	-0	1812	-0	-0	-0
1	14	Cond.2 - Solo P.P. Solaio Predalles - G1	--	-0	-0	5667	-0	-0	-0
1	15	Cond.3 - Solo Portati - G2	--	-0	-0	5667	-0	-0	-0
1	16	Cond.4 - Solo Variabile Neve	--	-0	-0	1532	-0	-0	-0
1	17	Cond.5 - Solo Variabile Vento	--	-0	-0	8.02e-05	-0	-0	-0
1	18	Cond.6 - Solo Variabile Folla	--	-0	-0	7658	-0	-0	-0
1	19	Cond.7 - Solo Variabile Soccorso POS.1	--	-0	-0	1526	-0	-0	-0
1	20	SLU 6 - Soccorso Pos.2	--	-0	-0	24480	-0	-0	-0
1	21	SLE 6 - Soccorso POS:2	--	-0	-0	16560	-0	-0	-0
1	22	Cond.8 - Solo Variabile Soccorso POS.2	--	-0	-0	3418	-0	-0	-0
1	23	Inviluppo (pos)	--	-0	-0	30840	-0	-0	-0
1	24	Inviluppo (neg)	--	-0	-0	0	-0	-0	-0
1	25	Inviluppo	--	-0	-0	30840	-0	-0	-0
2	1	Dinamica	EX + 0.3 EY + 0.3 EZ	11430	0	13372.5	0	0	0
2	1	Dinamica	EX + 0.3 EY - 0.3 EZ	11430	0	12907.5	0	0	0
2	1	Dinamica	EX - 0.3 EY + 0.3 EZ	13770	0	13372.5	0	0	0
2	1	Dinamica	EX - 0.3 EY - 0.3 EZ	13770	0	12907.5	0	0	0
2	1	Dinamica	-EX + 0.3 EY + 0.3 EZ	-13770	0	13372.5	0	0	0
2	1	Dinamica	-EX + 0.3 EY - 0.3 EZ	-13770	0	12907.5	0	0	0
2	1	Dinamica	-EX - 0.3 EY + 0.3 EZ	-11430	0	13372.5	0	0	0
2	1	Dinamica	-EX - 0.3 EY - 0.3 EZ	-11430	-0	12907.5	-0	-0	-0
2	1	Dinamica	0.3 EX + EY + 0.3 EZ	-120	0	13372.5	0	0	0
2	1	Dinamica	0.3 EX + EY - 0.3 EZ	-120	0	12907.5	0	0	0
2	1	Dinamica	-0.3 EX + EY + 0.3 EZ	-7680	0	13372.5	0	0	0
2	1	Dinamica	-0.3 EX + EY - 0.3 EZ	-7680	0	12907.5	0	0	0
2	1	Dinamica	0.3 EX - EY + 0.3 EZ	7680	0	13372.5	0	0	0
2	1	Dinamica	0.3 EX - EY - 0.3 EZ	7680	0	12907.5	0	0	0
2	1	Dinamica	-0.3 EX - EY + 0.3 EZ	120	0	13372.5	0	0	0
2	1	Dinamica	-0.3 EX - EY - 0.3 EZ	120	-0	12907.5	-0	-0	-0
2	1	Dinamica	0.3 EX + 0.3 EY + EZ	2610	0	13915	0	0	0
2	1	Dinamica	0.3 EX - 0.3 EY + EZ	4950	0	13915	0	0	0
2	1	Dinamica	-0.3 EX + 0.3 EY + EZ	-4950	0	13915	0	0	0

2	1	Dinamica	-0.3 EX - 0.3 EY + EZ	-2610	0	13915	0	0	0
2	1	Dinamica	0.3 EX + 0.3 EY - EZ	2610	0	12365	0	0	0
2	1	Dinamica	0.3 EX - 0.3 EY - EZ	4950	0	12365	0	0	0
2	1	Dinamica	-0.3 EX + 0.3 EY - EZ	-4950	0	12365	0	0	0
2	1	Dinamica	-0.3 EX - 0.3 EY - EZ	-2610	-0	12365	-0	-0	-0
2	2	SLU1 - Statica solo Vento --		-3110	-0	13140	-0	-0	-0
2	3	SLU2 - Statica Neve dom --		-1866	-0	21650	-0	-0	-0
2	4	SLU3 - Statica Acc dom --		-1866	-0	30840	-0	-0	-0
2	5	SLU4 - Statica Vento dom --		-3110	-0	23950	-0	-0	-0
2	7	SLU5 - Statica soccorso POS.1 --		844.9	-0	24840	-0	-0	-0
2	8	SLE1 - Rara Vento dom --		-2074	-0	16210	-0	-0	-0
2	9	SLE2 - Rara Solo Vento --		-2074	-0	13140	-0	-0	-0
2	10	SLE3 - Rara Acc dom --		-1244	-0	20800	-0	-0	-0
2	11	SLE4 - Neve dom --		-1244	-0	14680	-0	-0	-0
2	12	SLE 5 - Soccorso POS.1 --		563.3	-0	16800	-0	-0	-0
2	13	Cond.1 - Solo P.P. Struttura --		-5.919e-06	-0	1812	-0	-0	-0
2	14	Cond.2 - Solo P.P. Solaio Predalles - G1 --		-2.21e-05	-0	5667	-0	-0	-0
2	15	Cond.3 - Solo Portati - G2 --		-2.21e-05	-0	5667	-0	-0	-0
2	16	Cond.4 - Solo Variabile Neve --		-5.973e-06	-0	1532	-0	-0	-0
2	17	Cond.5 - Solo Variabile Vento --		-2074	-0	-8.02e-05	-0	-0	-0
2	18	Cond.6 - Solo Variabile Folla --		-2.987e-05	-0	7658	-0	-0	-0
2	19	Cond.7 - Solo Variabile Soccorso POS.1 --		-563.3	-0	3657	-0	-0	-0
2	20	SLU 6 - Soccorso Pos.2 --		844.9	-0	31620	-0	-0	-0
2	21	SLE 6 - Soccorso POS:2 --		563.3	-0	21320	-0	-0	-0
2	22	Cond.8 - Solo Variabile Soccorso POS.2 --		-563.3	-0	8174	-0	-0	-0
2	23	Inviluppo (pos)	--	13770	-0	31620	-0	-0	-0
2	24	Inviluppo (neg)	--	-13770	-0	-8.02e-05	-0	-0	-0
2	25	Inviluppo	--	-13770	-0	31620	-0	-0	-0
5	1	Dinamica	EX + 0.3 EY + 0.3 EZ	12948	4519	13098.1	0	0	0
5	1	Dinamica	EX + 0.3 EY - 0.3 EZ	12948	4519	12661.9	0	0	0
5	1	Dinamica	EX - 0.3 EY + 0.3 EZ	10452	-5741	13098.1	0	0	0
5	1	Dinamica	EX - 0.3 EY - 0.3 EZ	10452	-5741	12661.9	0	0	0
5	1	Dinamica	-EX + 0.3 EY + 0.3 EZ	-10452	5741	13098.1	0	0	0
5	1	Dinamica	-EX + 0.3 EY - 0.3 EZ	-10452	5741	12661.9	0	0	0
5	1	Dinamica	-EX - 0.3 EY + 0.3 EZ	-12948	-4519	13098.1	0	0	0
5	1	Dinamica	-EX - 0.3 EY - 0.3 EZ	-12948	-4519	12661.9	-0	-0	-0
5	1	Dinamica	0.3 EX + EY + 0.3 EZ	7670	16916.7	13098.1	0	0	0
5	1	Dinamica	0.3 EX + EY - 0.3 EZ	7670	16916.7	12661.9	0	0	0
5	1	Dinamica	-0.3 EX + EY + 0.3 EZ	650	17283.3	13098.1	0	0	0
5	1	Dinamica	-0.3 EX + EY - 0.3 EZ	650	17283.3	12661.9	0	0	0
5	1	Dinamica	0.3 EX - EY + 0.3 EZ	-650	-17283.3	13098.1	0	0	0
5	1	Dinamica	0.3 EX - EY - 0.3 EZ	-650	-17283.3	12661.9	0	0	0
5	1	Dinamica	-0.3 EX - EY + 0.3 EZ	-7670	-16916.7	13098.1	0	0	0
5	1	Dinamica	-0.3 EX - EY - 0.3 EZ	-7670	-16916.7	12661.9	-0	-0	-0
5	1	Dinamica	0.3 EX + 0.3 EY + EZ	4758	4946.7	13607	0	0	0
5	1	Dinamica	0.3 EX - 0.3 EY + EZ	2262	-5313.3	13607	0	0	0
5	1	Dinamica	-0.3 EX + 0.3 EY + EZ	-2262	5313.3	13607	0	0	0
5	1	Dinamica	-0.3 EX - 0.3 EY + EZ	-4758	-4946.7	13607	0	0	0
5	1	Dinamica	0.3 EX + 0.3 EY - EZ	4758	4946.7	12153	0	0	0
5	1	Dinamica	0.3 EX - 0.3 EY - EZ	2262	-5313.3	12153	0	0	0
5	1	Dinamica	-0.3 EX + 0.3 EY - EZ	-2262	5313.3	12153	0	0	0
5	1	Dinamica	-0.3 EX - 0.3 EY - EZ	-4758	-4946.7	12153	-0	-0	-0
5	2	SLU1 - Statica solo Vento --		-3048	-4.32e-06	12880	-0	-0	-0
5	3	SLU2 - Statica Neve dom --		-1828	-5.616e-06	21220	-0	-0	-0
5	4	SLU3 - Statica Acc dom --		-1828	-5.616e-06	30220	-0	-0	-0
5	5	SLU4 - Statica Vento dom --		-3048	-5.616e-06	23470	-0	-0	-0
5	7	SLU5 - Statica soccorso POS.1 --		-844.9	-10800	26180	-0	-0	-0
5	8	SLE1 - Rara Vento dom --		-2032	-4.32e-06	15880	-0	-0	-0
5	9	SLE2 - Rara Solo Vento --		-2032	-4.32e-06	12880	-0	-0	-0
5	10	SLE3 - Rara Acc dom --		-1219	-4.32e-06	20390	-0	-0	-0
5	11	SLE4 - Neve dom --		-1219	-4.32e-06	14380	-0	-0	-0
5	12	SLE 5 - Soccorso POS.1 --		-563.3	-7200	17690	-0	-0	-0
5	13	Cond.1 - Solo P.P. Struttura --		-6.934e-06	-4.32e-06	1778	-0	-0	-0
5	14	Cond.2 - Solo P.P. Solaio Predalles - G1 --		-2.165e-05	-3.341e-20	5552	-0	-0	-0
5	15	Cond.3 - Solo Portati - G2 --		-2.165e-05	-3.341e-20	5552	-0	-0	-0
5	16	Cond.4 - Solo Variabile Neve --		-5.853e-06	-8.733e-21	1501	-0	-0	-0
5	17	Cond.5 - Solo Variabile Vento --		-2032	1.589e-12	-4.022e-05	-0	-0	-0
5	18	Cond.6 - Solo Variabile Folla --		-2.926e-05	-4.894e-20	7503	-0	-0	-0
5	19	Cond.7 - Solo Variabile Soccorso POS.1 --		563.3	7200	4804	-0	-0	-0
5	20	SLU 6 - Soccorso Pos.2 --		-844.9	-10800	19400	-0	-0	-0
5	21	SLE 6 - Soccorso POS:2 --		-563.3	-7200	13170	-0	-0	-0
5	22	Cond.8 - Solo Variabile Soccorso POS.2 --		563.3	7200	287.6	-0	-0	-0
5	23	Inviluppo (pos)	--	12948	17283.3	30220	-0	-0	-0
5	24	Inviluppo (neg)	--	-12948	-17283.3	-4.022e-05	-0	-0	-0
5	25	Inviluppo	--	-12948	-17283.3	30220	-0	-0	-0
6	1	Dinamica	EX + 0.3 EY + 0.3 EZ	0	0	13098.1	0	0	0
6	1	Dinamica	EX + 0.3 EY - 0.3 EZ	0	0	12661.9	0	0	0
6	1	Dinamica	EX - 0.3 EY + 0.3 EZ	0	0	13098.1	0	0	0
6	1	Dinamica	EX - 0.3 EY - 0.3 EZ	0	0	12661.9	0	0	0
6	1	Dinamica	-EX + 0.3 EY + 0.3 EZ	0	0	13098.1	0	0	0
6	1	Dinamica	-EX + 0.3 EY - 0.3 EZ	0	0	12661.9	0	0	0
6	1	Dinamica	-EX - 0.3 EY + 0.3 EZ	0	0	13098.1	0	0	0
6	1	Dinamica	-EX - 0.3 EY - 0.3 EZ	-0	-0	12661.9	-0	-0	-0
6	1	Dinamica	0.3 EX + EY + 0.3 EZ	0	0	13098.1	0	0	0
6	1	Dinamica	0.3 EX + EY - 0.3 EZ	0	0	12661.9	0	0	0
6	1	Dinamica	-0.3 EX + EY + 0.3 EZ	0	0	13098.1	0	0	0
6	1	Dinamica	-0.3 EX + EY - 0.3 EZ	0	0	12661.9	0	0	0
6	1	Dinamica	0.3 EX - EY + 0.3 EZ	0	0	13098.1	0	0	0
6	1	Dinamica	0.3 EX - EY - 0.3 EZ	0	0	12661.9	0	0	0
6	1	Dinamica	-0.3 EX - EY + 0.3 EZ	0	0	13098.1	0	0	0
6	1	Dinamica	-0.3 EX - EY - 0.3 EZ	-0	-0	12661.9	-0	-0	-0
6	1	Dinamica	0.3 EX + 0.3 EY + EZ	0	0	13607	0	0	0
6	1	Dinamica	0.3 EX - 0.3 EY + EZ	0	0	13607	0	0	0
6	1	Dinamica	-0.3 EX + 0.3 EY + EZ	0	0	13607	0	0	0
6	1	Dinamica	-0.3 EX - 0.3 EY + EZ	0	0	13607	0	0	0
6	1	Dinamica	0.3 EX + 0.3 EY - EZ	0	0	12153	0	0	0
6	1	Dinamica	0.3 EX - 0.3 EY - EZ	0	0	12153	0	0	0
6	1	Dinamica	-0.3 EX + 0.3 EY - EZ	0	0	12153	0	0	0

6	1	Dinamica	-0.3 EX - 0.3 EY - EZ	-0	-0	12153	-0	-0	-0
6	2	SLU1	- Statica solo Vento --	-0	-0	12880	-0	-0	-0
6	3	SLU2	- Statica Neve dom --	-0	-0	21220	-0	-0	-0
6	4	SLU3	- Statica Acc dom --	-0	-0	30220	-0	-0	-0
6	5	SLU4	- Statica Vento dom --	-0	-0	23470	-0	-0	-0
6	7	SLU5	- Statica soccorso POS.1 --	-0	-0	21990	-0	-0	-0
6	8	SLE1	- Rara Vento dom --	-0	-0	15880	-0	-0	-0
6	9	SLE2	- Rara Solo Vento --	-0	-0	12880	-0	-0	-0
6	10	SLE3	- Rara Acc dom --	-0	-0	20390	-0	-0	-0
6	11	SLE4	- Neve dom --	-0	-0	14380	-0	-0	-0
6	12	SLE 5	- Soccorso POS.1 --	-0	-0	14900	-0	-0	-0
6	13	Cond.1	- Solo P.P. Struttura --	-0	-0	1778	-0	-0	-0
6	14	Cond.2	- Solo P.P. Solaio Predalles - G1 --	-0	-0	5552	-0	-0	-0
6	15	Cond.3	- Solo Portati - G2 --	-0	-0	5552	-0	-0	-0
6	16	Cond.4	- Solo Variabile Neve --	-0	-0	1501	-0	-0	-0
6	17	Cond.5	- Solo Variabile Vento --	-0	-0	4.022e-05	-0	-0	-0
6	18	Cond.6	- Solo Variabile Folla --	-0	-0	7503	-0	-0	-0
6	19	Cond.7	- Solo Variabile Soccorso POS.1 --	-0	-0	2012	-0	-0	-0
6	20	SLU 6	- Soccorso Pos.2 --	-0	-0	19150	-0	-0	-0
6	21	SLE 6	- Soccorso POS:2 --	-0	-0	13000	-0	-0	-0
6	22	Cond.8	- Solo Variabile Soccorso POS.2 --	-0	-0	120.6	-0	-0	-0
6	23	Inviluppo	(pos) --	-0	-0	30220	-0	-0	-0
6	24	Inviluppo	(neg) --	-0	-0	0	-0	-0	-0
6	25	Inviluppo	--	-0	-0	30220	-0	-0	-0

Sommario

INTRODUZIONE AI MODELLI DI CALCOLO	2
<i>I NODI</i>	2
<i>I MATERIALI</i>	3
<i>LE SEZIONI</i>	3
<i>I CARICHI</i>	4
<i>GLI ELEMENTI FINITI</i>	4
<i>ELEMENTO TRUSS (ASTA RETICOLARE)</i>	4
<i>ELEMENTO FRAME (TRAVE E PILASTRO, TRAVE DI FONDAZIONE)</i>	5
<i>ELEMENTO SHELL (GUSCIO)</i>	6
<i>ELEMENTO PLANE</i>	7
<i>ELEMENTO BOUNDARY (VINCOLO)</i>	7
STAMPA DEI DATI DI PROGETTO	8
<i>INTESTAZIONE E DATI CARATTERISTICI DELLA STRUTTURA</i>	8
<i>CARICHI PER EL.TI TRAVE, TRAVE DI FONDAZIONE E RETICOLARE</i>	9
<i>LISTA MATERIALI UTILIZZATI</i>	9
<i>RIEPILOGO DELLE SEZ. UTILIZZATE NEL MODELLO STRUTTURALE</i>	9
<i>GRUPPI DELLA STRUTTURA</i>	10
<i>NODI DEL MODELLO</i>	10
<i>GRUPPI elemento finito TRAVE</i>	12
<i>GRUPPI ELEMENTO finito VINCOLO</i>	14
<i>COMBINAZIONI DI CARICO</i>	15
<i>REAZIONI VINCOLARI STATICA</i>	19
<i>TABELLA INVILUPPI REAZIONI VINCOLARI</i>	21
<i>TABELLA MASSE ECCITATE</i>	22

VERIFICHE DEGLI ELEMENTI STRUTTURALI.....	25
INTERPRETAZIONE DEI RISULTATI DELLE VERIFICHE	25
VERIFICHE DI OPERE IN ACCIAIO, CON IL METODO DEGLI S.LIMITE	25
VERIFICHE OPERE IN ACCIAIO CON L'EUROCODICE 3	28
RISULTATI DELLE VERIFICHE	30
VERIFICA ELEMENTI IN ACCIAIO	30
VERIFICA GIUNTO DIAGONALE DI CONTROVENTO	65
VERIFICA APPOGGIO ESTREMITÀ "A"	67
VERIFICA PARAPETTO	69
Azioni agli appoggi	71

A9 – FASCICOLO DEI CALCOLI OPERE IN CA

In conformità al paragrafo 10.2 del D.M. 17.01.2018 e relativa CIRCOLARE applicativa

21/12/2023

Progetto eseguito con l'ausilio del software di calcolo DOLMEN



TABULATI DI CALCOLO

INDICE

- 1 - DATI DELLA STRUTTURA
- 2 - VERIFICA PIASTRE E SETTI

1 - DATI DELLA STRUTTURA

Le tabelle seguenti contengono informazioni dettagliate relative al modello strutturale realizzato con DOLMEN (coordinate dei nodi, proprietà delle aste, materiali, vincoli, carichi).

Unita` di misura :
 LUNGHEZZE : cm
 SUPERFICI : cm2
 DATI SEZIONALI : cm
 ANGOLI : gradi
 FORZE : daN
 MOMENTI : daNcm
 CARICHI LINEARI : daN/cm
 CARICHI SUPERFIC.: daN/cm2
 TENSIONI : daN/cm2
 PESI DI VOLUME : daN/cm3
 COEFF. DI WINKLER: daN/cm3
 RIGIDENZE VINCOL.: daN/cm - daNcm/rad

NODI--	-----	-----	-----	-----	num.=
Nome	Coord. X	Coord. Y	Coord. Z		
1	1465.000	0.000	300.000		
2	1465.000	390.000	300.000		
5	5.000	390.000	300.000		
6	5.000	0.000	300.000		
100	1470.000	383.000	385.000		
101	1470.000	430.000	385.000		
102	1470.000	430.000	342.500		
103	1470.000	383.000	342.500		
104	1470.000	430.000	300.000		
105	1470.000	336.000	385.000		
106	1470.000	336.000	342.500		
107	1470.000	336.000	300.000		
108	1470.000	289.000	385.000		
109	1470.000	289.000	342.500		
110	1470.000	289.000	300.000		
111	1470.000	242.000	385.000		
112	1470.000	242.000	342.500		
113	1470.000	242.000	300.000		
114	1470.000	195.000	385.000		
115	1470.000	195.000	342.500		
116	1470.000	195.000	300.000		
117	1470.000	148.000	385.000		
118	1470.000	148.000	342.500		
119	1470.000	148.000	300.000		
120	1470.000	101.000	385.000		
121	1470.000	101.000	342.500		
122	1470.000	101.000	300.000		
123	1470.000	54.000	385.000		
124	1470.000	54.000	342.500		
125	1470.000	54.000	300.000		
126	1470.000	7.000	385.000		
127	1470.000	7.000	342.500		
128	1470.000	-40.000	385.000		
129	1470.000	-40.000	342.500		
130	1470.000	-40.000	300.000		
131	1470.000	-168.000	300.000		
132	1470.000	-136.000	321.300		
133	1470.000	-125.300	300.000		
134	1470.000	-104.000	342.500		
135	1470.000	-82.700	300.000		
136	1470.000	-72.000	363.800		
137	1470.000	-56.000	331.900		
138	1470.000	526.000	321.300		

139	1470.000	558.000	300.000
140	1470.000	515.300	300.000
141	1470.000	494.000	342.500
142	1470.000	472.700	300.000
143	1470.000	462.000	363.800
144	1470.000	446.000	331.900
145	1470.000	430.000	257.800
146	1470.000	472.600	257.800
147	1470.000	472.500	215.700
148	1470.000	430.000	215.700
149	1470.000	515.200	257.800
150	1470.000	515.000	215.700
151	1470.000	557.800	257.800
152	1470.000	557.500	215.700
153	1470.000	653.300	236.700
154	1470.000	685.000	215.700
155	1470.000	642.500	215.700
156	1470.000	621.500	257.800
157	1470.000	600.000	215.700
158	1470.000	589.800	278.900
159	1470.000	573.600	247.300
160	1470.000	685.000	175.400
161	1470.000	642.500	175.400
162	1470.000	685.000	135.200
163	1470.000	642.500	135.200
164	1470.000	685.000	95.000
165	1470.000	642.500	95.000
166	1470.000	600.000	175.400
167	1470.000	600.000	135.200
168	1470.000	600.000	95.000
169	1470.000	557.500	175.400
170	1470.000	557.500	135.200
171	1470.000	557.500	95.000
172	1470.000	515.000	175.400
173	1470.000	515.000	135.200
174	1470.000	515.000	95.000
175	1470.000	472.500	175.400
176	1470.000	472.500	135.200
177	1470.000	472.500	95.000
178	1470.000	430.000	175.400
179	1470.000	430.000	135.200
180	1470.000	430.000	95.000
181	1470.000	-82.600	257.800
182	1470.000	-40.000	257.800
183	1470.000	-40.000	215.700
184	1470.000	-82.500	215.700
185	1470.000	-125.200	257.800
186	1470.000	-125.000	215.700
187	1470.000	-167.800	257.800
188	1470.000	-167.500	215.700
189	1470.000	-295.000	215.700
190	1470.000	-263.300	236.700
191	1470.000	-252.500	215.700
192	1470.000	-231.500	257.800
193	1470.000	-210.000	215.700
194	1470.000	-199.800	278.900
195	1470.000	-183.600	247.300
196	1470.000	-40.000	175.400
197	1470.000	-82.500	175.400
198	1470.000	-40.000	135.200
199	1470.000	-82.500	135.200
200	1470.000	-40.000	95.000
201	1470.000	-82.500	95.000
202	1470.000	-125.000	175.400
203	1470.000	-125.000	135.200
204	1470.000	-125.000	95.000
205	1470.000	-167.500	175.400

206	1470.000	-167.500	135.200
207	1470.000	-167.500	95.000
208	1470.000	-210.000	175.400
209	1470.000	-210.000	135.200
210	1470.000	-210.000	95.000
211	1470.000	-252.500	175.400
212	1470.000	-252.500	135.200
213	1470.000	-252.500	95.000
214	1470.000	-295.000	175.400
215	1470.000	-295.000	135.200
216	1470.000	-295.000	95.000
217	1470.000	383.000	257.800
218	1470.000	383.000	215.700
219	1470.000	336.000	257.800
220	1470.000	336.000	215.700
221	1470.000	289.000	257.800
222	1470.000	289.000	215.700
223	1470.000	242.000	257.800
224	1470.000	242.000	215.700
225	1470.000	195.000	257.800
226	1470.000	195.000	215.700
227	1470.000	148.000	257.800
228	1470.000	148.000	215.700
229	1470.000	101.000	257.800
230	1470.000	101.000	215.700
231	1470.000	54.000	257.800
232	1470.000	54.000	215.700
233	1470.000	7.000	257.800
234	1470.000	7.000	215.700
235	1470.000	383.000	175.400
236	1470.000	383.000	135.200
237	1470.000	383.000	95.000
238	1470.000	336.000	175.400
239	1470.000	336.000	135.200
240	1470.000	336.000	95.000
241	1470.000	289.000	175.400
242	1470.000	289.000	135.200
243	1470.000	289.000	95.000
244	1470.000	242.000	175.400
245	1470.000	242.000	135.200
246	1470.000	242.000	95.000
247	1470.000	195.000	175.400
248	1470.000	195.000	135.200
249	1470.000	195.000	95.000
250	1470.000	148.000	175.400
251	1470.000	148.000	135.200
252	1470.000	148.000	95.000
253	1470.000	101.000	175.400
254	1470.000	101.000	135.200
255	1470.000	101.000	95.000
256	1470.000	54.000	175.400
257	1470.000	54.000	135.200
258	1470.000	54.000	95.000
259	1470.000	7.000	175.400
260	1470.000	7.000	135.200
261	1470.000	7.000	95.000
262	1470.000	430.000	47.500
263	1470.000	383.000	47.500
264	1470.000	430.000	0.000
265	1470.000	383.000	0.000
266	1470.000	336.000	47.500
267	1470.000	336.000	0.000
268	1470.000	289.000	47.500
269	1470.000	289.000	0.000
270	1470.000	242.000	47.500
271	1470.000	242.000	0.000
272	1470.000	195.000	47.500

273	1470.000	148.000	47.500
274	1470.000	148.000	0.000
275	1470.000	101.000	47.500
276	1470.000	101.000	0.000
277	1470.000	54.000	47.500
278	1470.000	54.000	0.000
279	1470.000	7.000	47.500
280	1470.000	7.000	0.000
281	1470.000	-40.000	47.500
282	1470.000	-40.000	0.000
283	1520.000	642.500	95.000
284	1520.000	685.000	95.000
285	1570.000	642.500	95.000
286	1570.000	685.000	95.000
287	1520.000	600.000	95.000
288	1570.000	600.000	95.000
289	1520.000	557.500	95.000
290	1570.000	557.500	95.000
291	1520.000	515.000	95.000
292	1570.000	515.000	95.000
293	1520.000	472.500	95.000
294	1570.000	472.500	95.000
295	1520.000	430.000	95.000
296	1570.000	430.000	95.000
297	1520.000	-82.500	95.000
298	1520.000	-40.000	95.000
299	1570.000	-82.500	95.000
300	1570.000	-40.000	95.000
301	1520.000	-125.000	95.000
302	1570.000	-125.000	95.000
303	1520.000	-167.500	95.000
304	1570.000	-167.500	95.000
305	1520.000	-210.000	95.000
306	1570.000	-210.000	95.000
307	1520.000	-252.500	95.000
308	1570.000	-252.500	95.000
309	1520.000	-295.000	95.000
310	1570.000	-295.000	95.000
311	1470.000	35.000	0.000
312	1470.000	195.000	0.000
313	1470.000	355.000	0.000
314	1470.000	0.000	300.000
316	1470.000	390.000	300.000
319	0.000	390.000	300.000
321	0.000	0.000	300.000
322	0.000	7.000	257.800
323	0.000	-40.000	257.800
324	0.000	-40.000	215.700
325	0.000	7.000	215.700
326	0.000	54.000	257.800
327	0.000	54.000	215.700
328	0.000	101.000	300.000
329	0.000	54.000	300.000
330	0.000	101.000	257.800
331	0.000	101.000	215.700
332	0.000	148.000	300.000
333	0.000	148.000	257.800
334	0.000	148.000	215.700
335	0.000	195.000	300.000
336	0.000	195.000	257.800
337	0.000	195.000	215.700
338	0.000	242.000	300.000
339	0.000	242.000	257.800
340	0.000	242.000	215.700
341	0.000	289.000	300.000
342	0.000	289.000	257.800
343	0.000	289.000	215.700

344	0.000	336.000	300.000
345	0.000	336.000	257.800
346	0.000	336.000	215.700
347	0.000	383.000	257.800
348	0.000	383.000	215.700
349	0.000	430.000	257.800
350	0.000	430.000	215.700
351	0.000	-40.000	175.400
352	0.000	7.000	175.400
353	0.000	-40.000	135.200
354	0.000	7.000	135.200
355	0.000	-40.000	95.000
356	0.000	7.000	95.000
357	0.000	54.000	175.400
358	0.000	54.000	135.200
359	0.000	54.000	95.000
360	0.000	101.000	175.400
361	0.000	101.000	135.200
362	0.000	101.000	95.000
363	0.000	148.000	175.400
364	0.000	148.000	135.200
365	0.000	148.000	95.000
366	0.000	195.000	175.400
367	0.000	195.000	135.200
368	0.000	195.000	95.000
369	0.000	242.000	175.400
370	0.000	242.000	135.200
371	0.000	242.000	95.000
372	0.000	289.000	175.400
373	0.000	289.000	135.200
374	0.000	289.000	95.000
375	0.000	336.000	175.400
376	0.000	336.000	135.200
377	0.000	336.000	95.000
378	0.000	383.000	175.400
379	0.000	383.000	135.200
380	0.000	383.000	95.000
381	0.000	430.000	175.400
382	0.000	430.000	135.200
383	0.000	430.000	95.000
384	0.000	-40.000	47.500
385	0.000	7.000	47.500
386	0.000	-40.000	0.000
387	0.000	7.000	0.000
388	0.000	54.000	47.500
389	0.000	101.000	47.500
390	0.000	54.000	0.000
391	0.000	101.000	0.000
392	0.000	148.000	47.500
393	0.000	148.000	0.000
394	0.000	195.000	47.500
395	0.000	195.000	0.000
396	0.000	242.000	47.500
397	0.000	242.000	0.000
398	0.000	289.000	47.500
399	0.000	289.000	0.000
400	0.000	336.000	47.500
401	0.000	336.000	0.000
402	0.000	383.000	47.500
403	0.000	430.000	47.500
404	0.000	383.000	0.000
405	0.000	430.000	0.000
406	0.000	-252.500	95.000
407	-50.000	-252.500	95.000
408	-50.000	-295.000	95.000
409	0.000	-295.000	95.000
410	-100.000	-252.500	95.000

411	-100.000	-295.000	95.000
412	0.000	-210.000	95.000
413	-50.000	-210.000	95.000
414	-100.000	-210.000	95.000
415	0.000	-167.500	95.000
416	-50.000	-167.500	95.000
417	-100.000	-167.500	95.000
418	0.000	-125.000	95.000
419	-50.000	-125.000	95.000
420	-100.000	-125.000	95.000
421	0.000	-82.500	95.000
422	-50.000	-82.500	95.000
423	-100.000	-82.500	95.000
424	-50.000	-40.000	95.000
425	-100.000	-40.000	95.000
426	0.000	472.500	95.000
427	-50.000	472.500	95.000
428	-50.000	430.000	95.000
429	-100.000	472.500	95.000
430	-100.000	430.000	95.000
431	0.000	515.000	95.000
432	-50.000	515.000	95.000
433	-100.000	515.000	95.000
434	0.000	557.500	95.000
435	-50.000	557.500	95.000
436	-100.000	557.500	95.000
437	0.000	600.000	95.000
438	-50.000	600.000	95.000
439	-100.000	600.000	95.000
440	0.000	642.500	95.000
441	-50.000	642.500	95.000
442	-100.000	642.500	95.000
443	0.000	685.000	95.000
444	-50.000	685.000	95.000
445	-100.000	685.000	95.000
446	0.000	355.000	0.000
447	0.000	35.000	0.000
448	0.000	-40.000	300.000
449	0.000	430.000	300.000
450	0.000	7.000	385.000
451	0.000	-40.000	385.000
452	0.000	-40.000	342.500
453	0.000	7.000	342.500
454	0.000	54.000	385.000
455	0.000	54.000	342.500
456	0.000	101.000	385.000
457	0.000	101.000	342.500
458	0.000	148.000	385.000
459	0.000	148.000	342.500
460	0.000	195.000	385.000
461	0.000	195.000	342.500
462	0.000	242.000	385.000
463	0.000	242.000	342.500
464	0.000	289.000	385.000
465	0.000	289.000	342.500
466	0.000	336.000	385.000
467	0.000	336.000	342.500
468	0.000	383.000	385.000
469	0.000	383.000	342.500
470	0.000	430.000	385.000
471	0.000	430.000	342.500
472	0.000	558.000	300.000
473	0.000	526.000	321.300
474	0.000	515.300	300.000
475	0.000	494.000	342.500
476	0.000	472.700	300.000
477	0.000	462.000	363.800

478	0.000	446.000	331.900
479	0.000	-136.000	321.300
480	0.000	-168.000	300.000
481	0.000	-125.300	300.000
482	0.000	-104.000	342.500
483	0.000	-82.700	300.000
484	0.000	-72.000	363.800
485	0.000	-56.000	331.900
486	0.000	472.600	257.800
487	0.000	472.500	215.700
488	0.000	515.200	257.800
489	0.000	515.000	215.700
490	0.000	557.800	257.800
491	0.000	557.500	215.700
492	0.000	685.000	215.700
493	0.000	653.300	236.700
494	0.000	642.500	215.700
495	0.000	621.500	257.800
496	0.000	600.000	215.700
497	0.000	589.800	278.900
498	0.000	573.600	247.300
499	0.000	472.500	175.400
500	0.000	472.500	135.200
501	0.000	515.000	175.400
502	0.000	515.000	135.200
503	0.000	557.500	175.400
504	0.000	557.500	135.200
505	0.000	600.000	175.400
506	0.000	600.000	135.200
507	0.000	642.500	175.400
508	0.000	642.500	135.200
509	0.000	685.000	175.400
510	0.000	685.000	135.200
511	0.000	-82.600	257.800
512	0.000	-82.500	215.700
513	0.000	-125.200	257.800
514	0.000	-125.000	215.700
515	0.000	-167.800	257.800
516	0.000	-167.500	215.700
517	0.000	-263.300	236.700
518	0.000	-295.000	215.700
519	0.000	-252.500	215.700
520	0.000	-231.500	257.800
521	0.000	-210.000	215.700
522	0.000	-199.800	278.900
523	0.000	-183.600	247.300
524	0.000	-295.000	175.400
525	0.000	-252.500	175.400
526	0.000	-295.000	135.200
527	0.000	-252.500	135.200
528	0.000	-210.000	175.400
529	0.000	-210.000	135.200
530	0.000	-167.500	175.400
531	0.000	-167.500	135.200
532	0.000	-125.000	175.400
533	0.000	-125.000	135.200
534	0.000	-82.500	175.400
535	0.000	-82.500	135.200

ASTE-- ----- ----- ----- ----- num.=						4
Nome	Proprieta`	Nodo iniz.	Nodo fin.	Rilasci in.	Rilasci fin.	Orient.
4	1	1	314			0.0
5	1	2	316			0.0
6	1	5	319			0.0
7	1	6	321			0.0

GUSCI TRIANGOLARI-- ----- ----- ----- ----- num.=						36
---	--	--	--	--	--	----

Nome	Proprieta`	Nodo 1	Nodo 2	Nodo 3
21	1	131	132	133
24	1	135	137	130
25	1	137	129	130
27	1	138	139	140
30	1	144	142	104
31	1	102	144	104
39	2	153	154	155
42	2	159	157	152
43	2	151	159	152
69	2	189	190	191
72	2	193	195	188
73	2	195	187	188
199	3	279	311	280
200	3	279	277	311
201	3	311	277	278
202	3	266	313	267
203	3	266	263	313
204	3	313	263	265
293	3	402	446	404
294	3	402	400	446
295	3	446	400	401
296	3	388	447	390
297	3	388	385	447
298	3	447	385	387
319	1	472	473	474
322	1	476	478	449
323	1	478	471	449
325	1	479	480	481
328	1	485	483	448
329	1	452	485	448
341	2	492	493	494
344	2	496	498	491
345	2	498	490	491
371	2	517	518	519
374	2	523	521	516
375	2	515	523	516

GUSCI RETTANGOLARI |-----|-----|-----|-----| num.= 344

Nome	Proprieta`	Nodo 1	Nodo 2	Nodo 3	Nodo 4
1	1	100	101	102	103
2	1	103	102	104	316
3	1	105	100	103	106
4	1	106	103	316	107
5	1	108	105	106	109
6	1	109	106	107	110
7	1	111	108	109	112
8	1	112	109	110	113
9	1	114	111	112	115
10	1	115	112	113	116
11	1	117	114	115	118
12	1	118	115	116	119
13	1	120	117	118	121
14	1	121	118	119	122
15	1	123	120	121	124
16	1	124	121	122	125
17	1	126	123	124	127
18	1	127	124	125	314
19	1	128	126	127	129
20	1	129	127	314	130
22	1	132	134	135	133
23	1	134	136	137	135
26	1	136	128	129	137
28	1	141	138	140	142
29	1	143	141	142	144
32	1	101	143	144	102
33	2	145	146	147	148

34	2	104	142	146	145
35	2	146	149	150	147
36	2	142	140	149	146
37	2	149	151	152	150
38	2	140	139	151	149
40	2	156	153	155	157
41	2	158	156	157	159
44	2	139	158	159	151
45	2	155	154	160	161
46	2	161	160	162	163
47	2	163	162	164	165
48	2	157	155	161	166
49	2	166	161	163	167
50	2	167	163	165	168
51	2	152	157	166	169
52	2	169	166	167	170
53	2	170	167	168	171
54	2	150	152	169	172
55	2	172	169	170	173
56	2	173	170	171	174
57	2	147	150	172	175
58	2	175	172	173	176
59	2	176	173	174	177
60	2	148	147	175	178
61	2	178	175	176	179
62	2	179	176	177	180
63	2	181	182	183	184
64	2	135	130	182	181
65	2	185	181	184	186
66	2	133	135	181	185
67	2	187	185	186	188
68	2	131	133	185	187
70	2	190	192	193	191
71	2	192	194	195	193
74	2	194	131	187	195
75	2	184	183	196	197
76	2	197	196	198	199
77	2	199	198	200	201
78	2	186	184	197	202
79	2	202	197	199	203
80	2	203	199	201	204
81	2	188	186	202	205
82	2	205	202	203	206
83	2	206	203	204	207
84	2	193	188	205	208
85	2	208	205	206	209
86	2	209	206	207	210
87	2	191	193	208	211
88	2	211	208	209	212
89	2	212	209	210	213
90	2	189	191	211	214
91	2	214	211	212	215
92	2	215	212	213	216
93	3	316	104	145	217
94	3	217	145	148	218
95	3	107	316	217	219
96	3	219	217	218	220
97	3	110	107	219	221
98	3	221	219	220	222
99	3	113	110	221	223
100	3	223	221	222	224
101	3	116	113	223	225
102	3	225	223	224	226
103	3	119	116	225	227
104	3	227	225	226	228
105	3	122	119	227	229
106	3	229	227	228	230

107	3	125	122	229	231
108	3	231	229	230	232
109	3	314	125	231	233
110	3	233	231	232	234
111	3	130	314	233	182
112	3	182	233	234	183
113	3	218	148	178	235
114	3	235	178	179	236
115	3	236	179	180	237
116	3	220	218	235	238
117	3	238	235	236	239
118	3	239	236	237	240
119	3	222	220	238	241
120	3	241	238	239	242
121	3	242	239	240	243
122	3	224	222	241	244
123	3	244	241	242	245
124	3	245	242	243	246
125	3	226	224	244	247
126	3	247	244	245	248
127	3	248	245	246	249
128	3	228	226	247	250
129	3	250	247	248	251
130	3	251	248	249	252
131	3	230	228	250	253
132	3	253	250	251	254
133	3	254	251	252	255
134	3	232	230	253	256
135	3	256	253	254	257
136	3	257	254	255	258
137	3	234	232	256	259
138	3	259	256	257	260
139	3	260	257	258	261
140	3	183	234	259	196
141	3	196	259	260	198
142	3	198	260	261	200
143	3	237	180	262	263
144	3	263	262	264	265
145	3	240	237	263	266
147	3	243	240	266	268
148	3	268	266	267	269
149	3	246	243	268	270
150	3	270	268	269	271
151	3	249	246	270	272
152	3	272	270	271	312
153	3	252	249	272	273
154	3	273	272	312	274
155	3	255	252	273	275
156	3	275	273	274	276
157	3	258	255	275	277
158	3	277	275	276	278
159	3	261	258	277	279
161	3	200	261	279	281
162	3	281	279	280	282
175	2	165	283	284	164
176	2	283	285	286	284
177	2	168	287	283	165
178	2	287	288	285	283
179	2	171	289	287	168
180	2	289	290	288	287
181	2	174	291	289	171
182	2	291	292	290	289
183	2	177	293	291	174
184	2	293	294	292	291
185	2	180	295	293	177
186	2	295	296	294	293
187	2	201	297	298	200

188	2	297	299	300	298
189	2	204	301	297	201
190	2	301	302	299	297
191	2	207	303	301	204
192	2	303	304	302	301
193	2	210	305	303	207
194	2	305	306	304	303
195	2	213	307	305	210
196	2	307	308	306	305
197	2	216	309	307	213
198	2	309	310	308	307
205	3	322	323	324	325
206	3	326	322	325	327
207	3	328	329	326	330
208	3	330	326	327	331
209	3	332	328	330	333
210	3	333	330	331	334
211	3	335	332	333	336
212	3	336	333	334	337
213	3	338	335	336	339
214	3	339	336	337	340
215	3	341	338	339	342
216	3	342	339	340	343
217	3	344	341	342	345
218	3	345	342	343	346
219	3	347	345	346	348
220	3	349	347	348	350
221	3	325	324	351	352
222	3	352	351	353	354
223	3	354	353	355	356
224	3	327	325	352	357
225	3	357	352	354	358
226	3	358	354	356	359
227	3	331	327	357	360
228	3	360	357	358	361
229	3	361	358	359	362
230	3	334	331	360	363
231	3	363	360	361	364
232	3	364	361	362	365
233	3	337	334	363	366
234	3	366	363	364	367
235	3	367	364	365	368
236	3	340	337	366	369
237	3	369	366	367	370
238	3	370	367	368	371
239	3	343	340	369	372
240	3	372	369	370	373
241	3	373	370	371	374
242	3	346	343	372	375
243	3	375	372	373	376
244	3	376	373	374	377
245	3	348	346	375	378
246	3	378	375	376	379
247	3	379	376	377	380
248	3	350	348	378	381
249	3	381	378	379	382
250	3	382	379	380	383
251	3	356	355	384	385
252	3	385	384	386	387
253	3	359	356	385	388
254	3	362	359	388	389
255	3	389	388	390	391
256	3	365	362	389	392
257	3	392	389	391	393
258	3	368	365	392	394
259	3	394	392	393	395
260	3	371	368	394	396

261	3	396	394	395	397
262	3	374	371	396	398
263	3	398	396	397	399
264	3	377	374	398	400
265	3	400	398	399	401
266	3	380	377	400	402
267	3	383	380	402	403
268	3	403	402	404	405
269	2	406	407	408	409
270	2	407	410	411	408
271	2	412	413	407	406
272	2	413	414	410	407
273	2	415	416	413	412
274	2	416	417	414	413
275	2	418	419	416	415
276	2	419	420	417	416
277	2	421	422	419	418
278	2	422	423	420	419
279	2	355	424	422	421
280	2	424	425	423	422
281	2	426	427	428	383
282	2	427	429	430	428
283	2	431	432	427	426
284	2	432	433	429	427
285	2	434	435	432	431
286	2	435	436	433	432
287	2	437	438	435	434
288	2	438	439	436	435
289	2	440	441	438	437
290	2	441	442	439	438
291	2	443	444	441	440
292	2	444	445	442	441
299	3	321	448	323	322
300	3	329	321	322	326
301	3	319	344	345	347
302	3	449	319	347	349
303	1	450	451	452	453
304	1	454	450	453	455
305	1	456	454	455	457
306	1	457	455	329	328
307	1	458	456	457	459
308	1	459	457	328	332
309	1	460	458	459	461
310	1	461	459	332	335
311	1	462	460	461	463
312	1	463	461	335	338
313	1	464	462	463	465
314	1	465	463	338	341
315	1	466	464	465	467
316	1	467	465	341	344
317	1	468	466	467	469
318	1	470	468	469	471
320	1	473	475	476	474
321	1	475	477	478	476
324	1	477	470	471	478
326	1	482	479	481	483
327	1	484	482	483	485
330	1	451	484	485	452
331	1	453	452	448	321
332	1	455	453	321	329
333	1	469	467	344	319
334	1	471	469	319	449
335	2	486	349	350	487
336	2	476	449	349	486
337	2	488	486	487	489
338	2	474	476	486	488
339	2	490	488	489	491

340	2	472	474	488	490
342	2	493	495	496	494
343	2	495	497	498	496
346	2	497	472	490	498
347	2	487	350	381	499
348	2	499	381	382	500
349	2	500	382	383	426
350	2	489	487	499	501
351	2	501	499	500	502
352	2	502	500	426	431
353	2	491	489	501	503
354	2	503	501	502	504
355	2	504	502	431	434
356	2	496	491	503	505
357	2	505	503	504	506
358	2	506	504	434	437
359	2	494	496	505	507
360	2	507	505	506	508
361	2	508	506	437	440
362	2	492	494	507	509
363	2	509	507	508	510
364	2	510	508	440	443
365	2	323	511	512	324
366	2	448	483	511	323
367	2	511	513	514	512
368	2	483	481	513	511
369	2	513	515	516	514
370	2	481	480	515	513
372	2	520	517	519	521
373	2	522	520	521	523
376	2	480	522	523	515
377	2	519	518	524	525
378	2	525	524	526	527
379	2	527	526	409	406
380	2	521	519	525	528
381	2	528	525	527	529
382	2	529	527	406	412
383	2	516	521	528	530
384	2	530	528	529	531
385	2	531	529	412	415
386	2	514	516	530	532
387	2	532	530	531	533
388	2	533	531	415	418
389	2	512	514	532	534
390	2	534	532	533	535
391	2	535	533	418	421
392	2	324	512	534	351
393	2	351	534	535	353
394	2	353	535	421	355

PROPRIETA` ASTE---							num.=	1
Nome	Materiale	Base Kw vertic.	Altezza Kw orizz.	Area J tors.	Area tag. J fless. Y	Area tag. J fless. Z		
1	1	20.00 0.000000	20.00 0.000000	4.00000E+02 2.25330E+04	3.33333E+02 1.33333E+04	3.33333E+02 1.33333E+04		

PROPRIETA` GUSCI--					num.=	3
Nome	Materiale	Sp.membr.	Sp. piastra	Kw		
1	1	20.00	20.00	0.000000		
2	1	40.00	40.00	0.000000		
3	1	140.00	140.00	0.000000		

MATERIALI-----						num.=	1
Nome	Mod. elast.	Coeff. nu	Mod. tang.	Peso spec.	Dil. te.		
1	3.00000E+05	1.50000E-01	1.30000E+05	2.50000E-03	1.00000E-05		

VINCOLI-----							num.=	6
--------------	--	--	--	--	--	--	-------	---

Nodo	Rigid. X	Rigid. Y	Rigid. Z	Rigid. RX	Rigid. RY	Rigid. RZ
311	2.98328E+05	2.98328E+05	8.16192E+05	6.50725E+09	6.50725E+09	4.76827E+08
312	2.98328E+05	2.98328E+05	8.16192E+05	6.50725E+09	6.50725E+09	4.76827E+08
313	2.98328E+05	2.98328E+05	8.16192E+05	6.50725E+09	6.50725E+09	4.76827E+08
395	2.98328E+05	2.98328E+05	8.16192E+05	6.50725E+09	6.50725E+09	4.76827E+08
446	2.98328E+05	2.98328E+05	8.16192E+05	6.50725E+09	6.50725E+09	4.76827E+08
447	2.98328E+05	2.98328E+05	8.16192E+05	6.50725E+09	6.50725E+09	4.76827E+08

CARICHI NODI-----|-----|-----|-----|-----|num.= 296

Nome	Nodo	Direzione	Intensita`
1 azioni.txt_1	1	Z	-13372.5
2 azioni.txt_2	1	Z	-12907.5
3 azioni.txt_3	1	Z	-13372.5
4 azioni.txt_4	1	Z	-12907.5
5 azioni.txt_5	1	Z	-13372.5
6 azioni.txt_6	1	Z	-12907.5
7 azioni.txt_7	1	Z	-13372.5
8 azioni.txt_8	1	Z	-12907.5
9 azioni.txt_9	1	Z	-13372.5
10 azioni.txt_10	1	Z	-12907.5
11 azioni.txt_11	1	Z	-13372.5
12 azioni.txt_12	1	Z	-12907.5
13 azioni.txt_13	1	Z	-13372.5
14 azioni.txt_14	1	Z	-12907.5
15 azioni.txt_15	1	Z	-13372.5
16 azioni.txt_16	1	Z	-12907.5
17 azioni.txt_17	1	Z	-13915.0
18 azioni.txt_18	1	Z	-13915.0
19 azioni.txt_19	1	Z	-13915.0
20 azioni.txt_20	1	Z	-13915.0
21 azioni.txt_21	1	Z	-12365.0
22 azioni.txt_22	1	Z	-12365.0
23 azioni.txt_23	1	Z	-12365.0
24 azioni.txt_24	1	Z	-12365.0
25 azioni.txt_25	1	Z	-13140.0
26 azioni.txt_26	1	Z	-21650.0
27 azioni.txt_27	1	Z	-30840.0
28 azioni.txt_28	1	Z	-23950.0
29 azioni.txt_29	1	Z	-21650.0
30 azioni.txt_30	1	Z	-16210.0
31 azioni.txt_31	1	Z	-13140.0
32 azioni.txt_32	1	Z	-20800.0
33 azioni.txt_33	1	Z	-14680.0
34 azioni.txt_34	1	Z	-14670.0
35 azioni.txt_35	1	Z	-1812.0
36 azioni.txt_36	1	Z	-5667.0
37 azioni.txt_37	1	Z	-5667.0
38 azioni.txt_38	1	Z	-1532.0
39 azioni.txt_40	1	Z	-7658.0
40 azioni.txt_41	1	Z	-1526.0
41 azioni.txt_42	1	Z	-24480.0
42 azioni.txt_43	1	Z	-16560.0
43 azioni.txt_44	1	Z	-3418.0
44 azioni.txt_45	1	Z	-30840.0
45 azioni.txt_47	1	Z	-30840.0
46 azioni.txt_48	2	X	11430.0
47 azioni.txt_48	2	Z	-13372.5
48 azioni.txt_49	2	X	11430.0
49 azioni.txt_49	2	Z	-12907.5
50 azioni.txt_50	2	X	13770.0
51 azioni.txt_50	2	Z	-13372.5
52 azioni.txt_51	2	X	13770.0
53 azioni.txt_51	2	Z	-12907.5
54 azioni.txt_52	2	X	-13770.0
55 azioni.txt_52	2	Z	-13372.5
56 azioni.txt_53	2	X	-13770.0
57 azioni.txt_53	2	Z	-12907.5

58	azioni.txt_54	2	X	-11430.0
59	azioni.txt_54	2	Z	-13372.5
60	azioni.txt_55	2	X	-11430.0
61	azioni.txt_55	2	Z	-12907.5
62	azioni.txt_56	2	X	-120.0
63	azioni.txt_56	2	Z	-13372.5
64	azioni.txt_57	2	X	-120.0
65	azioni.txt_57	2	Z	-12907.5
66	azioni.txt_58	2	X	-7680.0
67	azioni.txt_58	2	Z	-13372.5
68	azioni.txt_59	2	X	-7680.0
69	azioni.txt_59	2	Z	-12907.5
70	azioni.txt_60	2	X	7680.0
71	azioni.txt_60	2	Z	-13372.5
72	azioni.txt_61	2	X	7680.0
73	azioni.txt_61	2	Z	-12907.5
74	azioni.txt_62	2	X	120.0
75	azioni.txt_62	2	Z	-13372.5
76	azioni.txt_63	2	X	120.0
77	azioni.txt_63	2	Z	-12907.5
78	azioni.txt_64	2	X	2610.0
79	azioni.txt_64	2	Z	-13915.0
80	azioni.txt_65	2	X	4950.0
81	azioni.txt_65	2	Z	-13915.0
82	azioni.txt_66	2	X	-4950.0
83	azioni.txt_66	2	Z	-13915.0
84	azioni.txt_67	2	X	-2610.0
85	azioni.txt_67	2	Z	-13915.0
86	azioni.txt_68	2	X	2610.0
87	azioni.txt_68	2	Z	-12365.0
88	azioni.txt_69	2	X	4950.0
89	azioni.txt_69	2	Z	-12365.0
90	azioni.txt_70	2	X	-4950.0
91	azioni.txt_70	2	Z	-12365.0
92	azioni.txt_71	2	X	-2610.0
93	azioni.txt_71	2	Z	-12365.0
94	azioni.txt_72	2	X	-3110.0
95	azioni.txt_72	2	Z	-13140.0
96	azioni.txt_73	2	X	-1866.0
97	azioni.txt_73	2	Z	-21650.0
98	azioni.txt_74	2	X	-1866.0
99	azioni.txt_74	2	Z	-30840.0
100	azioni.txt_75	2	X	-3110.0
101	azioni.txt_75	2	Z	-23950.0
102	azioni.txt_76	2	X	844.9
103	azioni.txt_76	2	Z	-24840.0
104	azioni.txt_77	2	X	-2074.0
105	azioni.txt_77	2	Z	-16210.0
106	azioni.txt_78	2	X	-2074.0
107	azioni.txt_78	2	Z	-13140.0
108	azioni.txt_79	2	X	-1244.0
109	azioni.txt_79	2	Z	-20800.0
110	azioni.txt_80	2	X	-1244.0
111	azioni.txt_80	2	Z	-14680.0
112	azioni.txt_81	2	X	563.3
113	azioni.txt_81	2	Z	-16800.0
114	azioni.txt_82	2	Z	-1812.0
115	azioni.txt_83	2	Z	-5667.0
116	azioni.txt_84	2	Z	-5667.0
117	azioni.txt_85	2	Z	-1532.0
118	azioni.txt_86	2	X	-2074.0
119	azioni.txt_87	2	Z	-7658.0
120	azioni.txt_88	2	X	-563.3
121	azioni.txt_88	2	Z	-3657.0
122	azioni.txt_89	2	X	844.9
123	azioni.txt_89	2	Z	-31620.0
124	azioni.txt_90	2	X	563.3

125	azioni.txt_90	2	Z	-21320.0
126	azioni.txt_91	2	X	-563.3
127	azioni.txt_91	2	Z	-8174.0
128	azioni.txt_92	2	X	13770.0
129	azioni.txt_92	2	Z	-31620.0
130	azioni.txt_93	2	X	-13770.0
131	azioni.txt_94	2	X	-13770.0
132	azioni.txt_94	2	Z	-31620.0
133	azioni.txt_95	5	X	12948.0
134	azioni.txt_95	5	Y	4519.0
135	azioni.txt_95	5	Z	-13098.1
136	azioni.txt_96	5	X	12948.0
137	azioni.txt_96	5	Y	4519.0
138	azioni.txt_96	5	Z	-12661.9
139	azioni.txt_97	5	X	10452.0
140	azioni.txt_97	5	Y	-5741.0
141	azioni.txt_97	5	Z	-13098.1
142	azioni.txt_98	5	X	10452.0
143	azioni.txt_98	5	Y	-5741.0
144	azioni.txt_98	5	Z	-12661.9
145	azioni.txt_99	5	X	-10452.0
146	azioni.txt_99	5	Y	5741.0
147	azioni.txt_99	5	Z	-13098.1
148	azioni.txt_100	5	X	-10452.0
149	azioni.txt_100	5	Y	5741.0
150	azioni.txt_100	5	Z	-12661.9
151	azioni.txt_101	5	X	-12948.0
152	azioni.txt_101	5	Y	-4519.0
153	azioni.txt_101	5	Z	-13098.1
154	azioni.txt_102	5	X	-12948.0
155	azioni.txt_102	5	Y	-4519.0
156	azioni.txt_102	5	Z	-12661.9
157	azioni.txt_103	5	X	7670.0
158	azioni.txt_103	5	Y	16916.7
159	azioni.txt_103	5	Z	-13098.1
160	azioni.txt_104	5	X	7670.0
161	azioni.txt_104	5	Y	16916.7
162	azioni.txt_104	5	Z	-12661.9
163	azioni.txt_105	5	X	650.0
164	azioni.txt_105	5	Y	17283.3
165	azioni.txt_105	5	Z	-13098.1
166	azioni.txt_106	5	X	650.0
167	azioni.txt_106	5	Y	17283.3
168	azioni.txt_106	5	Z	-12661.9
169	azioni.txt_107	5	X	-650.0
170	azioni.txt_107	5	Y	-17283.3
171	azioni.txt_107	5	Z	-13098.1
172	azioni.txt_108	5	X	-650.0
173	azioni.txt_108	5	Y	-17283.3
174	azioni.txt_108	5	Z	-12661.9
175	azioni.txt_109	5	X	-7670.0
176	azioni.txt_109	5	Y	-16916.7
177	azioni.txt_109	5	Z	-13098.1
178	azioni.txt_110	5	X	-7670.0
179	azioni.txt_110	5	Y	-16916.7
180	azioni.txt_110	5	Z	-12661.9
181	azioni.txt_111	5	X	4758.0
182	azioni.txt_111	5	Y	4946.7
183	azioni.txt_111	5	Z	-13607.0
184	azioni.txt_112	5	X	2262.0
185	azioni.txt_112	5	Y	-5313.3
186	azioni.txt_112	5	Z	-13607.0
187	azioni.txt_113	5	X	-2262.0
188	azioni.txt_113	5	Y	5313.3
189	azioni.txt_113	5	Z	-13607.0
190	azioni.txt_114	5	X	-4758.0
191	azioni.txt_114	5	Y	-4946.7

192	azioni.txt_114	5	Z	-13607.0
193	azioni.txt_115	5	X	4758.0
194	azioni.txt_115	5	Y	4946.7
195	azioni.txt_115	5	Z	-12153.0
196	azioni.txt_116	5	X	2262.0
197	azioni.txt_116	5	Y	-5313.3
198	azioni.txt_116	5	Z	-12153.0
199	azioni.txt_117	5	X	-2262.0
200	azioni.txt_117	5	Y	5313.3
201	azioni.txt_117	5	Z	-12153.0
202	azioni.txt_118	5	X	-4946.7
203	azioni.txt_118	5	Y	-4946.7
204	azioni.txt_118	5	Z	-12153.0
205	azioni.txt_119	5	X	-3048.0
206	azioni.txt_119	5	Z	-12880.0
207	azioni.txt_120	5	X	-1828.0
208	azioni.txt_120	5	Z	-21220.0
209	azioni.txt_121	5	X	-1828.0
210	azioni.txt_121	5	Z	-30220.0
211	azioni.txt_122	5	X	-3048.0
212	azioni.txt_122	5	Z	-23470.0
213	azioni.txt_123	5	X	-844.9
214	azioni.txt_123	5	Y	-10800.0
215	azioni.txt_123	5	Z	-26180.0
216	azioni.txt_124	5	X	-2032.0
217	azioni.txt_124	5	Z	-15880.0
218	azioni.txt_125	5	X	-2032.0
219	azioni.txt_125	5	Z	-12880.0
220	azioni.txt_126	5	X	-1219.0
221	azioni.txt_126	5	Z	-20390.0
222	azioni.txt_127	5	X	-1219.0
223	azioni.txt_127	5	Z	-14380.0
224	azioni.txt_128	5	X	-563.3
225	azioni.txt_128	5	Y	-7200.0
226	azioni.txt_128	5	Z	-17690.0
227	azioni.txt_129	5	Z	-1778.0
228	azioni.txt_130	5	Z	-5552.0
229	azioni.txt_131	5	Z	-5552.0
230	azioni.txt_132	5	Z	-1501.0
231	azioni.txt_133	5	X	-2032.0
232	azioni.txt_134	5	Z	-7503.0
233	azioni.txt_135	5	X	563.3
234	azioni.txt_135	5	Y	7200.0
235	azioni.txt_135	5	Z	-4804.0
236	azioni.txt_136	5	X	-844.9
237	azioni.txt_136	5	Y	19400.0
238	azioni.txt_136	5	Z	-19400.0
239	azioni.txt_137	5	X	-563.3
240	azioni.txt_137	5	Y	13170.0
241	azioni.txt_137	5	Z	-13170.0
242	azioni.txt_138	5	X	563.3
243	azioni.txt_138	5	Y	7200.0
244	azioni.txt_138	5	Z	-287.6
245	azioni.txt_139	5	X	12948.0
246	azioni.txt_139	5	Y	30220.0
247	azioni.txt_139	5	Z	-30220.0
248	azioni.txt_140	5	X	-12948.0
249	azioni.txt_141	5	X	-12948.0
250	azioni.txt_141	5	Y	30220.0
251	azioni.txt_141	5	Z	-30220.0
252	azioni.txt_142	6	Z	-13098.1
253	azioni.txt_143	6	Z	-12661.9
254	azioni.txt_144	6	Z	-13098.1
255	azioni.txt_145	6	Z	-12661.9
256	azioni.txt_146	6	Z	-13098.1
257	azioni.txt_147	6	Z	-12661.9
258	azioni.txt_148	6	Z	-13098.1

259	azioni.txt_149	6	Z	-12661.9
260	azioni.txt_150	6	Z	-13098.1
261	azioni.txt_151	6	Z	-12661.9
262	azioni.txt_152	6	Z	-13098.1
263	azioni.txt_153	6	Z	-12661.9
264	azioni.txt_154	6	Z	-13098.1
265	azioni.txt_155	6	Z	-12661.9
266	azioni.txt_156	6	Z	-13098.1
267	azioni.txt_157	6	Z	-12661.9
268	azioni.txt_158	6	Z	-13607.0
269	azioni.txt_159	6	Z	-13607.0
270	azioni.txt_160	6	Z	-13607.0
271	azioni.txt_161	6	Z	-13607.0
272	azioni.txt_162	6	Z	-12153.0
273	azioni.txt_163	6	Z	-12153.0
274	azioni.txt_164	6	Z	-12153.0
275	azioni.txt_165	6	Z	-12153.0
276	azioni.txt_166	6	Z	-12880.0
277	azioni.txt_167	6	Z	-21220.0
278	azioni.txt_168	6	Z	-30220.0
279	azioni.txt_169	6	Z	-23470.0
280	azioni.txt_170	6	Z	-21990.0
281	azioni.txt_171	6	Z	-15880.0
282	azioni.txt_172	6	Z	-12880.0
283	azioni.txt_173	6	Z	-20390.0
284	azioni.txt_174	6	Z	-14380.0
285	azioni.txt_175	6	Z	-14900.0
286	azioni.txt_176	6	Z	-1778.0
287	azioni.txt_177	6	Z	-5552.0
288	azioni.txt_178	6	Z	-5552.0
289	azioni.txt_179	6	Z	-1501.0
290	azioni.txt_181	6	Z	-7503.0
291	azioni.txt_182	6	Z	-2012.0
292	azioni.txt_183	6	Z	-19150.0
293	azioni.txt_184	6	Z	-13000.0
294	azioni.txt_185	6	Z	-120.6
295	azioni.txt_186	6	Z	-30220.0
296	azioni.txt_188	6	Z	-30220.0

PESI PROPRI ASTE--|-----|-----|-----|-----|-----|
 Cond. Nome Carichi Aste
 48 297-300 4-7

CARICHI DI LINEA |-----|-----|-----|-----|num.= 0
 numero coordinata Intensità
 Nome inizio fine Cond. Direz. inizio fine Descrizione

CARICHI GUSCI----|-----|-----|-----|-----|num.= 1424
 Nome Guscio Dir Tip RIF Intensita`
 301 pesoterra 175 Z FD glo -0.36000
 302 pesoterra 176 Z FD glo -0.36000
 303 pesoterra 177 Z FD glo -0.36000
 304 pesoterra 178 Z FD glo -0.36000
 305 pesoterra 179 Z FD glo -0.36000
 306 pesoterra 180 Z FD glo -0.36000
 307 pesoterra 181 Z FD glo -0.36000
 308 pesoterra 182 Z FD glo -0.36000
 309 pesoterra 183 Z FD glo -0.36000
 310 pesoterra 184 Z FD glo -0.36000
 311 pesoterra 185 Z FD glo -0.36000
 312 pesoterra 186 Z FD glo -0.36000
 313 pesoterra 187 Z FD glo -0.36000
 314 pesoterra 188 Z FD glo -0.36000
 315 pesoterra 189 Z FD glo -0.36000
 316 pesoterra 190 Z FD glo -0.36000
 317 pesoterra 191 Z FD glo -0.36000
 318 pesoterra 192 Z FD glo -0.36000

319	pesoterra	193	Z	FD glo	-0.36000
320	pesoterra	194	Z	FD glo	-0.36000
321	pesoterra	195	Z	FD glo	-0.36000
322	pesoterra	196	Z	FD glo	-0.36000
323	pesoterra	197	Z	FD glo	-0.36000
324	pesoterra	198	Z	FD glo	-0.36000
325	pesoterra	269	Z	FD glo	-0.36000
326	pesoterra	270	Z	FD glo	-0.36000
327	pesoterra	271	Z	FD glo	-0.36000
328	pesoterra	272	Z	FD glo	-0.36000
329	pesoterra	273	Z	FD glo	-0.36000
330	pesoterra	274	Z	FD glo	-0.36000
331	pesoterra	275	Z	FD glo	-0.36000
332	pesoterra	276	Z	FD glo	-0.36000
333	pesoterra	277	Z	FD glo	-0.36000
334	pesoterra	278	Z	FD glo	-0.36000
335	pesoterra	279	Z	FD glo	-0.36000
336	pesoterra	280	Z	FD glo	-0.36000
337	pesoterra	281	Z	FD glo	-0.36000
338	pesoterra	282	Z	FD glo	-0.36000
339	pesoterra	283	Z	FD glo	-0.36000
340	pesoterra	284	Z	FD glo	-0.36000
341	pesoterra	285	Z	FD glo	-0.36000
342	pesoterra	286	Z	FD glo	-0.36000
343	pesoterra	287	Z	FD glo	-0.36000
344	pesoterra	288	Z	FD glo	-0.36000
345	pesoterra	289	Z	FD glo	-0.36000
346	pesoterra	290	Z	FD glo	-0.36000
347	pesoterra	291	Z	FD glo	-0.36000
348	pesoterra	292	Z	FD glo	-0.36000
349	spintaterra	205	Z	FD loc	0.16490
350	spintaterra	206	Z	FD loc	0.16490
351	spintaterra	207	Z	FD loc	0.11953
352	spintaterra	208	Z	FD loc	0.16490
353	spintaterra	209	Z	FD loc	0.11953
354	spintaterra	210	Z	FD loc	0.16490
355	spintaterra	211	Z	FD loc	0.11953
356	spintaterra	212	Z	FD loc	0.16490
357	spintaterra	213	Z	FD loc	0.11953
358	spintaterra	214	Z	FD loc	0.16490
359	spintaterra	215	Z	FD loc	0.11953
360	spintaterra	216	Z	FD loc	0.16490
361	spintaterra	217	Z	FD loc	0.11953
362	spintaterra	218	Z	FD loc	0.16490
363	spintaterra	219	Z	FD loc	0.16490
364	spintaterra	220	Z	FD loc	0.16490
365	spintaterra	221	Z	FD loc	0.20922
366	spintaterra	222	Z	FD loc	0.25249
367	spintaterra	223	Z	FD loc	0.29576
368	spintaterra	224	Z	FD loc	0.20922
369	spintaterra	225	Z	FD loc	0.25249
370	spintaterra	226	Z	FD loc	0.29576
371	spintaterra	227	Z	FD loc	0.20922
372	spintaterra	228	Z	FD loc	0.25249
373	spintaterra	229	Z	FD loc	0.29576
374	spintaterra	230	Z	FD loc	0.20922
375	spintaterra	231	Z	FD loc	0.25249
376	spintaterra	232	Z	FD loc	0.29576
377	spintaterra	233	Z	FD loc	0.20922
378	spintaterra	234	Z	FD loc	0.25249
379	spintaterra	235	Z	FD loc	0.29576
380	spintaterra	236	Z	FD loc	0.20922
381	spintaterra	237	Z	FD loc	0.25249
382	spintaterra	238	Z	FD loc	0.29576
383	spintaterra	239	Z	FD loc	0.20922
384	spintaterra	240	Z	FD loc	0.25249
385	spintaterra	241	Z	FD loc	0.29576

386	spintaterra	242	Z	FD loc	0.20922
387	spintaterra	243	Z	FD loc	0.25249
388	spintaterra	244	Z	FD loc	0.29576
389	spintaterra	245	Z	FD loc	0.20922
390	spintaterra	246	Z	FD loc	0.25249
391	spintaterra	247	Z	FD loc	0.29576
392	spintaterra	248	Z	FD loc	0.20922
393	spintaterra	249	Z	FD loc	0.25249
394	spintaterra	250	Z	FD loc	0.29576
395	spintaterra	251	Z	FD loc	0.34295
396	spintaterra	252	Z	FD loc	0.39405
397	spintaterra	253	Z	FD loc	0.34295
398	spintaterra	254	Z	FD loc	0.34295
399	spintaterra	255	Z	FD loc	0.39405
400	spintaterra	256	Z	FD loc	0.34295
401	spintaterra	257	Z	FD loc	0.39405
402	spintaterra	258	Z	FD loc	0.34295
403	spintaterra	259	Z	FD loc	0.39405
404	spintaterra	260	Z	FD loc	0.34295
405	spintaterra	261	Z	FD loc	0.39405
406	spintaterra	262	Z	FD loc	0.34295
407	spintaterra	263	Z	FD loc	0.39405
408	spintaterra	264	Z	FD loc	0.34295
409	spintaterra	265	Z	FD loc	0.39405
410	spintaterra	266	Z	FD loc	0.34295
411	spintaterra	267	Z	FD loc	0.34295
412	spintaterra	268	Z	FD loc	0.39405
413	spintaterra	293	Z	FD loc	0.40257
414	spintaterra	294	Z	FD loc	0.38553
415	spintaterra	295	Z	FD loc	0.40257
416	spintaterra	296	Z	FD loc	0.40257
417	spintaterra	297	Z	FD loc	0.38553
418	spintaterra	298	Z	FD loc	0.40257
419	spintaterra	299	Z	FD loc	0.12014
420	spintaterra	300	Z	FD loc	0.11901
421	spintaterra	301	Z	FD loc	0.11901
422	spintaterra	302	Z	FD loc	0.12014
423	spintaterra	303	Z	FD loc	0.02826
424	spintaterra	304	Z	FD loc	0.02826
425	spintaterra	305	Z	FD loc	0.02826
426	spintaterra	306	Z	FD loc	0.07399
427	spintaterra	307	Z	FD loc	0.02826
428	spintaterra	308	Z	FD loc	0.07399
429	spintaterra	309	Z	FD loc	0.02826
430	spintaterra	310	Z	FD loc	0.07399
431	spintaterra	311	Z	FD loc	0.02826
432	spintaterra	312	Z	FD loc	0.07399
433	spintaterra	313	Z	FD loc	0.02826
434	spintaterra	314	Z	FD loc	0.07399
435	spintaterra	315	Z	FD loc	0.02826
436	spintaterra	316	Z	FD loc	0.07399
437	spintaterra	317	Z	FD loc	0.02826
438	spintaterra	318	Z	FD loc	0.02826
439	spintaterra	319	Z	FD loc	0.08923
440	spintaterra	320	Z	FD loc	0.07907
441	spintaterra	321	Z	FD loc	0.06038
442	spintaterra	322	Z	FD loc	0.08542
443	spintaterra	323	Z	FD loc	0.07017
444	spintaterra	324	Z	FD loc	0.03461
445	spintaterra	325	Z	FD loc	0.08923
446	spintaterra	326	Z	FD loc	0.07907
447	spintaterra	327	Z	FD loc	0.06038
448	spintaterra	328	Z	FD loc	0.08542
449	spintaterra	329	Z	FD loc	0.07017
450	spintaterra	330	Z	FD loc	0.03461
451	spintaterra	331	Z	FD loc	0.07337
452	spintaterra	332	Z	FD loc	0.07451

453	spintaterra	333	Z	FD loc	0.07451
454	spintaterra	334	Z	FD loc	0.07337
455	spintaterra	335	Z	FD loc	0.16489
456	spintaterra	336	Z	FD loc	0.11952
457	spintaterra	337	Z	FD loc	0.16489
458	spintaterra	338	Z	FD loc	0.11952
459	spintaterra	339	Z	FD loc	0.16489
460	spintaterra	340	Z	FD loc	0.11952
461	spintaterra	341	Z	FD loc	0.18002
462	spintaterra	342	Z	FD loc	0.16994
463	spintaterra	343	Z	FD loc	0.15139
464	spintaterra	344	Z	FD loc	0.17624
465	spintaterra	345	Z	FD loc	0.16112
466	spintaterra	346	Z	FD loc	0.12583
467	spintaterra	347	Z	FD loc	0.20922
468	spintaterra	348	Z	FD loc	0.25249
469	spintaterra	349	Z	FD loc	0.29576
470	spintaterra	350	Z	FD loc	0.20922
471	spintaterra	351	Z	FD loc	0.25249
472	spintaterra	352	Z	FD loc	0.29576
473	spintaterra	353	Z	FD loc	0.20922
474	spintaterra	354	Z	FD loc	0.25249
475	spintaterra	355	Z	FD loc	0.29576
476	spintaterra	356	Z	FD loc	0.20922
477	spintaterra	357	Z	FD loc	0.25249
478	spintaterra	358	Z	FD loc	0.29576
479	spintaterra	359	Z	FD loc	0.20922
480	spintaterra	360	Z	FD loc	0.25249
481	spintaterra	361	Z	FD loc	0.29576
482	spintaterra	362	Z	FD loc	0.20922
483	spintaterra	363	Z	FD loc	0.25249
484	spintaterra	364	Z	FD loc	0.29576
485	spintaterra	365	Z	FD loc	0.16489
486	spintaterra	366	Z	FD loc	0.11952
487	spintaterra	367	Z	FD loc	0.16489
488	spintaterra	368	Z	FD loc	0.11952
489	spintaterra	369	Z	FD loc	0.16489
490	spintaterra	370	Z	FD loc	0.11952
491	spintaterra	371	Z	FD loc	0.18002
492	spintaterra	372	Z	FD loc	0.16994
493	spintaterra	373	Z	FD loc	0.15139
494	spintaterra	374	Z	FD loc	0.17624
495	spintaterra	375	Z	FD loc	0.16112
496	spintaterra	376	Z	FD loc	0.12583
497	spintaterra	377	Z	FD loc	0.20922
498	spintaterra	378	Z	FD loc	0.25249
499	spintaterra	379	Z	FD loc	0.29576
500	spintaterra	380	Z	FD loc	0.20922
501	spintaterra	381	Z	FD loc	0.25249
502	spintaterra	382	Z	FD loc	0.29576
503	spintaterra	383	Z	FD loc	0.20922
504	spintaterra	384	Z	FD loc	0.25249
505	spintaterra	385	Z	FD loc	0.29576
506	spintaterra	386	Z	FD loc	0.20922
507	spintaterra	387	Z	FD loc	0.25249
508	spintaterra	388	Z	FD loc	0.29576
509	spintaterra	389	Z	FD loc	0.20922
510	spintaterra	390	Z	FD loc	0.25249
511	spintaterra	391	Z	FD loc	0.29576
512	spintaterra	392	Z	FD loc	0.20922
513	spintaterra	393	Z	FD loc	0.25249
514	spintaterra	394	Z	FD loc	0.29576
515	spintaterra	94	Z	FD loc	0.16490
516	spintaterra	96	Z	FD loc	0.16490
517	spintaterra	97	Z	FD loc	0.11953
518	spintaterra	98	Z	FD loc	0.16490
519	spintaterra	99	Z	FD loc	0.11953

520	spintaterra	100	Z	FD loc	0.16490
521	spintaterra	101	Z	FD loc	0.11953
522	spintaterra	102	Z	FD loc	0.16490
523	spintaterra	103	Z	FD loc	0.11953
524	spintaterra	104	Z	FD loc	0.16490
525	spintaterra	105	Z	FD loc	0.11953
526	spintaterra	106	Z	FD loc	0.16490
527	spintaterra	107	Z	FD loc	0.11953
528	spintaterra	108	Z	FD loc	0.16490
529	spintaterra	110	Z	FD loc	0.16490
530	spintaterra	112	Z	FD loc	0.16490
531	spintaterra	113	Z	FD loc	0.20922
532	spintaterra	114	Z	FD loc	0.25249
533	spintaterra	115	Z	FD loc	0.29576
534	spintaterra	116	Z	FD loc	0.20922
535	spintaterra	117	Z	FD loc	0.25249
536	spintaterra	118	Z	FD loc	0.29576
537	spintaterra	119	Z	FD loc	0.20922
538	spintaterra	120	Z	FD loc	0.25249
539	spintaterra	121	Z	FD loc	0.29576
540	spintaterra	122	Z	FD loc	0.20922
541	spintaterra	123	Z	FD loc	0.25249
542	spintaterra	124	Z	FD loc	0.29576
543	spintaterra	125	Z	FD loc	0.20922
544	spintaterra	126	Z	FD loc	0.25249
545	spintaterra	127	Z	FD loc	0.29576
546	spintaterra	128	Z	FD loc	0.20922
547	spintaterra	129	Z	FD loc	0.25249
548	spintaterra	130	Z	FD loc	0.29576
549	spintaterra	131	Z	FD loc	0.20922
550	spintaterra	132	Z	FD loc	0.25249
551	spintaterra	133	Z	FD loc	0.29576
552	spintaterra	134	Z	FD loc	0.20922
553	spintaterra	135	Z	FD loc	0.25249
554	spintaterra	136	Z	FD loc	0.29576
555	spintaterra	137	Z	FD loc	0.20922
556	spintaterra	138	Z	FD loc	0.25249
557	spintaterra	139	Z	FD loc	0.29576
558	spintaterra	140	Z	FD loc	0.20922
559	spintaterra	141	Z	FD loc	0.25249
560	spintaterra	142	Z	FD loc	0.29576
561	spintaterra	143	Z	FD loc	0.34295
562	spintaterra	144	Z	FD loc	0.39405
563	spintaterra	145	Z	FD loc	0.34295
564	spintaterra	147	Z	FD loc	0.34295
565	spintaterra	148	Z	FD loc	0.39405
566	spintaterra	149	Z	FD loc	0.34295
567	spintaterra	150	Z	FD loc	0.39405
568	spintaterra	151	Z	FD loc	0.34295
569	spintaterra	152	Z	FD loc	0.39405
570	spintaterra	153	Z	FD loc	0.34295
571	spintaterra	154	Z	FD loc	0.39405
572	spintaterra	155	Z	FD loc	0.34295
573	spintaterra	156	Z	FD loc	0.39405
574	spintaterra	157	Z	FD loc	0.34295
575	spintaterra	158	Z	FD loc	0.39405
576	spintaterra	159	Z	FD loc	0.34295
577	spintaterra	161	Z	FD loc	0.34295
578	spintaterra	162	Z	FD loc	0.39405
579	spintaterra	199	Z	FD loc	0.40257
580	spintaterra	200	Z	FD loc	0.38553
581	spintaterra	201	Z	FD loc	0.40257
582	spintaterra	202	Z	FD loc	0.40257
583	spintaterra	203	Z	FD loc	0.38553
584	spintaterra	204	Z	FD loc	0.40257
585	spintaterra	93	Z	FD loc	0.12014
586	spintaterra	95	Z	FD loc	0.11901

587	spintaterra	109	Z	FD loc	0.11901
588	spintaterra	111	Z	FD loc	0.12014
589	spintaterra	1	Z	FD loc	0.02826
590	spintaterra	3	Z	FD loc	0.02826
591	spintaterra	5	Z	FD loc	0.02826
592	spintaterra	6	Z	FD loc	0.07399
593	spintaterra	7	Z	FD loc	0.02826
594	spintaterra	8	Z	FD loc	0.07399
595	spintaterra	9	Z	FD loc	0.02826
596	spintaterra	10	Z	FD loc	0.07399
597	spintaterra	11	Z	FD loc	0.02826
598	spintaterra	12	Z	FD loc	0.07399
599	spintaterra	13	Z	FD loc	0.02826
600	spintaterra	14	Z	FD loc	0.07399
601	spintaterra	15	Z	FD loc	0.02826
602	spintaterra	16	Z	FD loc	0.07399
603	spintaterra	17	Z	FD loc	0.02826
604	spintaterra	19	Z	FD loc	0.02826
605	spintaterra	21	Z	FD loc	0.08923
606	spintaterra	22	Z	FD loc	0.07907
607	spintaterra	23	Z	FD loc	0.06038
608	spintaterra	24	Z	FD loc	0.08542
609	spintaterra	25	Z	FD loc	0.07017
610	spintaterra	26	Z	FD loc	0.03461
611	spintaterra	27	Z	FD loc	0.08923
612	spintaterra	28	Z	FD loc	0.07907
613	spintaterra	29	Z	FD loc	0.06038
614	spintaterra	30	Z	FD loc	0.08542
615	spintaterra	31	Z	FD loc	0.07017
616	spintaterra	32	Z	FD loc	0.03461
617	spintaterra	2	Z	FD loc	0.07337
618	spintaterra	4	Z	FD loc	0.07451
619	spintaterra	18	Z	FD loc	0.07451
620	spintaterra	20	Z	FD loc	0.07337
621	spintaterra	63	Z	FD loc	0.16489
622	spintaterra	64	Z	FD loc	0.11952
623	spintaterra	65	Z	FD loc	0.16489
624	spintaterra	66	Z	FD loc	0.11952
625	spintaterra	67	Z	FD loc	0.16489
626	spintaterra	68	Z	FD loc	0.11952
627	spintaterra	69	Z	FD loc	0.18002
628	spintaterra	70	Z	FD loc	0.16994
629	spintaterra	71	Z	FD loc	0.15139
630	spintaterra	72	Z	FD loc	0.17624
631	spintaterra	73	Z	FD loc	0.16112
632	spintaterra	74	Z	FD loc	0.12583
633	spintaterra	75	Z	FD loc	0.20922
634	spintaterra	76	Z	FD loc	0.25249
635	spintaterra	77	Z	FD loc	0.29576
636	spintaterra	78	Z	FD loc	0.20922
637	spintaterra	79	Z	FD loc	0.25249
638	spintaterra	80	Z	FD loc	0.29576
639	spintaterra	81	Z	FD loc	0.20922
640	spintaterra	82	Z	FD loc	0.25249
641	spintaterra	83	Z	FD loc	0.29576
642	spintaterra	84	Z	FD loc	0.20922
643	spintaterra	85	Z	FD loc	0.25249
644	spintaterra	86	Z	FD loc	0.29576
645	spintaterra	87	Z	FD loc	0.20922
646	spintaterra	88	Z	FD loc	0.25249
647	spintaterra	89	Z	FD loc	0.29576
648	spintaterra	90	Z	FD loc	0.20922
649	spintaterra	91	Z	FD loc	0.25249
650	spintaterra	92	Z	FD loc	0.29576
651	spintaterra	33	Z	FD loc	0.16489
652	spintaterra	34	Z	FD loc	0.11952
653	spintaterra	35	Z	FD loc	0.16489

654	spintaterra	36	Z	FD loc	0.11952
655	spintaterra	37	Z	FD loc	0.16489
656	spintaterra	38	Z	FD loc	0.11952
657	spintaterra	39	Z	FD loc	0.18002
658	spintaterra	40	Z	FD loc	0.16994
659	spintaterra	41	Z	FD loc	0.15139
660	spintaterra	42	Z	FD loc	0.17624
661	spintaterra	43	Z	FD loc	0.16112
662	spintaterra	44	Z	FD loc	0.12583
663	spintaterra	45	Z	FD loc	0.20922
664	spintaterra	46	Z	FD loc	0.25249
665	spintaterra	47	Z	FD loc	0.29576
666	spintaterra	48	Z	FD loc	0.20922
667	spintaterra	49	Z	FD loc	0.25249
668	spintaterra	50	Z	FD loc	0.29576
669	spintaterra	51	Z	FD loc	0.20922
670	spintaterra	52	Z	FD loc	0.25249
671	spintaterra	53	Z	FD loc	0.29576
672	spintaterra	54	Z	FD loc	0.20922
673	spintaterra	55	Z	FD loc	0.25249
674	spintaterra	56	Z	FD loc	0.29576
675	spintaterra	57	Z	FD loc	0.20922
676	spintaterra	58	Z	FD loc	0.25249
677	spintaterra	59	Z	FD loc	0.29576
678	spintaterra	60	Z	FD loc	0.20922
679	spintaterra	61	Z	FD loc	0.25249
680	spintaterra	62	Z	FD loc	0.29576
681	sovraspintasismica	205	Z	FD loc	0.09000
682	sovraspintasismica	206	Z	FD loc	0.09000
683	sovraspintasismica	207	Z	FD loc	0.09000
684	sovraspintasismica	208	Z	FD loc	0.09000
685	sovraspintasismica	209	Z	FD loc	0.09000
686	sovraspintasismica	210	Z	FD loc	0.09000
687	sovraspintasismica	211	Z	FD loc	0.09000
688	sovraspintasismica	212	Z	FD loc	0.09000
689	sovraspintasismica	213	Z	FD loc	0.09000
690	sovraspintasismica	214	Z	FD loc	0.09000
691	sovraspintasismica	215	Z	FD loc	0.09000
692	sovraspintasismica	216	Z	FD loc	0.09000
693	sovraspintasismica	217	Z	FD loc	0.09000
694	sovraspintasismica	218	Z	FD loc	0.09000
695	sovraspintasismica	219	Z	FD loc	0.09000
696	sovraspintasismica	220	Z	FD loc	0.09000
697	sovraspintasismica	221	Z	FD loc	0.09000
698	sovraspintasismica	222	Z	FD loc	0.09000
699	sovraspintasismica	223	Z	FD loc	0.09000
700	sovraspintasismica	224	Z	FD loc	0.09000
701	sovraspintasismica	225	Z	FD loc	0.09000
702	sovraspintasismica	226	Z	FD loc	0.09000
703	sovraspintasismica	227	Z	FD loc	0.09000
704	sovraspintasismica	228	Z	FD loc	0.09000
705	sovraspintasismica	229	Z	FD loc	0.09000
706	sovraspintasismica	230	Z	FD loc	0.09000
707	sovraspintasismica	231	Z	FD loc	0.09000
708	sovraspintasismica	232	Z	FD loc	0.09000
709	sovraspintasismica	233	Z	FD loc	0.09000
710	sovraspintasismica	234	Z	FD loc	0.09000
711	sovraspintasismica	235	Z	FD loc	0.09000
712	sovraspintasismica	236	Z	FD loc	0.09000
713	sovraspintasismica	237	Z	FD loc	0.09000
714	sovraspintasismica	238	Z	FD loc	0.09000
715	sovraspintasismica	239	Z	FD loc	0.09000
716	sovraspintasismica	240	Z	FD loc	0.09000
717	sovraspintasismica	241	Z	FD loc	0.09000
718	sovraspintasismica	242	Z	FD loc	0.09000
719	sovraspintasismica	243	Z	FD loc	0.09000
720	sovraspintasismica	244	Z	FD loc	0.09000

721	sovraspintasismica	245	Z	FD loc	0.09000
722	sovraspintasismica	246	Z	FD loc	0.09000
723	sovraspintasismica	247	Z	FD loc	0.09000
724	sovraspintasismica	248	Z	FD loc	0.09000
725	sovraspintasismica	249	Z	FD loc	0.09000
726	sovraspintasismica	250	Z	FD loc	0.09000
727	sovraspintasismica	251	Z	FD loc	0.09000
728	sovraspintasismica	252	Z	FD loc	0.09000
729	sovraspintasismica	253	Z	FD loc	0.09000
730	sovraspintasismica	254	Z	FD loc	0.09000
731	sovraspintasismica	255	Z	FD loc	0.09000
732	sovraspintasismica	256	Z	FD loc	0.09000
733	sovraspintasismica	257	Z	FD loc	0.09000
734	sovraspintasismica	258	Z	FD loc	0.09000
735	sovraspintasismica	259	Z	FD loc	0.09000
736	sovraspintasismica	260	Z	FD loc	0.09000
737	sovraspintasismica	261	Z	FD loc	0.09000
738	sovraspintasismica	262	Z	FD loc	0.09000
739	sovraspintasismica	263	Z	FD loc	0.09000
740	sovraspintasismica	264	Z	FD loc	0.09000
741	sovraspintasismica	265	Z	FD loc	0.09000
742	sovraspintasismica	266	Z	FD loc	0.09000
743	sovraspintasismica	267	Z	FD loc	0.09000
744	sovraspintasismica	268	Z	FD loc	0.09000
745	sovraspintasismica	293	Z	FD loc	0.09000
746	sovraspintasismica	294	Z	FD loc	0.09000
747	sovraspintasismica	295	Z	FD loc	0.09000
748	sovraspintasismica	296	Z	FD loc	0.09000
749	sovraspintasismica	297	Z	FD loc	0.09000
750	sovraspintasismica	298	Z	FD loc	0.09000
751	sovraspintasismica	299	Z	FD loc	0.09000
752	sovraspintasismica	300	Z	FD loc	0.09000
753	sovraspintasismica	301	Z	FD loc	0.09000
754	sovraspintasismica	302	Z	FD loc	0.09000
755	sovraspintasismica	303	Z	FD loc	0.09000
756	sovraspintasismica	304	Z	FD loc	0.09000
757	sovraspintasismica	305	Z	FD loc	0.09000
758	sovraspintasismica	306	Z	FD loc	0.09000
759	sovraspintasismica	307	Z	FD loc	0.09000
760	sovraspintasismica	308	Z	FD loc	0.09000
761	sovraspintasismica	309	Z	FD loc	0.09000
762	sovraspintasismica	310	Z	FD loc	0.09000
763	sovraspintasismica	311	Z	FD loc	0.09000
764	sovraspintasismica	312	Z	FD loc	0.09000
765	sovraspintasismica	313	Z	FD loc	0.09000
766	sovraspintasismica	314	Z	FD loc	0.09000
767	sovraspintasismica	315	Z	FD loc	0.09000
768	sovraspintasismica	316	Z	FD loc	0.09000
769	sovraspintasismica	317	Z	FD loc	0.09000
770	sovraspintasismica	318	Z	FD loc	0.09000
771	sovraspintasismica	319	Z	FD loc	0.09000
772	sovraspintasismica	320	Z	FD loc	0.09000
773	sovraspintasismica	321	Z	FD loc	0.09000
774	sovraspintasismica	322	Z	FD loc	0.09000
775	sovraspintasismica	323	Z	FD loc	0.09000
776	sovraspintasismica	324	Z	FD loc	0.09000
777	sovraspintasismica	325	Z	FD loc	0.09000
778	sovraspintasismica	326	Z	FD loc	0.09000
779	sovraspintasismica	327	Z	FD loc	0.09000
780	sovraspintasismica	328	Z	FD loc	0.09000
781	sovraspintasismica	329	Z	FD loc	0.09000
782	sovraspintasismica	330	Z	FD loc	0.09000
783	sovraspintasismica	331	Z	FD loc	0.09000
784	sovraspintasismica	332	Z	FD loc	0.09000
785	sovraspintasismica	333	Z	FD loc	0.09000
786	sovraspintasismica	334	Z	FD loc	0.09000
787	sovraspintasismica	335	Z	FD loc	0.09000

788	sovraspintasismica	336	Z	FD loc	0.09000
789	sovraspintasismica	337	Z	FD loc	0.09000
790	sovraspintasismica	338	Z	FD loc	0.09000
791	sovraspintasismica	339	Z	FD loc	0.09000
792	sovraspintasismica	340	Z	FD loc	0.09000
793	sovraspintasismica	341	Z	FD loc	0.09000
794	sovraspintasismica	342	Z	FD loc	0.09000
795	sovraspintasismica	343	Z	FD loc	0.09000
796	sovraspintasismica	344	Z	FD loc	0.09000
797	sovraspintasismica	345	Z	FD loc	0.09000
798	sovraspintasismica	346	Z	FD loc	0.09000
799	sovraspintasismica	347	Z	FD loc	0.09000
800	sovraspintasismica	348	Z	FD loc	0.09000
801	sovraspintasismica	349	Z	FD loc	0.09000
802	sovraspintasismica	350	Z	FD loc	0.09000
803	sovraspintasismica	351	Z	FD loc	0.09000
804	sovraspintasismica	352	Z	FD loc	0.09000
805	sovraspintasismica	353	Z	FD loc	0.09000
806	sovraspintasismica	354	Z	FD loc	0.09000
807	sovraspintasismica	355	Z	FD loc	0.09000
808	sovraspintasismica	356	Z	FD loc	0.09000
809	sovraspintasismica	357	Z	FD loc	0.09000
810	sovraspintasismica	358	Z	FD loc	0.09000
811	sovraspintasismica	359	Z	FD loc	0.09000
812	sovraspintasismica	360	Z	FD loc	0.09000
813	sovraspintasismica	361	Z	FD loc	0.09000
814	sovraspintasismica	362	Z	FD loc	0.09000
815	sovraspintasismica	363	Z	FD loc	0.09000
816	sovraspintasismica	364	Z	FD loc	0.09000
817	sovraspintasismica	365	Z	FD loc	0.09000
818	sovraspintasismica	366	Z	FD loc	0.09000
819	sovraspintasismica	367	Z	FD loc	0.09000
820	sovraspintasismica	368	Z	FD loc	0.09000
821	sovraspintasismica	369	Z	FD loc	0.09000
822	sovraspintasismica	370	Z	FD loc	0.09000
823	sovraspintasismica	371	Z	FD loc	0.09000
824	sovraspintasismica	372	Z	FD loc	0.09000
825	sovraspintasismica	373	Z	FD loc	0.09000
826	sovraspintasismica	374	Z	FD loc	0.09000
827	sovraspintasismica	375	Z	FD loc	0.09000
828	sovraspintasismica	376	Z	FD loc	0.09000
829	sovraspintasismica	377	Z	FD loc	0.09000
830	sovraspintasismica	378	Z	FD loc	0.09000
831	sovraspintasismica	379	Z	FD loc	0.09000
832	sovraspintasismica	380	Z	FD loc	0.09000
833	sovraspintasismica	381	Z	FD loc	0.09000
834	sovraspintasismica	382	Z	FD loc	0.09000
835	sovraspintasismica	383	Z	FD loc	0.09000
836	sovraspintasismica	384	Z	FD loc	0.09000
837	sovraspintasismica	385	Z	FD loc	0.09000
838	sovraspintasismica	386	Z	FD loc	0.09000
839	sovraspintasismica	387	Z	FD loc	0.09000
840	sovraspintasismica	388	Z	FD loc	0.09000
841	sovraspintasismica	389	Z	FD loc	0.09000
842	sovraspintasismica	390	Z	FD loc	0.09000
843	sovraspintasismica	391	Z	FD loc	0.09000
844	sovraspintasismica	392	Z	FD loc	0.09000
845	sovraspintasismica	393	Z	FD loc	0.09000
846	sovraspintasismica	394	Z	FD loc	0.09000
847	sovraspintasismica	94	Z	FD loc	0.09000
848	sovraspintasismica	96	Z	FD loc	0.09000
849	sovraspintasismica	97	Z	FD loc	0.09000
850	sovraspintasismica	98	Z	FD loc	0.09000
851	sovraspintasismica	99	Z	FD loc	0.09000
852	sovraspintasismica	100	Z	FD loc	0.09000
853	sovraspintasismica	101	Z	FD loc	0.09000
854	sovraspintasismica	102	Z	FD loc	0.09000

855	sovraspintasismica	103	Z	FD loc	0.09000
856	sovraspintasismica	104	Z	FD loc	0.09000
857	sovraspintasismica	105	Z	FD loc	0.09000
858	sovraspintasismica	106	Z	FD loc	0.09000
859	sovraspintasismica	107	Z	FD loc	0.09000
860	sovraspintasismica	108	Z	FD loc	0.09000
861	sovraspintasismica	110	Z	FD loc	0.09000
862	sovraspintasismica	112	Z	FD loc	0.09000
863	sovraspintasismica	113	Z	FD loc	0.09000
864	sovraspintasismica	114	Z	FD loc	0.09000
865	sovraspintasismica	115	Z	FD loc	0.09000
866	sovraspintasismica	116	Z	FD loc	0.09000
867	sovraspintasismica	117	Z	FD loc	0.09000
868	sovraspintasismica	118	Z	FD loc	0.09000
869	sovraspintasismica	119	Z	FD loc	0.09000
870	sovraspintasismica	120	Z	FD loc	0.09000
871	sovraspintasismica	121	Z	FD loc	0.09000
872	sovraspintasismica	122	Z	FD loc	0.09000
873	sovraspintasismica	123	Z	FD loc	0.09000
874	sovraspintasismica	124	Z	FD loc	0.09000
875	sovraspintasismica	125	Z	FD loc	0.09000
876	sovraspintasismica	126	Z	FD loc	0.09000
877	sovraspintasismica	127	Z	FD loc	0.09000
878	sovraspintasismica	128	Z	FD loc	0.09000
879	sovraspintasismica	129	Z	FD loc	0.09000
880	sovraspintasismica	130	Z	FD loc	0.09000
881	sovraspintasismica	131	Z	FD loc	0.09000
882	sovraspintasismica	132	Z	FD loc	0.09000
883	sovraspintasismica	133	Z	FD loc	0.09000
884	sovraspintasismica	134	Z	FD loc	0.09000
885	sovraspintasismica	135	Z	FD loc	0.09000
886	sovraspintasismica	136	Z	FD loc	0.09000
887	sovraspintasismica	137	Z	FD loc	0.09000
888	sovraspintasismica	138	Z	FD loc	0.09000
889	sovraspintasismica	139	Z	FD loc	0.09000
890	sovraspintasismica	140	Z	FD loc	0.09000
891	sovraspintasismica	141	Z	FD loc	0.09000
892	sovraspintasismica	142	Z	FD loc	0.09000
893	sovraspintasismica	143	Z	FD loc	0.09000
894	sovraspintasismica	144	Z	FD loc	0.09000
895	sovraspintasismica	145	Z	FD loc	0.09000
896	sovraspintasismica	147	Z	FD loc	0.09000
897	sovraspintasismica	148	Z	FD loc	0.09000
898	sovraspintasismica	149	Z	FD loc	0.09000
899	sovraspintasismica	150	Z	FD loc	0.09000
900	sovraspintasismica	151	Z	FD loc	0.09000
901	sovraspintasismica	152	Z	FD loc	0.09000
902	sovraspintasismica	153	Z	FD loc	0.09000
903	sovraspintasismica	154	Z	FD loc	0.09000
904	sovraspintasismica	155	Z	FD loc	0.09000
905	sovraspintasismica	156	Z	FD loc	0.09000
906	sovraspintasismica	157	Z	FD loc	0.09000
907	sovraspintasismica	158	Z	FD loc	0.09000
908	sovraspintasismica	159	Z	FD loc	0.09000
909	sovraspintasismica	161	Z	FD loc	0.09000
910	sovraspintasismica	162	Z	FD loc	0.09000
911	sovraspintasismica	199	Z	FD loc	0.09000
912	sovraspintasismica	200	Z	FD loc	0.09000
913	sovraspintasismica	201	Z	FD loc	0.09000
914	sovraspintasismica	202	Z	FD loc	0.09000
915	sovraspintasismica	203	Z	FD loc	0.09000
916	sovraspintasismica	204	Z	FD loc	0.09000
917	sovraspintasismica	93	Z	FD loc	0.09000
918	sovraspintasismica	95	Z	FD loc	0.09000
919	sovraspintasismica	109	Z	FD loc	0.09000
920	sovraspintasismica	111	Z	FD loc	0.09000
921	sovraspintasismica	1	Z	FD loc	0.09000

922	sovraspintasismica	3	Z	FD loc	0.09000
923	sovraspintasismica	5	Z	FD loc	0.09000
924	sovraspintasismica	6	Z	FD loc	0.09000
925	sovraspintasismica	7	Z	FD loc	0.09000
926	sovraspintasismica	8	Z	FD loc	0.09000
927	sovraspintasismica	9	Z	FD loc	0.09000
928	sovraspintasismica	10	Z	FD loc	0.09000
929	sovraspintasismica	11	Z	FD loc	0.09000
930	sovraspintasismica	12	Z	FD loc	0.09000
931	sovraspintasismica	13	Z	FD loc	0.09000
932	sovraspintasismica	14	Z	FD loc	0.09000
933	sovraspintasismica	15	Z	FD loc	0.09000
934	sovraspintasismica	16	Z	FD loc	0.09000
935	sovraspintasismica	17	Z	FD loc	0.09000
936	sovraspintasismica	19	Z	FD loc	0.09000
937	sovraspintasismica	21	Z	FD loc	0.09000
938	sovraspintasismica	22	Z	FD loc	0.09000
939	sovraspintasismica	23	Z	FD loc	0.09000
940	sovraspintasismica	24	Z	FD loc	0.09000
941	sovraspintasismica	25	Z	FD loc	0.09000
942	sovraspintasismica	26	Z	FD loc	0.09000
943	sovraspintasismica	27	Z	FD loc	0.09000
944	sovraspintasismica	28	Z	FD loc	0.09000
945	sovraspintasismica	29	Z	FD loc	0.09000
946	sovraspintasismica	30	Z	FD loc	0.09000
947	sovraspintasismica	31	Z	FD loc	0.09000
948	sovraspintasismica	32	Z	FD loc	0.09000
949	sovraspintasismica	2	Z	FD loc	0.09000
950	sovraspintasismica	4	Z	FD loc	0.09000
951	sovraspintasismica	18	Z	FD loc	0.09000
952	sovraspintasismica	20	Z	FD loc	0.09000
953	sovraspintasismica	63	Z	FD loc	0.09000
954	sovraspintasismica	64	Z	FD loc	0.09000
955	sovraspintasismica	65	Z	FD loc	0.09000
956	sovraspintasismica	66	Z	FD loc	0.09000
957	sovraspintasismica	67	Z	FD loc	0.09000
958	sovraspintasismica	68	Z	FD loc	0.09000
959	sovraspintasismica	69	Z	FD loc	0.09000
960	sovraspintasismica	70	Z	FD loc	0.09000
961	sovraspintasismica	71	Z	FD loc	0.09000
962	sovraspintasismica	72	Z	FD loc	0.09000
963	sovraspintasismica	73	Z	FD loc	0.09000
964	sovraspintasismica	74	Z	FD loc	0.09000
965	sovraspintasismica	75	Z	FD loc	0.09000
966	sovraspintasismica	76	Z	FD loc	0.09000
967	sovraspintasismica	77	Z	FD loc	0.09000
968	sovraspintasismica	78	Z	FD loc	0.09000
969	sovraspintasismica	79	Z	FD loc	0.09000
970	sovraspintasismica	80	Z	FD loc	0.09000
971	sovraspintasismica	81	Z	FD loc	0.09000
972	sovraspintasismica	82	Z	FD loc	0.09000
973	sovraspintasismica	83	Z	FD loc	0.09000
974	sovraspintasismica	84	Z	FD loc	0.09000
975	sovraspintasismica	85	Z	FD loc	0.09000
976	sovraspintasismica	86	Z	FD loc	0.09000
977	sovraspintasismica	87	Z	FD loc	0.09000
978	sovraspintasismica	88	Z	FD loc	0.09000
979	sovraspintasismica	89	Z	FD loc	0.09000
980	sovraspintasismica	90	Z	FD loc	0.09000
981	sovraspintasismica	91	Z	FD loc	0.09000
982	sovraspintasismica	92	Z	FD loc	0.09000
983	sovraspintasismica	33	Z	FD loc	0.09000
984	sovraspintasismica	34	Z	FD loc	0.09000
985	sovraspintasismica	35	Z	FD loc	0.09000
986	sovraspintasismica	36	Z	FD loc	0.09000
987	sovraspintasismica	37	Z	FD loc	0.09000
988	sovraspintasismica	38	Z	FD loc	0.09000

989	sovraspintasismica	39	Z	FD loc	0.09000
990	sovraspintasismica	40	Z	FD loc	0.09000
991	sovraspintasismica	41	Z	FD loc	0.09000
992	sovraspintasismica	42	Z	FD loc	0.09000
993	sovraspintasismica	43	Z	FD loc	0.09000
994	sovraspintasismica	44	Z	FD loc	0.09000
995	sovraspintasismica	45	Z	FD loc	0.09000
996	sovraspintasismica	46	Z	FD loc	0.09000
997	sovraspintasismica	47	Z	FD loc	0.09000
998	sovraspintasismica	48	Z	FD loc	0.09000
999	sovraspintasismica	49	Z	FD loc	0.09000
1000	sovraspintasismica	50	Z	FD loc	0.09000
1001	sovraspintasismica	51	Z	FD loc	0.09000
1002	sovraspintasismica	52	Z	FD loc	0.09000
1003	sovraspintasismica	53	Z	FD loc	0.09000
1004	sovraspintasismica	54	Z	FD loc	0.09000
1005	sovraspintasismica	55	Z	FD loc	0.09000
1006	sovraspintasismica	56	Z	FD loc	0.09000
1007	sovraspintasismica	57	Z	FD loc	0.09000
1008	sovraspintasismica	58	Z	FD loc	0.09000
1009	sovraspintasismica	59	Z	FD loc	0.09000
1010	sovraspintasismica	60	Z	FD loc	0.09000
1011	sovraspintasismica	61	Z	FD loc	0.09000
1012	sovraspintasismica	62	Z	FD loc	0.09000
1013	spintafolla	205	Z	FD loc	0.01350
1014	spintafolla	206	Z	FD loc	0.01350
1015	spintafolla	207	Z	FD loc	0.01350
1016	spintafolla	208	Z	FD loc	0.01350
1017	spintafolla	209	Z	FD loc	0.01350
1018	spintafolla	210	Z	FD loc	0.01350
1019	spintafolla	211	Z	FD loc	0.01350
1020	spintafolla	212	Z	FD loc	0.01350
1021	spintafolla	213	Z	FD loc	0.01350
1022	spintafolla	214	Z	FD loc	0.01350
1023	spintafolla	215	Z	FD loc	0.01350
1024	spintafolla	216	Z	FD loc	0.01350
1025	spintafolla	217	Z	FD loc	0.01350
1026	spintafolla	218	Z	FD loc	0.01350
1027	spintafolla	219	Z	FD loc	0.01350
1028	spintafolla	220	Z	FD loc	0.01350
1029	spintafolla	221	Z	FD loc	0.01350
1030	spintafolla	222	Z	FD loc	0.01350
1031	spintafolla	223	Z	FD loc	0.01350
1032	spintafolla	224	Z	FD loc	0.01350
1033	spintafolla	225	Z	FD loc	0.01350
1034	spintafolla	226	Z	FD loc	0.01350
1035	spintafolla	227	Z	FD loc	0.01350
1036	spintafolla	228	Z	FD loc	0.01350
1037	spintafolla	229	Z	FD loc	0.01350
1038	spintafolla	230	Z	FD loc	0.01350
1039	spintafolla	231	Z	FD loc	0.01350
1040	spintafolla	232	Z	FD loc	0.01350
1041	spintafolla	233	Z	FD loc	0.01350
1042	spintafolla	234	Z	FD loc	0.01350
1043	spintafolla	235	Z	FD loc	0.01350
1044	spintafolla	236	Z	FD loc	0.01350
1045	spintafolla	237	Z	FD loc	0.01350
1046	spintafolla	238	Z	FD loc	0.01350
1047	spintafolla	239	Z	FD loc	0.01350
1048	spintafolla	240	Z	FD loc	0.01350
1049	spintafolla	241	Z	FD loc	0.01350
1050	spintafolla	242	Z	FD loc	0.01350
1051	spintafolla	243	Z	FD loc	0.01350
1052	spintafolla	244	Z	FD loc	0.01350
1053	spintafolla	245	Z	FD loc	0.01350
1054	spintafolla	246	Z	FD loc	0.01350
1055	spintafolla	247	Z	FD loc	0.01350

1056	spintafolla	248	Z	FD loc	0.01350
1057	spintafolla	249	Z	FD loc	0.01350
1058	spintafolla	250	Z	FD loc	0.01350
1059	spintafolla	251	Z	FD loc	0.01350
1060	spintafolla	252	Z	FD loc	0.01350
1061	spintafolla	253	Z	FD loc	0.01350
1062	spintafolla	254	Z	FD loc	0.01350
1063	spintafolla	255	Z	FD loc	0.01350
1064	spintafolla	256	Z	FD loc	0.01350
1065	spintafolla	257	Z	FD loc	0.01350
1066	spintafolla	258	Z	FD loc	0.01350
1067	spintafolla	259	Z	FD loc	0.01350
1068	spintafolla	260	Z	FD loc	0.01350
1069	spintafolla	261	Z	FD loc	0.01350
1070	spintafolla	262	Z	FD loc	0.01350
1071	spintafolla	263	Z	FD loc	0.01350
1072	spintafolla	264	Z	FD loc	0.01350
1073	spintafolla	265	Z	FD loc	0.01350
1074	spintafolla	266	Z	FD loc	0.01350
1075	spintafolla	267	Z	FD loc	0.01350
1076	spintafolla	268	Z	FD loc	0.01350
1077	spintafolla	293	Z	FD loc	0.01350
1078	spintafolla	294	Z	FD loc	0.01350
1079	spintafolla	295	Z	FD loc	0.01350
1080	spintafolla	296	Z	FD loc	0.01350
1081	spintafolla	297	Z	FD loc	0.01350
1082	spintafolla	298	Z	FD loc	0.01350
1083	spintafolla	299	Z	FD loc	0.01350
1084	spintafolla	300	Z	FD loc	0.01350
1085	spintafolla	301	Z	FD loc	0.01350
1086	spintafolla	302	Z	FD loc	0.01350
1087	spintafolla	303	Z	FD loc	0.01350
1088	spintafolla	304	Z	FD loc	0.01350
1089	spintafolla	305	Z	FD loc	0.01350
1090	spintafolla	306	Z	FD loc	0.01350
1091	spintafolla	307	Z	FD loc	0.01350
1092	spintafolla	308	Z	FD loc	0.01350
1093	spintafolla	309	Z	FD loc	0.01350
1094	spintafolla	310	Z	FD loc	0.01350
1095	spintafolla	311	Z	FD loc	0.01350
1096	spintafolla	312	Z	FD loc	0.01350
1097	spintafolla	313	Z	FD loc	0.01350
1098	spintafolla	314	Z	FD loc	0.01350
1099	spintafolla	315	Z	FD loc	0.01350
1100	spintafolla	316	Z	FD loc	0.01350
1101	spintafolla	317	Z	FD loc	0.01350
1102	spintafolla	318	Z	FD loc	0.01350
1103	spintafolla	319	Z	FD loc	0.01350
1104	spintafolla	320	Z	FD loc	0.01350
1105	spintafolla	321	Z	FD loc	0.01350
1106	spintafolla	322	Z	FD loc	0.01350
1107	spintafolla	323	Z	FD loc	0.01350
1108	spintafolla	324	Z	FD loc	0.01350
1109	spintafolla	325	Z	FD loc	0.01350
1110	spintafolla	326	Z	FD loc	0.01350
1111	spintafolla	327	Z	FD loc	0.01350
1112	spintafolla	328	Z	FD loc	0.01350
1113	spintafolla	329	Z	FD loc	0.01350
1114	spintafolla	330	Z	FD loc	0.01350
1115	spintafolla	331	Z	FD loc	0.01350
1116	spintafolla	332	Z	FD loc	0.01350
1117	spintafolla	333	Z	FD loc	0.01350
1118	spintafolla	334	Z	FD loc	0.01350
1119	spintafolla	335	Z	FD loc	0.01350
1120	spintafolla	336	Z	FD loc	0.01350
1121	spintafolla	337	Z	FD loc	0.01350
1122	spintafolla	338	Z	FD loc	0.01350

1123	spintafolla	339	Z	FD loc	0.01350
1124	spintafolla	340	Z	FD loc	0.01350
1125	spintafolla	341	Z	FD loc	0.01350
1126	spintafolla	342	Z	FD loc	0.01350
1127	spintafolla	343	Z	FD loc	0.01350
1128	spintafolla	344	Z	FD loc	0.01350
1129	spintafolla	345	Z	FD loc	0.01350
1130	spintafolla	346	Z	FD loc	0.01350
1131	spintafolla	347	Z	FD loc	0.01350
1132	spintafolla	348	Z	FD loc	0.01350
1133	spintafolla	349	Z	FD loc	0.01350
1134	spintafolla	350	Z	FD loc	0.01350
1135	spintafolla	351	Z	FD loc	0.01350
1136	spintafolla	352	Z	FD loc	0.01350
1137	spintafolla	353	Z	FD loc	0.01350
1138	spintafolla	354	Z	FD loc	0.01350
1139	spintafolla	355	Z	FD loc	0.01350
1140	spintafolla	356	Z	FD loc	0.01350
1141	spintafolla	357	Z	FD loc	0.01350
1142	spintafolla	358	Z	FD loc	0.01350
1143	spintafolla	359	Z	FD loc	0.01350
1144	spintafolla	360	Z	FD loc	0.01350
1145	spintafolla	361	Z	FD loc	0.01350
1146	spintafolla	362	Z	FD loc	0.01350
1147	spintafolla	363	Z	FD loc	0.01350
1148	spintafolla	364	Z	FD loc	0.01350
1149	spintafolla	365	Z	FD loc	0.01350
1150	spintafolla	366	Z	FD loc	0.01350
1151	spintafolla	367	Z	FD loc	0.01350
1152	spintafolla	368	Z	FD loc	0.01350
1153	spintafolla	369	Z	FD loc	0.01350
1154	spintafolla	370	Z	FD loc	0.01350
1155	spintafolla	371	Z	FD loc	0.01350
1156	spintafolla	372	Z	FD loc	0.01350
1157	spintafolla	373	Z	FD loc	0.01350
1158	spintafolla	374	Z	FD loc	0.01350
1159	spintafolla	375	Z	FD loc	0.01350
1160	spintafolla	376	Z	FD loc	0.01350
1161	spintafolla	377	Z	FD loc	0.01350
1162	spintafolla	378	Z	FD loc	0.01350
1163	spintafolla	379	Z	FD loc	0.01350
1164	spintafolla	380	Z	FD loc	0.01350
1165	spintafolla	381	Z	FD loc	0.01350
1166	spintafolla	382	Z	FD loc	0.01350
1167	spintafolla	383	Z	FD loc	0.01350
1168	spintafolla	384	Z	FD loc	0.01350
1169	spintafolla	385	Z	FD loc	0.01350
1170	spintafolla	386	Z	FD loc	0.01350
1171	spintafolla	387	Z	FD loc	0.01350
1172	spintafolla	388	Z	FD loc	0.01350
1173	spintafolla	389	Z	FD loc	0.01350
1174	spintafolla	390	Z	FD loc	0.01350
1175	spintafolla	391	Z	FD loc	0.01350
1176	spintafolla	392	Z	FD loc	0.01350
1177	spintafolla	393	Z	FD loc	0.01350
1178	spintafolla	394	Z	FD loc	0.01350
1179	spintafolla	94	Z	FD loc	0.01350
1180	spintafolla	96	Z	FD loc	0.01350
1181	spintafolla	97	Z	FD loc	0.01350
1182	spintafolla	98	Z	FD loc	0.01350
1183	spintafolla	99	Z	FD loc	0.01350
1184	spintafolla	100	Z	FD loc	0.01350
1185	spintafolla	101	Z	FD loc	0.01350
1186	spintafolla	102	Z	FD loc	0.01350
1187	spintafolla	103	Z	FD loc	0.01350
1188	spintafolla	104	Z	FD loc	0.01350
1189	spintafolla	105	Z	FD loc	0.01350

1190	spintafolla	106	Z	FD loc	0.01350
1191	spintafolla	107	Z	FD loc	0.01350
1192	spintafolla	108	Z	FD loc	0.01350
1193	spintafolla	110	Z	FD loc	0.01350
1194	spintafolla	112	Z	FD loc	0.01350
1195	spintafolla	113	Z	FD loc	0.01350
1196	spintafolla	114	Z	FD loc	0.01350
1197	spintafolla	115	Z	FD loc	0.01350
1198	spintafolla	116	Z	FD loc	0.01350
1199	spintafolla	117	Z	FD loc	0.01350
1200	spintafolla	118	Z	FD loc	0.01350
1201	spintafolla	119	Z	FD loc	0.01350
1202	spintafolla	120	Z	FD loc	0.01350
1203	spintafolla	121	Z	FD loc	0.01350
1204	spintafolla	122	Z	FD loc	0.01350
1205	spintafolla	123	Z	FD loc	0.01350
1206	spintafolla	124	Z	FD loc	0.01350
1207	spintafolla	125	Z	FD loc	0.01350
1208	spintafolla	126	Z	FD loc	0.01350
1209	spintafolla	127	Z	FD loc	0.01350
1210	spintafolla	128	Z	FD loc	0.01350
1211	spintafolla	129	Z	FD loc	0.01350
1212	spintafolla	130	Z	FD loc	0.01350
1213	spintafolla	131	Z	FD loc	0.01350
1214	spintafolla	132	Z	FD loc	0.01350
1215	spintafolla	133	Z	FD loc	0.01350
1216	spintafolla	134	Z	FD loc	0.01350
1217	spintafolla	135	Z	FD loc	0.01350
1218	spintafolla	136	Z	FD loc	0.01350
1219	spintafolla	137	Z	FD loc	0.01350
1220	spintafolla	138	Z	FD loc	0.01350
1221	spintafolla	139	Z	FD loc	0.01350
1222	spintafolla	140	Z	FD loc	0.01350
1223	spintafolla	141	Z	FD loc	0.01350
1224	spintafolla	142	Z	FD loc	0.01350
1225	spintafolla	143	Z	FD loc	0.01350
1226	spintafolla	144	Z	FD loc	0.01350
1227	spintafolla	145	Z	FD loc	0.01350
1228	spintafolla	147	Z	FD loc	0.01350
1229	spintafolla	148	Z	FD loc	0.01350
1230	spintafolla	149	Z	FD loc	0.01350
1231	spintafolla	150	Z	FD loc	0.01350
1232	spintafolla	151	Z	FD loc	0.01350
1233	spintafolla	152	Z	FD loc	0.01350
1234	spintafolla	153	Z	FD loc	0.01350
1235	spintafolla	154	Z	FD loc	0.01350
1236	spintafolla	155	Z	FD loc	0.01350
1237	spintafolla	156	Z	FD loc	0.01350
1238	spintafolla	157	Z	FD loc	0.01350
1239	spintafolla	158	Z	FD loc	0.01350
1240	spintafolla	159	Z	FD loc	0.01350
1241	spintafolla	161	Z	FD loc	0.01350
1242	spintafolla	162	Z	FD loc	0.01350
1243	spintafolla	199	Z	FD loc	0.01350
1244	spintafolla	200	Z	FD loc	0.01350
1245	spintafolla	201	Z	FD loc	0.01350
1246	spintafolla	202	Z	FD loc	0.01350
1247	spintafolla	203	Z	FD loc	0.01350
1248	spintafolla	204	Z	FD loc	0.01350
1249	spintafolla	93	Z	FD loc	0.01350
1250	spintafolla	95	Z	FD loc	0.01350
1251	spintafolla	109	Z	FD loc	0.01350
1252	spintafolla	111	Z	FD loc	0.01350
1253	spintafolla	1	Z	FD loc	0.01350
1254	spintafolla	3	Z	FD loc	0.01350
1255	spintafolla	5	Z	FD loc	0.01350
1256	spintafolla	6	Z	FD loc	0.01350

1257	spintafolla	7	Z	FD loc	0.01350
1258	spintafolla	8	Z	FD loc	0.01350
1259	spintafolla	9	Z	FD loc	0.01350
1260	spintafolla	10	Z	FD loc	0.01350
1261	spintafolla	11	Z	FD loc	0.01350
1262	spintafolla	12	Z	FD loc	0.01350
1263	spintafolla	13	Z	FD loc	0.01350
1264	spintafolla	14	Z	FD loc	0.01350
1265	spintafolla	15	Z	FD loc	0.01350
1266	spintafolla	16	Z	FD loc	0.01350
1267	spintafolla	17	Z	FD loc	0.01350
1268	spintafolla	19	Z	FD loc	0.01350
1269	spintafolla	21	Z	FD loc	0.01350
1270	spintafolla	22	Z	FD loc	0.01350
1271	spintafolla	23	Z	FD loc	0.01350
1272	spintafolla	24	Z	FD loc	0.01350
1273	spintafolla	25	Z	FD loc	0.01350
1274	spintafolla	26	Z	FD loc	0.01350
1275	spintafolla	27	Z	FD loc	0.01350
1276	spintafolla	28	Z	FD loc	0.01350
1277	spintafolla	29	Z	FD loc	0.01350
1278	spintafolla	30	Z	FD loc	0.01350
1279	spintafolla	31	Z	FD loc	0.01350
1280	spintafolla	32	Z	FD loc	0.01350
1281	spintafolla	2	Z	FD loc	0.01350
1282	spintafolla	4	Z	FD loc	0.01350
1283	spintafolla	18	Z	FD loc	0.01350
1284	spintafolla	20	Z	FD loc	0.01350
1285	spintafolla	63	Z	FD loc	0.01350
1286	spintafolla	64	Z	FD loc	0.01350
1287	spintafolla	65	Z	FD loc	0.01350
1288	spintafolla	66	Z	FD loc	0.01350
1289	spintafolla	67	Z	FD loc	0.01350
1290	spintafolla	68	Z	FD loc	0.01350
1291	spintafolla	69	Z	FD loc	0.01350
1292	spintafolla	70	Z	FD loc	0.01350
1293	spintafolla	71	Z	FD loc	0.01350
1294	spintafolla	72	Z	FD loc	0.01350
1295	spintafolla	73	Z	FD loc	0.01350
1296	spintafolla	74	Z	FD loc	0.01350
1297	spintafolla	75	Z	FD loc	0.01350
1298	spintafolla	76	Z	FD loc	0.01350
1299	spintafolla	77	Z	FD loc	0.01350
1300	spintafolla	78	Z	FD loc	0.01350
1301	spintafolla	79	Z	FD loc	0.01350
1302	spintafolla	80	Z	FD loc	0.01350
1303	spintafolla	81	Z	FD loc	0.01350
1304	spintafolla	82	Z	FD loc	0.01350
1305	spintafolla	83	Z	FD loc	0.01350
1306	spintafolla	84	Z	FD loc	0.01350
1307	spintafolla	85	Z	FD loc	0.01350
1308	spintafolla	86	Z	FD loc	0.01350
1309	spintafolla	87	Z	FD loc	0.01350
1310	spintafolla	88	Z	FD loc	0.01350
1311	spintafolla	89	Z	FD loc	0.01350
1312	spintafolla	90	Z	FD loc	0.01350
1313	spintafolla	91	Z	FD loc	0.01350
1314	spintafolla	92	Z	FD loc	0.01350
1315	spintafolla	33	Z	FD loc	0.01350
1316	spintafolla	34	Z	FD loc	0.01350
1317	spintafolla	35	Z	FD loc	0.01350
1318	spintafolla	36	Z	FD loc	0.01350
1319	spintafolla	37	Z	FD loc	0.01350
1320	spintafolla	38	Z	FD loc	0.01350
1321	spintafolla	39	Z	FD loc	0.01350
1322	spintafolla	40	Z	FD loc	0.01350
1323	spintafolla	41	Z	FD loc	0.01350

1324	spintafolla	42	Z	FD loc	0.01350
1325	spintafolla	43	Z	FD loc	0.01350
1326	spintafolla	44	Z	FD loc	0.01350
1327	spintafolla	45	Z	FD loc	0.01350
1328	spintafolla	46	Z	FD loc	0.01350
1329	spintafolla	47	Z	FD loc	0.01350
1330	spintafolla	48	Z	FD loc	0.01350
1331	spintafolla	49	Z	FD loc	0.01350
1332	spintafolla	50	Z	FD loc	0.01350
1333	spintafolla	51	Z	FD loc	0.01350
1334	spintafolla	52	Z	FD loc	0.01350
1335	spintafolla	53	Z	FD loc	0.01350
1336	spintafolla	54	Z	FD loc	0.01350
1337	spintafolla	55	Z	FD loc	0.01350
1338	spintafolla	56	Z	FD loc	0.01350
1339	spintafolla	57	Z	FD loc	0.01350
1340	spintafolla	58	Z	FD loc	0.01350
1341	spintafolla	59	Z	FD loc	0.01350
1342	spintafolla	60	Z	FD loc	0.01350
1343	spintafolla	61	Z	FD loc	0.01350
1344	spintafolla	62	Z	FD loc	0.01350

PESI PROPRI GUSCI-|-----|-----|-----|-----|-----|
 Cond. Nome Carichi Gusci
 48 1345-1724 1-145, 147-159, 161-162, 175-394

CONDIZIONI DI CARICO-----|-----|-----|-----|num.= 51

Nome		
1	Din_EX+0.3EY+0.3EZ	N. carichi: 7 Lista carichi: 1, 46-47, 133-135, 252
2	Din_EX+0.3EY-0.3EZ	N. carichi: 7 Lista carichi: 2, 48-49, 136-138, 253
3	Din_EX-0.3EY+0.3EZ	N. carichi: 7 Lista carichi: 3, 50-51, 139-141, 254
4	Din_EX-0.3EY+0.3EZ	N. carichi: 7 Lista carichi: 4, 52-53, 142-144, 255
5	Din_-EX+0.3EY+0.3EZ	N. carichi: 7 Lista carichi: 5, 54-55, 145-147, 256
6	Din_-EX+0.3EY-0.3EZ	N. carichi: 7 Lista carichi: 6, 56-57, 148-150, 257
7	Din_-EX-0.3EY+0.3EZ	N. carichi: 7 Lista carichi: 7, 58-59, 151-153, 258
8	Din_0.3EX+EY+0.3EZ	N. carichi: 7 Lista carichi: 8, 60-61, 154-156, 259
9	Din_0.3EX+EY-0.3EZ	N. carichi: 7 Lista carichi: 9, 62-63, 157-159, 260
10	Din_-0.3EX+EY+0.3EZ	N. carichi: 7 Lista carichi: 10, 64-65, 160-162, 261
11	Din_-0.3EX+EY-0.3EZ	N. carichi: 7 Lista carichi: 11, 66-67, 163-165, 262
12	Din_0.3EX-EY+0.3EZ	N. carichi: 7 Lista carichi: 12, 68-69, 166-168, 263
13	Din_0.3EX-EY-0.3EZ	N. carichi: 7 Lista carichi: 13, 70-71, 169-171, 264

14	Din_-0.3EX-EY+0.3EZ	N. carichi:	7
	Lista carichi:	14, 72-73, 172-174, 265	
15	Din_-0.3EX-EY-0.3EZ	N. carichi:	7
	Lista carichi:	15, 74-75, 175-177, 266	
16	Din_0.3EX+0.3EY+EZ	N. carichi:	7
	Lista carichi:	16, 76-77, 178-180, 267	
17	Din_0.3EX+0.3EY+EZ	N. carichi:	7
	Lista carichi:	17, 78-79, 181-183, 268	
18	Din_0.3EX-0.3EY+EZ	N. carichi:	7
	Lista carichi:	18, 80-81, 184-186, 269	
19	Din_-0.3EX+0.3EY+EZ	N. carichi:	7
	Lista carichi:	19, 82-83, 187-189, 270	
20	Din_-0.3EX-0.3EY+EZ	N. carichi:	7
	Lista carichi:	20, 84-85, 190-192, 271	
21	Din_0.3EX+0.3EY-EZ	N. carichi:	7
	Lista carichi:	21, 86-87, 193-195, 272	
22	Din_0.3EX-0.3EY-EZ	N. carichi:	7
	Lista carichi:	22, 88-89, 196-198, 273	
23	Din_-0.3EX+0.3EY-EZ	N. carichi:	7
	Lista carichi:	23, 90-91, 199-201, 274	
24	Din_-0.3EX-0.3EY-EZ	N. carichi:	7
	Lista carichi:	24, 92-93, 202-204, 275	
25	SLU1Stat_solo_Vento	N. carichi:	6
	Lista carichi:	25, 94-95, 205-206, 276	
26	SLU2Stat_Neve_dom	N. carichi:	6
	Lista carichi:	26, 96-97, 207-208, 277	
27	SLU3Stat_Acc_dom	N. carichi:	6
	Lista carichi:	27, 98-99, 209-210, 278	
28	SLU4Stat_Vento_dom	N. carichi:	6
	Lista carichi:	28, 100-101, 211-212, 279	
29	SLU5Stat_socc_POS.1	N. carichi:	7
	Lista carichi:	29, 102-103, 213-215, 280	
30	SLE1Rara_Vento_dom	N. carichi:	6
	Lista carichi:	30, 104-105, 216-217, 281	
31	SLE2Rara_Solo_Vento	N. carichi:	6
	Lista carichi:	31, 106-107, 218-219, 282	
32	SLE3Rara_Acc_dom	N. carichi:	6
	Lista carichi:	32, 108-109, 220-221, 283	
33	SLE4Neve_dom	N. carichi:	6
	Lista carichi:	33, 110-111, 222-223, 284	
34	SLE5Soccorso_POS.1	N. carichi:	7
	Lista carichi:	34, 112-113, 224-226, 285	
35	Cond1Solo_P.P.Strut	N. carichi:	4
	Lista carichi:	35, 114, 227, 286	
36	Cond2Solo_P.P.SolPr	N. carichi:	4

Lista carichi: 36, 115, 228, 287

37 Cond3Solo_Portati-G N. carichi: 4
Lista carichi: 37, 116, 229, 288

38 Cond4Solo_Var_Neve N. carichi: 4
Lista carichi: 38, 117, 230, 289

39 Cond5Solo_Var_Vento N. carichi: 2
Lista carichi: 118, 231

40 Cond6Solo_Var_Folla N. carichi: 4
Lista carichi: 39, 119, 232, 290

41 Cond7Solo_Var_Socc N. carichi: 7
Lista carichi: 40, 120-121, 233-235, 291

42 SLU6Soccorso_Pos.2 N. carichi: 7
Lista carichi: 41, 122-123, 236-238, 292

43 SLU6Soccorso_Pos.2 N. carichi: 7
Lista carichi: 42, 124-125, 239-241, 293

44 Cond8SoloVarSoccPOS N. carichi: 7
Lista carichi: 43, 126-127, 242-244, 294

45 Inviluppo_(pos) N. carichi: 7
Lista carichi: 44, 128-129, 245-247, 295

46 Inviluppo_(neg) N. carichi: 2
Lista carichi: 130, 248

47 Inviluppo N. carichi: 7
Lista carichi: 45, 131-132, 249-251, 296

48 peso_proprio N. carichi: 432
Lista carichi: 297-348, 1345-1724

49 spinta_ter N. carichi: 332
Lista carichi: 349-680

50 sovraspinta_sismica N. carichi: 332
Lista carichi: 681-1012

51 spinta_folla N. carichi: 332
Lista carichi: 1013-1344

RISULTANTI DEI CARICHI (punto di applicazione nell'origine degli assi):

cond.	FX	FY	FZ	MX	MY	MZ
1	2.437800E+04	4.519000E+03	-5.294120E+04	-1.167923E+07	4.662581E+07	-
9.484825E+06						
2	2.437800E+04	4.519000E+03	-5.113880E+04	-1.132777E+07	4.525899E+07	-
9.484825E+06						
3	2.422200E+04	-5.741000E+03	-5.294120E+04	-8.601234E+06	4.657901E+07	-
9.475285E+06						
4	2.422200E+04	-5.741000E+03	-5.113880E+04	-8.249766E+06	4.521219E+07	-
9.475285E+06						
5	-2.422200E+04	5.741000E+03	-5.294120E+04	-1.204583E+07	3.204581E+07	
9.475285E+06						
6	-2.422200E+04	5.741000E+03	-5.113880E+04	-1.169437E+07	3.067899E+07	
9.475285E+06						
7	-2.437800E+04	-4.519000E+03	-5.294120E+04	-8.967834E+06	3.199901E+07	
9.484825E+06						
8	-2.437800E+04	-4.519000E+03	-5.113880E+04	-8.616366E+06	3.063219E+07	
9.484825E+06						
9	7.550000E+03	1.691670E+04	-5.294120E+04	-1.539854E+07	4.157741E+07	-
2.859917E+06						

10	7.550000E+03	1.691670E+04	-5.113880E+04	-1.504708E+07	4.021059E+07	-
2.859917E+06						
11	-7.030000E+03	1.728330E+04	-5.294120E+04	-1.550852E+07	3.720341E+07	
2.828117E+06						
12	-7.030000E+03	1.728330E+04	-5.113880E+04	-1.515706E+07	3.583659E+07	
2.828117E+06						
13	7.030000E+03	-1.728330E+04	-5.294120E+04	-5.138544E+06	4.142141E+07	-
2.828117E+06						
14	7.030000E+03	-1.728330E+04	-5.113880E+04	-4.787076E+06	4.005459E+07	-
2.828117E+06						
15	-7.550000E+03	-1.691670E+04	-5.294120E+04	-5.248524E+06	3.704741E+07	
2.859917E+06						
16	-7.550000E+03	-1.691670E+04	-5.113880E+04	-4.897056E+06	3.568059E+07	
2.859917E+06						
17	7.368000E+03	4.946700E+03	-5.504400E+04	-1.221759E+07	4.311742E+07	-
2.848787E+06						
18	7.212000E+03	-5.313300E+03	-5.504400E+04	-9.139590E+06	4.307062E+07	-
2.839247E+06						
19	-7.212000E+03	5.313300E+03	-5.504400E+04	-1.232757E+07	3.874342E+07	
2.839247E+06						
20	-7.368000E+03	-4.946700E+03	-5.504400E+04	-9.249570E+06	3.869662E+07	
2.848787E+06						
21	7.368000E+03	4.946700E+03	-4.903600E+04	-1.104603E+07	3.856138E+07	-
2.848787E+06						
22	7.212000E+03	-5.313300E+03	-4.903600E+04	-7.968030E+06	3.851458E+07	-
2.839247E+06						
23	-7.212000E+03	5.313300E+03	-4.903600E+04	-1.115601E+07	3.418738E+07	
2.839247E+06						
24	-7.556700E+03	-4.946700E+03	-4.903600E+04	-8.078010E+06	3.408397E+07	
2.922380E+06						
25	-6.158000E+03	0.000000E+00	-5.204000E+04	-1.014780E+07	3.678160E+07	
2.401620E+06						
26	-3.694000E+03	0.000000E+00	-8.574000E+04	-1.671930E+07	6.253850E+07	
1.440660E+06						
27	-3.694000E+03	0.000000E+00	-1.221200E+05	-2.381340E+07	8.955520E+07	
1.440660E+06						
28	-6.158000E+03	0.000000E+00	-9.484000E+04	-1.849380E+07	6.856080E+07	
2.401620E+06						
29	0.000000E+00	-1.080000E+04	-9.466000E+04	-1.665780E+07	6.834870E+07	-
5.400000E+04						
30	-4.106000E+03	0.000000E+00	-6.418000E+04	-1.251510E+07	4.642230E+07	
1.601340E+06						
31	-4.106000E+03	0.000000E+00	-5.204000E+04	-1.014780E+07	3.739720E+07	
1.601340E+06						
32	-2.463000E+03	0.000000E+00	-8.238000E+04	-1.606410E+07	6.040900E+07	
9.605700E+05						
33	-2.463000E+03	0.000000E+00	-5.812000E+04	-1.133340E+07	4.241730E+07	
9.605700E+05						
34	0.000000E+00	-7.200000E+03	-6.406000E+04	-1.129110E+07	4.626650E+07	-
3.600000E+04						
35	0.000000E+00	0.000000E+00	-7.180000E+03	-1.400100E+06	5.326940E+06	
0.000000E+00						
36	0.000000E+00	0.000000E+00	-2.243800E+04	-4.375410E+06	1.665983E+07	
0.000000E+00						
37	0.000000E+00	0.000000E+00	-2.243800E+04	-4.375410E+06	1.665983E+07	
0.000000E+00						
38	0.000000E+00	0.000000E+00	-6.066000E+03	-1.182870E+06	4.503770E+06	
0.000000E+00						
39	-4.106000E+03	0.000000E+00	0.000000E+00	0.000000E+00	-1.231800E+06	
1.601340E+06						
40	0.000000E+00	0.000000E+00	-3.032200E+04	-5.912790E+06	2.251297E+07	
0.000000E+00						
41	0.000000E+00	7.200000E+03	-1.199900E+04	-5.459790E+06	7.627175E+06	
3.600000E+04						
42	0.000000E+00	1.940000E+04	-9.465000E+04	-2.571780E+07	8.237925E+07	
9.700000E+04						
43	0.000000E+00	1.317000E+04	-6.405000E+04	-1.740210E+07	5.562505E+07	

```

6.585000E+04
  44  0.000000E+00  7.200000E+03 -1.200020E+04 -5.460024E+06  1.698432E+07
3.600000E+04
  45  2.671800E+04  3.022000E+04 -1.229000E+05 -3.318360E+07  9.982150E+07 -
1.026892E+07
  46 -2.671800E+04  0.000000E+00  0.000000E+00  0.000000E+00 -8.015400E+06
1.042002E+07
  47 -2.671800E+04  3.022000E+04 -1.229000E+05 -3.318360E+07  8.379070E+07
1.057112E+07
  48  0.000000E+00  0.000000E+00 -1.694914E+05 -3.305081E+07  1.245761E+08
0.000000E+00
  49  0.000000E+00  0.000000E+00  0.000000E+00  0.000000E+00  0.000000E+00
0.000000E+00
  50  0.000000E+00  0.000000E+00  0.000000E+00  0.000000E+00  0.000000E+00
0.000000E+00
  51  0.000000E+00  0.000000E+00  0.000000E+00  0.000000E+00  0.000000E+00
0.000000E+00

```

2 - VERIFICA PIASTRE E SETTI

I tabulati che seguono contengono i risultati delle verifiche relative alle piastre e ai setti in cemento armato in termini di quantitativo di armatura e limiti di fessurazione. Se non diversamente specificato per il singolo elemento, le caratteristiche e i requisiti di riferimento sono quelli riportati all'inizio di questo capitolo.

Informazioni generali - Tipologia piastra/setto 1

CASI DI CARICO: ->

Nome	Descrizione
1	Din EX+0.3EY+0.3EZ
2	Din EX+0.3EY-0.3EZ
3	Din EX-0.3EY+0.3EZ
4	Din EX-0.3EY+0.3EZ
5	Din -EX+0.3EY+0.3EZ
6	Din -EX+0.3EY-0.3EZ
7	Din -EX-0.3EY+0.3EZ
8	Din -EX-0.3EY-0.3EZ
9	Din 0.3EX+EY+0.3EZ
10	Din 0.3EX+EY-0.3EZ
11	Din -0.3EX+EY+0.3EZ
12	Din -0.3EX+EY-0.3EZ
13	Din 0.3EX-EY+0.3EZ
14	Din 0.3EX-EY-0.3EZ
15	Din -0.3EX-EY+0.3EZ
16	Din -0.3EX-EY-0.3EZ
17	Din 0.3EX+0.3EY+EZ
18	Din 0.3EX-0.3EY+EZ
19	Din -0.3EX+0.3EY+EZ
20	Din -0.3EX-0.3EY+EZ
21	Din 0.3EX+0.3EY-EZ
22	Din 0.3EX-0.3EY-EZ
23	Din -0.3EX+0.3EY-EZ
24	Din -0.3EX-0.3EY-EZ
25	SLU1Stat solo Vento
26	SLU2Stat Neve dom
27	SLU3Stat Acc dom
28	SLU4Stat Vento dom
29	SLU5Stat socc POS.1
35	Cond1Solo P.P.Strutt
36	Cond2Solo P.P.SolPre
37	Cond3Solo Portati-G2
38	Cond4Solo Var Neve
39	Cond5Solo Var Vento
40	Cond6Solo Var Folla
41	Cond7Solo Var Socc
42	SLU6Soccorso Pos.2

43 SLU6Soccorso Pos.2
44 Cond8SoloVarSoccPOS2

DATI:

tensione di snervamento acciaio (fyk): 4500 daN/cm2
coefficiente sicurezza acciaio : 1.15
deformazione ultima acciaio : 1.9565 per mille
deformazione ultima cls : 3.5 per mille
rapporto rottura/snervamento (k): 1
resistenza cilindrica cls (fck): 249 daN/cm2
coefficiente sicurezza cls : 1.5

L'elemento che segue fa riferimento alla Tipologia 1.

VERIFICA ARMATURE EFFETTIVE (EFFETTO MEMBRANA + PIASTRA)

CASI DI CARICO: ->

Nome	Descrizione
1	Din EX+0.3EY+0.3EZ
2	Din EX+0.3EY-0.3EZ
3	Din EX-0.3EY+0.3EZ
4	Din EX-0.3EY-0.3EZ
5	Din -EX+0.3EY+0.3EZ
6	Din -EX+0.3EY-0.3EZ
7	Din -EX-0.3EY+0.3EZ
8	Din -EX-0.3EY-0.3EZ
9	Din 0.3EX+EY+0.3EZ
10	Din 0.3EX+EY-0.3EZ
11	Din -0.3EX+EY+0.3EZ
12	Din -0.3EX+EY-0.3EZ
13	Din 0.3EX-EY+0.3EZ
14	Din 0.3EX-EY-0.3EZ
15	Din -0.3EX-EY+0.3EZ
16	Din -0.3EX-EY-0.3EZ
17	Din 0.3EX+0.3EY+EZ
18	Din 0.3EX-0.3EY+EZ
19	Din -0.3EX+0.3EY+EZ
20	Din -0.3EX-0.3EY+EZ
21	Din 0.3EX+0.3EY-EZ
22	Din 0.3EX-0.3EY-EZ
23	Din -0.3EX+0.3EY-EZ
24	Din -0.3EX-0.3EY-EZ
25	SLU1Stat solo Vento
26	SLU2Stat Neve dom
27	SLU3Stat Acc dom
28	SLU4Stat Vento dom
29	SLU5Stat socc POS.1
35	Cond1Solo P.P.Strutt
36	Cond2Solo P.P.SolPre
37	Cond3Solo Portati-G2
38	Cond4Solo Var Neve
39	Cond5Solo Var Vento
40	Cond6Solo Var Folla
41	Cond7Solo Var Socc
42	SLU6Soccorso Pos.2
43	SLU6Soccorso Pos.2
44	Cond8SoloVarSoccPOS2

DATI:

tensione di snervamento acciaio (fyk): 4500 daN/cm2
coefficiente sicurezza acciaio : 1.15
deformazione ultima acciaio : 67.5 per mille
deformazione ultima cls : 3.5 per mille
rapporto rottura/snervamento (k): 1.15
resistenza cilindrica cls (fck): 249 daN/cm2
coefficiente sicurezza cls : 1.5
coefficiente riduttivo (alfa): 0.85
copriferro inferiore (asse armatura): 3 cm
copriferro superiore (asse armatura): 3 cm

moltiplicatore sollecitazioni : 1

LEGENDA:

spess = spessore guscio. Verifica effettuata su sezione BxH, con B=1 cm e H="spess" cm
 Af = area disposta al lembo teso, in cm2 al metro
 Afc = area disposta al lembo compresso, in cm2 al metro
 Mom = momento flettente [daNcm/cm]
 Nor = sforzo normale [daN]
 epsC = deformazione cls [per mille]
 epsF = deformazione acciaio [per mille]

<-

L'armatura è sufficiente se le deformazioni dei materiali sono ovunque minori delle corrispondenti deformazioni ultime.

MACROGUSCIO spalla_01

COEF. GUSCI spess MAX %	INFERIORE ORIZZONTALE								INFERIORE VERTICALE					
	Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF		
1	20	6.79	6.79	0.	60.	0.00	0.22	5.89	5.89	0.	14.	0.00	0.06	
10														
2	20	6.79	14.33	0.	43.	0.00	0.16	5.89	5.89	0.	29.	0.00	0.12	
6														
3	20	6.79	6.79	0.	86.	0.00	0.32	5.89	5.89	0.	12.	0.00	0.05	
14														
4	20	6.79	14.33	0.	80.	0.00	0.29	5.89	5.89	0.	31.	0.00	0.13	
8														
5	20	6.79	6.79	0.	94.	0.00	0.35	5.89	5.89	0.	8.	0.00	0.04	
15														
6	20	6.79	14.33	0.	87.	0.00	0.32	5.89	5.89	0.	18.	0.00	0.08	
9														
7	20	6.79	6.79	0.	97.	0.00	0.36	5.89	5.89	0.	4.	0.00	0.02	
16														
8	20	6.79	14.33	0.	86.	0.00	0.32	5.89	5.89	0.	2.	0.00	0.01	
9														
9	20	6.79	6.79	0.	98.	0.00	0.36	5.89	5.89	0.	-2.	0.00	0.01	
16														
10	20	6.79	14.33	0.	85.	0.00	0.31	5.89	5.89	0.	-1.	0.00	0.00	
9														
11	20	6.79	6.79	0.	98.	0.00	0.36	5.89	5.89	0.	-2.	0.00	0.01	
16														
12	20	6.79	14.33	0.	85.	0.00	0.31	5.89	5.89	0.	1.	0.00	0.00	
9														
13	20	6.79	6.79	0.	97.	0.00	0.36	5.89	5.89	0.	4.	0.00	0.02	
16														
14	20	6.79	14.33	0.	86.	0.00	0.32	5.89	5.89	0.	3.	0.00	0.01	
9														
15	20	6.79	6.79	0.	94.	0.00	0.35	5.89	5.89	0.	8.	0.00	0.04	
15														
16	20	6.79	14.33	0.	87.	0.00	0.32	5.89	5.89	0.	18.	0.00	0.08	
9														
17	20	6.79	6.79	0.	86.	0.00	0.32	5.89	5.89	0.	12.	0.00	0.05	
14														
18	20	6.79	14.33	0.	80.	0.00	0.29	5.89	5.89	0.	31.	0.00	0.13	
8														
19	20	6.79	6.79	0.	60.	0.00	0.22	5.89	5.89	0.	14.	0.00	0.06	
10														
20	20	6.79	14.33	0.	43.	0.00	0.16	5.89	5.89	0.	29.	0.00	0.12	
6														
21	20	6.03	6.03	0.	85.	0.00	0.35	6.09	6.09	0.	70.	0.00	0.29	
16														
22	20	6.03	6.03	0.	97.	0.00	0.40	6.09	6.09	0.	60.	0.00	0.25	
18														
23	20	6.03	6.03	0.	97.	0.00	0.40	6.09	6.09	0.	35.	0.00	0.14	
18														
24	20	6.03	6.03	0.	87.	0.00	0.36	6.09	6.09	0.	18.	0.00	0.07	
16														
25	20	6.03	6.03	0.	82.	0.00	0.34	6.09	6.09	0.	18.	0.00	0.08	
15														
26	20	6.03	6.03	0.	83.	0.00	0.34	6.09	6.09	0.	23.	0.00	0.10	
15														
27	20	6.03	6.03	0.	85.	0.00	0.35	6.09	6.09	0.	71.	0.00	0.29	
16														
28	20	6.03	6.03	0.	97.	0.00	0.40	6.09	6.09	0.	60.	0.00	0.25	

18													
29	20	6.03	6.03	0.	97.	0.00	0.40	6.09	6.09	0.	34.	0.00	0.14
18													
30	20	6.03	6.03	0.	87.	0.00	0.36	6.09	6.09	0.	17.	0.00	0.07
16													
31	20	6.03	6.03	0.	82.	0.00	0.34	11.98	11.98	0.	18.	0.00	0.04
15													
32	20	6.03	6.03	0.	83.	0.00	0.34	11.98	11.98	0.	23.	0.00	0.09
15													
33	40	6.03	6.03	0.	141.	0.00	0.58	22.45	22.45	0.	36.	0.00	0.15
26													
34	40	6.03	6.03	0.	156.	0.00	0.64	22.45	22.45	0.	37.	0.00	0.15
29													
35	40	6.03	6.03	0.	131.	0.00	0.54	6.09	6.09	0.	58.	0.00	0.24
24													
36	40	6.03	6.03	0.	155.	0.00	0.64	6.09	6.09	0.	54.	0.00	0.22
29													
37	40	6.03	6.03	0.	106.	0.00	0.44	6.09	6.09	0.	77.	0.00	0.31
20													
38	40	6.03	6.03	0.	133.	0.00	0.55	6.09	6.09	0.	72.	0.00	0.29
24													
39	40	6.03	6.03	0.	16.	0.00	0.07	6.09	6.09	0.	76.	0.00	0.31
14													
40	40	6.03	6.03	0.	45.	0.00	0.19	6.09	6.09	0.	88.	0.00	0.36
16													
41	40	6.03	6.03	0.	73.	0.00	0.30	6.09	6.09	0.	89.	0.00	0.36
16													
42	40	6.03	6.03	0.	63.	0.00	0.26	6.09	6.09	0.	79.	0.00	0.32
14													
43	40	6.03	6.03	0.	79.	0.00	0.33	6.09	6.09	0.	78.	0.00	0.32
15													
44	40	6.03	6.03	0.	101.	0.00	0.42	6.09	6.09	0.	82.	0.00	0.34
19													
45	40	6.03	6.03	0.	17.	0.00	0.07	6.09	6.09	0.	84.	0.00	0.34
15													
46	40	6.03	6.03	0.	17.	0.00	0.07	6.09	6.09	0.	86.	0.00	0.35
16													
47	40	6.03	6.03	0.	13.	0.00	0.05	6.09	6.09	0.	64.	0.00	0.26
12													
48	40	6.03	6.03	0.	43.	0.00	0.18	6.09	6.09	0.	89.	0.00	0.36
16													
49	40	6.03	6.03	0.	37.	0.00	0.15	6.09	6.09	0.	89.	0.00	0.36
16													
50	40	6.03	6.03	0.	21.	0.00	0.09	6.09	6.09	0.	63.	0.00	0.26
11													
51	40	6.03	6.03	0.	60.	0.00	0.25	6.09	6.09	0.	90.	0.00	0.37
16													
52	40	6.03	6.03	0.	42.	0.00	0.17	6.09	6.09	0.	89.	0.00	0.37
16													
53	40	6.03	6.03	0.	23.	0.00	0.10	6.09	6.09	0.	62.	0.00	0.26
11													
54	40	6.03	6.03	0.	72.	0.00	0.30	6.09	6.09	0.	87.	0.00	0.36
16													
55	40	6.03	6.03	0.	45.	0.00	0.19	6.09	6.09	0.	89.	0.00	0.36
16													
56	40	6.03	6.03	0.	23.	0.00	0.09	6.09	6.09	0.	60.	0.00	0.25
11													
57	40	6.03	12.49	0.	89.	0.00	0.37	6.09	6.09	0.	67.	0.00	0.28
16													
58	40	6.03	12.49	0.	63.	0.00	0.26	6.09	13.63	0.	73.	0.00	0.30
13													
59	40	6.03	12.49	0.	42.	0.00	0.17	6.09	13.63	0.	43.	0.00	0.18
8													
60	40	6.03	12.49	0.	106.	0.00	0.44	22.45	22.45	0.	43.	0.00	0.18
13													
61	40	6.03	12.49	0.	81.	0.00	0.34	22.45	29.99	0.	51.	0.00	0.21
10													
62	40	6.03	12.49	0.	61.	0.00	0.25	22.45	29.99	0.	30.	0.00	0.12
7													
63	40	6.03	6.03	0.	141.	0.00	0.58	6.09	6.09	0.	40.	0.00	0.17
26													
64	40	6.03	6.03	0.	155.	0.00	0.64	6.09	6.09	0.	34.	0.00	0.14
29													
65	40	6.03	6.03	0.	131.	0.00	0.54	6.09	6.09	0.	60.	0.00	0.25
24													
66	40	6.03	6.03	0.	155.	0.00	0.64	6.09	6.09	0.	55.	0.00	0.22

29																	
67		40		6.03	6.03	0.	106.	0.00	0.44		6.09	6.09	0.	76.	0.00	0.31	
20																	
68		40		6.03	6.03	0.	132.	0.00	0.55		6.09	6.09	0.	72.	0.00	0.29	
24																	
69		40		6.03	6.03	0.	16.	0.00	0.07		6.09	6.09	0.	76.	0.00	0.31	
14																	
70		40		6.03	6.03	0.	45.	0.00	0.19		6.09	6.09	0.	88.	0.00	0.36	
16																	
71		40		6.03	6.03	0.	73.	0.00	0.30		6.09	6.09	0.	89.	0.00	0.36	
16																	
72		40		6.03	6.03	0.	64.	0.00	0.27		6.09	6.09	0.	79.	0.00	0.32	
14																	
73		40		6.03	6.03	0.	79.	0.00	0.33		6.09	6.09	0.	78.	0.00	0.32	
15																	
74		40		6.03	6.03	0.	101.	0.00	0.42		6.09	6.09	0.	82.	0.00	0.34	
19																	
75		40		6.03	12.63	0.	106.	0.00	0.44		6.09	6.09	0.	47.	0.00	0.19	
13																	
76		40		6.03	12.63	0.	81.	0.00	0.33		6.09	13.63	0.	53.	0.00	0.22	
10																	
77		40		6.03	12.63	0.	60.	0.00	0.25		6.09	13.63	0.	31.	0.00	0.13	
7																	
78		40		6.03	6.03	0.	89.	0.00	0.37		6.09	6.09	0.	69.	0.00	0.28	
16																	
79		40		6.03	6.03	0.	63.	0.00	0.26		6.09	6.09	0.	74.	0.00	0.30	
14																	
80		40		6.03	6.03	0.	41.	0.00	0.17		6.09	6.09	0.	44.	0.00	0.18	
8																	
81		40		6.03	6.03	0.	72.	0.00	0.30		6.09	6.09	0.	87.	0.00	0.36	
16																	
82		40		6.03	6.03	0.	45.	0.00	0.19		6.09	6.09	0.	89.	0.00	0.36	
16																	
83		40		6.03	6.03	0.	23.	0.00	0.09		6.09	6.09	0.	60.	0.00	0.25	
11																	
84		40		6.03	6.03	0.	60.	0.00	0.25		6.09	6.09	0.	90.	0.00	0.37	
16																	
85		40		6.03	6.03	0.	43.	0.00	0.18		6.09	6.09	0.	89.	0.00	0.37	
16																	
86		40		6.03	6.03	0.	25.	0.00	0.10		6.09	6.09	0.	62.	0.00	0.26	
11																	
87		40		6.03	6.03	0.	43.	0.00	0.18		6.09	6.09	0.	89.	0.00	0.36	
16																	
88		40		6.03	6.03	0.	37.	0.00	0.15		6.09	6.09	0.	89.	0.00	0.36	
16																	
89		40		6.03	6.03	0.	21.	0.00	0.09		6.09	6.09	0.	63.	0.00	0.26	
11																	
90		40		6.03	6.03	0.	17.	0.00	0.07		6.09	6.09	0.	84.	0.00	0.34	
15																	
91		40		6.03	6.03	0.	17.	0.00	0.07		6.09	6.09	0.	86.	0.00	0.35	
16																	
92		40		6.03	6.03	0.	13.	0.00	0.05		6.09	6.09	0.	64.	0.00	0.26	
12																	
93		140		16.76	16.76	0.	119.	0.00	0.18		16.36	16.36	0.	70.	0.00	0.11	
8																	
94		140		16.76	16.76	0.	120.	0.00	0.18		16.36	16.36	0.	87.	0.00	0.13	
8																	
95		140		16.76	16.76	0.	218.	0.00	0.32		16.36	16.36	0.	58.	0.00	0.09	
14																	
96		140		16.76	16.76	0.	216.	0.00	0.32		16.36	16.36	0.	81.	0.00	0.12	
14																	
97		140		16.76	16.76	0.	224.	0.00	0.33		16.36	16.36	0.	53.	0.00	0.08	
15																	
98		140		16.76	16.76	0.	224.	0.00	0.33		16.36	16.36	0.	74.	0.00	0.11	
15																	
99		140		16.76	16.76	0.	219.	0.00	0.33		16.36	16.36	0.	37.	0.00	0.06	
15																	
100		140		16.76	16.76	0.	219.	0.00	0.33		16.36	16.36	0.	40.	0.00	0.06	
15																	
101		140		16.76	16.76	0.	209.	0.00	0.31		16.36	16.36	0.	-13.	0.00	0.01	
14																	
102		140		16.76	16.76	0.	209.	0.00	0.31		16.36	16.36	0.	-23.	0.00	0.00	
14																	
103		140		16.76	16.76	0.	209.	0.00	0.31		16.36	16.36	0.	15.	0.00	0.02	
14																	
104		140		16.76	16.76	0.	209.	0.00	0.31		16.36	16.36	0.	-25.	0.00	0.00	

14															
105		140	16.76	16.76	0.	225.	0.00	0.33	16.36	16.36	0.	44.	0.00	0.07	
15															
106		140	16.76	16.76	0.	225.	0.00	0.33	16.36	16.36	0.	39.	0.00	0.06	
15															
107		140	16.76	16.76	0.	222.	0.00	0.33	16.36	16.36	0.	61.	0.00	0.09	
15															
108		140	16.76	16.76	0.	222.	0.00	0.33	16.36	16.36	0.	76.	0.00	0.12	
15															
109		140	16.76	16.76	0.	222.	0.00	0.33	16.36	16.36	0.	70.	0.00	0.11	
15															
110		140	16.76	16.76	0.	221.	0.00	0.33	16.36	16.36	0.	87.	0.00	0.13	
15															
111		140	16.76	16.76	0.	114.	0.00	0.17	16.36	16.36	0.	80.	0.00	0.12	
8															
112		140	16.76	16.76	0.	116.	0.00	0.17	16.36	16.36	0.	96.	0.00	0.15	
8															
113		140	16.76	16.76	0.	120.	0.00	0.18	16.36	16.36	0.	103.	0.00	0.16	
8															
114		140	16.76	16.76	0.	120.	0.00	0.18	16.36	16.36	0.	115.	0.00	0.18	
8															
115		140	16.76	16.76	0.	120.	0.00	0.18	16.36	16.36	0.	79.	0.00	0.12	
8															
116		140	16.76	16.76	0.	216.	0.00	0.32	16.36	16.36	0.	94.	0.00	0.14	
14															
117		140	16.76	16.76	0.	216.	0.00	0.32	16.36	16.36	0.	104.	0.00	0.16	
14															
118		140	16.76	16.76	0.	216.	0.00	0.32	16.36	16.36	0.	74.	0.00	0.11	
14															
119		140	16.76	16.76	0.	224.	0.00	0.33	16.36	16.36	0.	85.	0.00	0.13	
15															
120		140	16.76	16.76	0.	224.	0.00	0.33	16.36	16.36	0.	95.	0.00	0.14	
15															
121		140	16.76	16.76	0.	224.	0.00	0.33	16.36	16.36	0.	65.	0.00	0.10	
15															
122		140	16.76	16.76	0.	219.	0.00	0.33	16.36	16.36	0.	44.	0.00	0.07	
15															
123		140	16.76	16.76	0.	219.	0.00	0.33	16.36	16.36	0.	40.	0.00	0.06	
15															
124		140	16.76	16.76	0.	219.	0.00	0.33	16.36	16.36	0.	24.	0.00	0.04	
15															
125		140	16.76	16.76	0.	209.	0.00	0.31	16.36	16.36	0.	-28.	0.00	0.00	
14															
126		140	16.76	16.76	0.	209.	0.00	0.31	16.36	16.36	0.	-18.	0.00	0.00	
14															
127		140	16.76	16.76	0.	209.	0.00	0.31	16.36	16.36	0.	18.	0.00	0.03	
14															
128		140	16.76	16.76	0.	209.	0.00	0.31	16.36	16.36	0.	-28.	0.00	0.00	
14															
129		140	16.76	16.76	0.	209.	0.00	0.31	16.36	16.36	0.	-16.	0.00	0.00	
14															
130		140	16.76	16.76	0.	209.	0.00	0.31	16.36	16.36	0.	18.	0.00	0.03	
14															
131		140	16.76	16.76	0.	225.	0.00	0.33	16.36	16.36	0.	44.	0.00	0.07	
15															
132		140	16.76	16.76	0.	225.	0.00	0.33	16.36	16.36	0.	45.	0.00	0.07	
15															
133		140	16.76	16.76	0.	225.	0.00	0.33	16.36	16.36	0.	24.	0.00	0.04	
15															
134		140	16.76	16.76	0.	222.	0.00	0.33	16.36	16.36	0.	86.	0.00	0.13	
15															
135		140	16.76	16.76	0.	222.	0.00	0.33	16.36	16.36	0.	99.	0.00	0.15	
15															
136		140	16.76	16.76	0.	222.	0.00	0.33	16.36	16.36	0.	66.	0.00	0.10	
15															
137		140	16.76	16.76	0.	221.	0.00	0.33	16.36	16.36	0.	100.	0.00	0.15	
15															
138		140	16.76	16.76	0.	221.	0.00	0.33	16.36	16.36	0.	114.	0.00	0.17	
15															
139		140	16.76	16.76	0.	221.	0.00	0.33	16.36	16.36	0.	76.	0.00	0.12	
15															
140		140	16.76	16.76	0.	116.	0.00	0.17	16.36	16.36	0.	109.	0.00	0.17	
8															
141		140	16.76	16.76	0.	116.	0.00	0.17	16.36	23.90	0.	122.	0.00	0.19	
8															
142		140	16.76	16.76	0.	116.	0.00	0.17	16.36	23.90	0.	81.	0.00	0.12	

8													
143	140	16.76	16.76	0.	120.	0.00	0.18	16.36	16.36	0.	-9.	0.00	0.00
8													
144	140	16.76	16.76	0.	114.	0.00	0.17	16.36	16.36	0.	-67.	0.00	0.00
8													
145	140	16.76	16.76	0.	216.	0.00	0.32	16.36	16.36	0.	-10.	0.00	0.00
14													
147	140	16.76	16.76	0.	224.	0.00	0.33	16.36	16.36	0.	-10.	0.00	0.00
15													
148	140	16.76	16.76	0.	211.	0.00	0.31	16.36	16.36	0.	-98.	0.00	0.00
14													
149	140	16.76	16.76	0.	219.	0.00	0.33	16.36	16.36	0.	-9.	0.00	0.00
15													
150	140	16.76	16.76	0.	207.	0.00	0.31	16.36	16.36	0.	-98.	0.00	0.00
14													
151	140	16.76	16.76	0.	209.	0.00	0.31	16.36	16.36	0.	-9.	0.00	0.00
14													
152	140	16.76	16.76	0.	193.	0.00	0.29	16.36	16.36	0.	-98.	0.00	0.00
13													
153	140	16.76	16.76	0.	209.	0.00	0.31	16.36	16.36	0.	-9.	0.00	0.00
14													
154	140	16.76	16.76	0.	191.	0.00	0.29	16.36	16.36	0.	-98.	0.00	0.00
13													
155	140	16.76	16.76	0.	225.	0.00	0.33	16.36	16.36	0.	-9.	0.00	0.00
15													
156	140	16.76	16.76	0.	210.	0.00	0.31	16.36	16.36	0.	-98.	0.00	0.00
14													
157	140	16.76	16.76	0.	222.	0.00	0.33	16.36	16.36	0.	-10.	0.00	0.00
15													
158	140	16.76	16.76	0.	207.	0.00	0.31	16.36	16.36	0.	-99.	0.00	0.00
14													
159	140	16.76	16.76	0.	221.	0.00	0.33	16.36	16.36	0.	-9.	0.00	0.00
15													
161	140	16.76	16.76	0.	116.	0.00	0.17	16.36	16.36	0.	-3.	0.00	0.00
8													
162	140	16.76	16.76	0.	109.	0.00	0.16	16.36	16.36	0.	-64.	0.00	0.00
7													
199	140	16.76	16.76	0.	199.	0.00	0.30	16.36	16.36	0.	-44.	0.00	0.00
13													
200	140	16.76	16.76	0.	214.	0.00	0.32	16.36	16.36	0.	-37.	0.00	0.00
14													
201	140	16.76	16.76	0.	113.	0.00	0.17	16.36	16.36	0.	-79.	0.00	0.00
7													
202	140	16.76	16.76	0.	112.	0.00	0.17	16.36	16.36	0.	-81.	0.00	0.00
7													
203	140	16.76	16.76	0.	206.	0.00	0.31	16.36	16.36	0.	-39.	0.00	0.00
14													
204	140	16.76	16.76	0.	194.	0.00	0.29	16.36	16.36	0.	-47.	0.00	0.00
13													

COEF. GUSCI spess MAX %	SUPERIORE ORIZZONTALE								SUPERIORE VERTICALE					
	Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF		
1	20	14.33	6.79	100.	60.	0.00	0.27	5.89	5.89	41.	14.	0.00	0.08	
12														
2	20	14.33	6.79	4128.	38.	0.47	1.04	5.89	5.89	177.	24.	0.00	0.20	
50														
3	20	14.33	6.79	78.	83.	0.00	0.34	5.89	5.89	35.	12.	0.00	0.07	
15														
4	20	14.33	6.79	4425.	72.	0.45	1.17	5.89	5.89	177.	28.	0.00	0.22	
57														
5	20	14.33	6.79	98.	90.	0.00	0.37	5.89	5.89	32.	8.	0.00	0.05	
16														
6	20	14.33	6.79	5262.	70.	0.60	1.36	5.89	5.89	271.	12.	0.02	0.20	
66														
7	20	14.33	6.79	111.	90.	0.00	0.38	5.89	5.89	14.	4.	0.00	0.02	
17														
8	20	14.33	6.79	5725.	69.	0.68	1.47	5.89	5.89	342.	1.	0.06	0.19	
72														
9	20	14.33	6.79	119.	89.	0.00	0.38	5.89	5.89	3.	-2.	0.00	0.01	
17														
10	20	14.33	6.79	5924.	68.	0.71	1.51	5.89	5.89	375.	-1.	0.07	0.21	
74														
11	20	14.33	6.79	121.	89.	0.00	0.38	5.89	5.89	5.	-2.	0.00	0.01	
17														

12		20		14.33	6.79	5873.	68.	0.70	1.50		5.89	5.89	377.	1.	0.07	0.21	
73																	
13		20		14.33	6.79	116.	90.	0.00	0.38		5.89	5.89	15.	4.	0.00	0.02	
17																	
14		20		14.33	6.79	5569.	69.	0.65	1.43		5.89	5.89	345.	2.	0.06	0.20	
70																	
15		20		14.33	6.79	107.	90.	0.00	0.37		5.89	5.89	34.	8.	0.00	0.05	
16																	
16		20		14.33	6.79	5029.	70.	0.56	1.30		5.89	5.89	271.	12.	0.01	0.20	
64																	
17		20		14.33	6.79	89.	83.	0.00	0.34		5.89	5.89	35.	12.	0.00	0.07	
15																	
18		20		14.33	6.79	4287.	72.	0.43	1.13		5.89	5.89	181.	28.	0.00	0.22	
55																	
19		20		14.33	6.79	106.	60.	0.00	0.27		5.89	5.89	41.	14.	0.00	0.08	
12																	
20		20		14.33	6.79	3519.	38.	0.38	0.89		5.89	5.89	174.	25.	0.00	0.20	
43																	
21		20		6.03	6.03	2121.	85.	0.29	1.50		6.09	6.09	184.	70.	0.00	0.39	
73																	
22		20		6.03	6.03	2402.	92.	0.37	1.69		6.09	6.09	318.	47.	0.00	0.37	
82																	
23		20		6.03	6.03	1757.	89.	0.17	1.32		6.09	6.09	280.	35.	0.00	0.29	
64																	
24		20		6.03	6.03	2314.	87.	0.34	1.62		6.09	6.09	243.	18.	0.00	0.20	
79																	
25		20		6.03	6.03	1498.	82.	0.10	1.15		6.09	6.09	184.	18.	0.00	0.17	
55																	
26		20		6.03	6.03	696.	81.	0.00	0.71		6.09	6.09	90.	23.	0.00	0.14	
33																	
27		20		6.03	6.03	2118.	85.	0.29	1.50		6.09	6.09	183.	71.	0.00	0.39	
73																	
28		20		6.03	6.03	2396.	92.	0.37	1.68		6.09	6.09	317.	47.	0.00	0.37	
82																	
29		20		6.03	6.03	1748.	89.	0.17	1.32		6.09	6.09	281.	34.	0.00	0.29	
63																	
30		20		6.03	6.03	2304.	87.	0.34	1.61		6.09	6.09	246.	17.	0.00	0.20	
78																	
31		20		6.03	6.03	1486.	82.	0.10	1.15		11.98	11.98	186.	18.	0.00	0.09	
55																	
32		20		6.03	6.03	691.	81.	0.00	0.71		11.98	11.98	92.	23.	0.00	0.14	
33																	
33		40		12.49	6.03	6642.	120.	0.26	1.94		22.45	22.45	1304.	22.	0.01	0.43	
96																	
34		40		6.03	6.03	4446.	146.	0.07	1.66		22.45	22.45	932.	30.	0.00	0.34	
81																	
35		40		6.03	6.03	4085.	122.	0.06	1.48		6.09	6.09	1324.	58.	0.00	0.55	
72																	
36		40		6.03	6.03	3603.	139.	0.00	1.44		6.09	6.09	1020.	54.	0.00	0.46	
69																	
37		40		6.03	6.03	2558.	106.	0.00	1.05		6.09	6.09	1396.	77.	0.00	0.64	
50																	
38		40		6.03	6.03	2570.	133.	0.00	1.16		6.09	6.09	1205.	72.	0.00	0.58	
55																	
39		40		6.03	6.03	240.	16.	0.00	0.12		6.09	6.09	835.	76.	0.00	0.51	
23																	
40		40		6.03	6.03	762.	45.	0.00	0.37		6.09	6.09	1201.	86.	0.00	0.64	
30																	
41		40		6.03	6.03	1408.	72.	0.00	0.64		6.09	6.09	1325.	84.	0.00	0.66	
31																	
42		40		6.03	6.03	1380.	63.	0.00	0.59		6.09	6.09	1208.	79.	0.00	0.61	
28																	
43		40		6.03	6.03	1662.	79.	0.00	0.72		6.09	6.09	1370.	78.	0.00	0.64	
34																	
44		40		6.03	6.03	1809.	101.	0.00	0.85		6.09	6.09	1230.	82.	0.00	0.63	
40																	
45		40		6.03	6.03	228.	17.	0.00	0.12		6.09	6.09	1125.	83.	0.00	0.61	
28																	
46		40		6.03	6.03	228.	17.	0.00	0.12		6.09	6.09	1491.	86.	0.00	0.70	
33																	
47		40		6.03	6.03	183.	13.	0.00	0.10		6.09	6.09	2311.	63.	0.00	0.81	
38																	
48		40		6.03	6.03	683.	43.	0.00	0.34		6.09	6.09	1389.	85.	0.00	0.68	
31																	
49		40		6.03	6.03	621.	37.	0.00	0.30		6.09	6.09	1812.	89.	0.00	0.79	
37																	

50		40		6.03	6.03	517.	21.	0.00	0.21		6.09	6.09	2363.	62.	0.00	0.81	
39																	
51		40		6.03	6.03	1306.	60.	0.00	0.56		6.09	6.09	1691.	85.	0.00	0.75	
35																	
52		40		6.03	6.03	1129.	40.	0.00	0.43		6.09	6.09	2277.	89.	0.00	0.90	
43																	
53		40		6.03	6.03	877.	23.	0.00	0.31		6.09	6.09	2944.	60.	0.01	0.94	
45																	
54		40		6.03	6.03	2327.	72.	0.00	0.85		6.09	6.09	1874.	87.	0.00	0.80	
40																	
55		40		6.03	6.03	2196.	45.	0.02	0.71		6.09	6.09	2641.	88.	0.00	0.98	
47																	
56		40		6.03	6.03	1962.	21.	0.08	0.56		6.09	6.09	3570.	59.	0.09	1.08	
52																	
57		40		12.49	6.03	4778.	82.	0.10	1.39		6.09	6.09	2359.	65.	0.00	0.83	
68																	
58		40		12.49	6.03	4897.	62.	0.13	1.26		13.63	6.09	3410.	69.	0.03	1.09	
61																	
59		40		12.49	6.03	4978.	40.	0.16	1.16		13.63	6.09	6142.	34.	0.22	1.40	
68																	
60		40		12.49	6.03	8820.	85.	0.19	1.21		22.45	22.45	4079.	28.	0.12	1.08	
60																	
61		40		12.49	6.03	9738.	66.	0.27	1.28		29.99	22.45	5776.	37.	0.11	0.69	
63																	
62		40		12.49	6.03	10974.	44.	0.37	1.38		29.99	22.45	10053.	23.	0.25	0.94	
67																	
63		40		6.03	6.03	6654.	120.	0.87	10.84		6.09	6.09	1801.	39.	0.00	0.58	
96																	
64		40		6.03	6.03	4458.	146.	0.08	1.67		6.09	6.09	885.	34.	0.00	0.35	
81																	
65		40		6.03	6.03	4090.	121.	0.06	1.48		6.09	6.09	1393.	60.	0.00	0.58	
72																	
66		40		6.03	6.03	3610.	139.	0.00	1.44		6.09	6.09	1051.	55.	0.00	0.47	
69																	
67		40		6.03	6.03	2563.	106.	0.00	1.05		6.09	6.09	1401.	76.	0.00	0.64	
50																	
68		40		6.03	6.03	2575.	132.	0.00	1.16		6.09	6.09	1213.	72.	0.00	0.58	
55																	
69		40		6.03	6.03	240.	16.	0.00	0.12		6.09	6.09	836.	76.	0.00	0.51	
23																	
70		40		6.03	6.03	764.	45.	0.00	0.37		6.09	6.09	1203.	86.	0.00	0.64	
30																	
71		40		6.03	6.03	1411.	72.	0.00	0.64		6.09	6.09	1329.	84.	0.00	0.66	
31																	
72		40		6.03	6.03	1383.	64.	0.00	0.60		6.09	6.09	1211.	79.	0.00	0.61	
28																	
73		40		6.03	6.03	1666.	79.	0.00	0.72		6.09	6.09	1375.	78.	0.00	0.65	
34																	
74		40		6.03	6.03	1812.	101.	0.00	0.85		6.09	6.09	1235.	82.	0.00	0.63	
40																	
75		40		12.63	6.03	8833.	85.	0.18	1.20		6.09	6.09	3455.	33.	0.11	0.95	
59																	
76		40		12.63	6.03	9746.	65.	0.27	1.27		13.63	6.09	6211.	50.	0.13	0.76	
62																	
77		40		12.63	6.03	10980.	43.	0.37	1.36		13.63	6.09	9764.	23.	0.33	1.10	
67																	
78		40		12.63	6.03	4782.	82.	0.10	1.40		6.09	6.09	2725.	54.	0.00	0.87	
68																	
79		40		12.63	6.03	4900.	62.	0.13	1.26		6.09	6.09	3973.	70.	0.09	1.23	
61																	
80		40		12.63	6.03	4977.	39.	0.16	1.16		6.09	6.09	6599.	35.	0.32	1.70	
83																	
81		40		6.03	6.03	2332.	72.	0.00	0.85		6.09	6.09	1877.	87.	0.00	0.80	
41																	
82		40		6.03	6.03	2200.	45.	0.02	0.71		6.09	6.09	2640.	88.	0.00	0.98	
47																	
83		40		6.03	6.03	1966.	21.	0.08	0.56		6.09	6.09	3759.	49.	0.10	1.09	
52																	
84		40		6.03	6.03	1309.	60.	0.00	0.56		6.09	6.09	1693.	85.	0.00	0.75	
35																	
85		40		6.03	6.03	1132.	40.	0.00	0.44		6.09	6.09	2277.	89.	0.00	0.90	
43																	
86		40		6.03	6.03	880.	25.	0.00	0.31		6.09	6.09	2944.	60.	0.01	0.94	
45																	
87		40		6.03	6.03	685.	43.	0.00	0.34		6.09	6.09	1390.	85.	0.00	0.68	
31																	

88		40		6.03	6.03	623.	37.	0.00	0.30		6.09	6.09	1811.	89.	0.00	0.79	
37																	
89		40		6.03	6.03	519.	21.	0.00	0.21		6.09	6.09	2363.	62.	0.00	0.81	
39																	
90		40		6.03	6.03	228.	17.	0.00	0.12		6.09	6.09	1125.	83.	0.00	0.61	
28																	
91		40		6.03	6.03	227.	17.	0.00	0.12		6.09	6.09	1491.	86.	0.00	0.70	
33																	
92		40		6.03	6.03	183.	13.	0.00	0.10		6.09	6.09	2310.	63.	0.00	0.80	
38																	
93		140		16.76	16.76	8759.	119.	0.00	0.38		16.36	16.36	2963.	70.	0.00	0.18	
17																	
94		140		16.76	16.76	8795.	120.	0.00	0.38		16.36	16.36	4052.	87.	0.00	0.23	
18																	
95		140		16.76	16.76	13662.	209.	0.00	0.62		16.36	16.36	2784.	58.	0.00	0.15	
29																	
96		140		16.76	16.76	13742.	209.	0.00	0.62		16.36	16.36	4142.	81.	0.00	0.22	
29																	
97		140		16.76	16.76	11718.	211.	0.00	0.58		16.36	16.36	2601.	53.	0.00	0.14	
27																	
98		140		16.76	16.76	11718.	211.	0.00	0.58		16.36	16.36	3969.	74.	0.00	0.21	
27																	
99		140		16.76	16.76	12631.	219.	0.00	0.61		16.36	16.36	2499.	37.	0.00	0.11	
28																	
100		140		16.76	16.76	12631.	219.	0.00	0.61		16.36	16.36	4064.	37.	0.00	0.15	
28																	
101		140		16.76	16.76	16487.	193.	0.00	0.66		16.36	16.36	2447.	-13.	0.01	0.07	
31																	
102		140		16.76	16.76	16487.	193.	0.00	0.66		16.36	16.36	4013.	-23.	0.02	0.10	
31																	
103		140		16.76	16.76	12799.	209.	0.00	0.60		16.36	16.36	2677.	13.	0.01	0.08	
28																	
104		140		16.76	16.76	12799.	209.	0.00	0.60		16.36	16.36	4053.	-25.	0.02	0.10	
28																	
105		140		16.76	16.76	10257.	210.	0.00	0.55		16.36	16.36	2795.	44.	0.00	0.13	
26																	
106		140		16.76	16.76	10257.	210.	0.00	0.55		16.36	16.36	4391.	39.	0.00	0.16	
26																	
107		140		16.76	16.76	8975.	222.	0.00	0.53		16.36	16.36	2980.	61.	0.00	0.16	
25																	
108		140		16.76	16.76	8975.	222.	0.00	0.53		16.36	16.36	4405.	76.	0.00	0.22	
25																	
109		140		16.76	16.76	11039.	217.	0.00	0.57		16.36	16.36	3174.	70.	0.00	0.18	
26																	
110		140		16.76	16.76	11093.	217.	0.00	0.57		16.36	16.36	4591.	87.	0.00	0.24	
27																	
111		140		16.76	16.76	7716.	114.	0.00	0.35		16.36	16.36	2965.	80.	0.00	0.19	
16																	
112		140		16.76	16.76	7762.	116.	0.00	0.35		16.36	16.36	4359.	96.	0.00	0.25	
16																	
113		140		16.76	16.76	8795.	120.	0.00	0.38		16.36	16.36	6474.	103.	0.00	0.31	
18																	
114		140		16.76	16.76	8795.	120.	0.00	0.38		16.36	16.36	9104.	115.	0.00	0.39	
18																	
115		140		16.76	16.76	8795.	120.	0.00	0.38		16.36	16.36	12949.	73.	0.00	0.41	
20																	
116		140		16.76	16.76	13742.	209.	0.00	0.62		16.36	16.36	6584.	94.	0.00	0.30	
29																	
117		140		16.76	16.76	13742.	209.	0.00	0.62		16.36	16.36	9352.	104.	0.00	0.38	
29																	
118		140		16.76	16.76	13742.	209.	0.00	0.62		16.36	16.36	13222.	68.	0.00	0.41	
29																	
119		140		16.76	16.76	11718.	211.	0.00	0.58		16.36	16.36	6479.	85.	0.00	0.28	
27																	
120		140		16.76	16.76	11718.	211.	0.00	0.58		16.36	16.36	9676.	91.	0.00	0.36	
27																	
121		140		16.76	16.76	11718.	211.	0.00	0.58		16.36	16.36	13385.	65.	0.01	0.41	
27																	
122		140		16.76	16.76	12631.	219.	0.00	0.61		16.36	16.36	6596.	38.	0.01	0.22	
28																	
123		140		16.76	16.76	12631.	219.	0.00	0.61		16.36	16.36	9396.	40.	0.04	0.28	
28																	
124		140		16.76	16.76	12631.	219.	0.00	0.61		16.36	16.36	13722.	24.	0.05	0.36	
28																	
125		140		16.76	16.76	16487.	193.	0.00	0.66		16.36	16.36	6682.	-28.	0.03	0.16	
31																	

126		140		16.76	16.76	16487.	193.	0.00	0.66		16.36	16.36	10002.	-9.	0.04	0.23	
31																	
127		140		16.76	16.76	16487.	193.	0.00	0.66		16.36	16.36	13825.	18.	0.06	0.35	
31																	
128		140		16.76	16.76	12799.	209.	0.00	0.60		16.36	16.36	6718.	-28.	0.03	0.16	
28																	
129		140		16.76	16.76	12799.	209.	0.00	0.60		16.36	16.36	10087.	-8.	0.04	0.23	
28																	
130		140		16.76	16.76	12799.	209.	0.00	0.60		16.36	16.36	13884.	18.	0.06	0.35	
28																	
131		140		16.76	16.76	10257.	210.	0.00	0.55		16.36	16.36	6841.	44.	0.01	0.23	
26																	
132		140		16.76	16.76	10257.	210.	0.00	0.55		16.36	16.36	9813.	45.	0.04	0.30	
26																	
133		140		16.76	16.76	10257.	210.	0.00	0.55		16.36	16.36	14199.	21.	0.05	0.36	
26																	
134		140		16.76	16.76	8975.	222.	0.00	0.53		16.36	16.36	6955.	86.	0.00	0.29	
25																	
135		140		16.76	16.76	8975.	222.	0.00	0.53		16.36	16.36	10213.	97.	0.00	0.39	
25																	
136		140		16.76	16.76	8975.	222.	0.00	0.53		16.36	16.36	14049.	63.	0.01	0.42	
25																	
137		140		16.76	16.76	11093.	217.	0.00	0.57		16.36	16.36	6617.	100.	0.00	0.31	
27																	
138		140		16.76	16.76	11093.	217.	0.00	0.57		16.36	16.36	9759.	114.	0.00	0.40	
27																	
139		140		16.76	16.76	11093.	217.	0.00	0.57		16.36	16.36	13476.	69.	0.00	0.42	
27																	
140		140		16.76	16.76	7762.	116.	0.00	0.35		16.36	16.36	6271.	109.	0.00	0.31	
16																	
141		140		16.76	16.76	7762.	116.	0.00	0.35		23.90	16.36	9359.	122.	0.00	0.40	
19																	
142		140		16.76	16.76	7762.	116.	0.00	0.35		23.90	16.36	13000.	74.	0.00	0.42	
20																	
143		140		16.76	16.76	8795.	120.	0.00	0.38		16.36	16.36	27568.	-9.	0.12	0.64	
31																	
144		140		16.76	16.76	9058.	113.	0.00	0.37		16.36	16.36	37461.	-10.	0.16	0.87	
42																	
145		140		16.76	16.76	13742.	209.	0.00	0.62		16.36	16.36	27003.	-8.	0.12	0.63	
31																	
147		140		16.76	16.76	11718.	211.	0.00	0.58		16.36	16.36	26641.	-8.	0.11	0.62	
30																	
148		140		16.76	16.76	12604.	173.	0.00	0.58		16.36	16.36	38941.	-20.	0.17	0.90	
44																	
149		140		16.76	16.76	12631.	219.	0.00	0.61		16.36	16.36	26601.	-8.	0.11	0.62	
30																	
150		140		16.76	16.76	13010.	202.	0.00	0.60		16.36	16.36	38811.	-19.	0.17	0.89	
44																	
151		140		16.76	16.76	16487.	193.	0.00	0.66		16.36	16.36	26601.	-8.	0.11	0.62	
31																	
152		140		16.76	16.76	17732.	150.	0.00	0.66		16.36	16.36	38811.	-19.	0.17	0.89	
44																	
153		140		16.76	16.76	12799.	209.	0.00	0.60		16.36	16.36	26601.	-8.	0.11	0.62	
30																	
154		140		16.76	16.76	13183.	191.	0.00	0.58		16.36	16.36	38811.	-19.	0.17	0.89	
44																	
155		140		16.76	16.76	10257.	210.	0.00	0.55		16.36	16.36	26601.	-8.	0.11	0.62	
30																	
156		140		16.76	16.76	10257.	210.	0.00	0.54		16.36	16.36	38811.	-19.	0.17	0.89	
44																	
157		140		16.76	16.76	8975.	222.	0.00	0.53		16.36	16.36	26572.	-8.	0.11	0.62	
30																	
158		140		16.76	16.76	9244.	207.	0.00	0.52		16.36	16.36	38886.	-19.	0.17	0.90	
44																	
159		140		16.76	16.76	11093.	217.	0.00	0.57		16.36	16.36	26403.	-8.	0.11	0.61	
30																	
161		140		16.76	16.76	7762.	116.	0.00	0.35		16.36	16.36	26566.	-1.	0.11	0.62	
30																	
162		140		16.76	16.76	7994.	109.	0.00	0.34		16.36	16.36	36190.	-11.	0.16	0.84	
41																	
199		140		16.76	16.76	10192.	199.	0.00	0.53		16.36	16.36	31268.	-44.	0.14	0.71	
35																	
200		140		16.76	16.76	11290.	214.	0.00	0.57		16.36	16.36	37309.	-37.	0.16	0.85	
41																	
201		140		16.76	16.76	9109.	113.	0.00	0.37		16.36	16.36	32770.	-79.	0.14	0.72	
35																	

202 37	140	16.76	16.76	8763.	112.	0.00	0.37	16.36	16.36	33936.	-81.	0.15	0.75
203 43	140	16.76	16.76	13978.	206.	0.00	0.62	16.36	16.36	38644.	-39.	0.17	0.88
204 39	140	16.76	16.76	12295.	194.	0.00	0.57	16.36	16.36	35399.	-47.	0.15	0.80

L'ARMATURA È OVUNQUE > DELLA QUANTITÀ RICHIESTA: IL PUNTO 2.3 DELLE NTC È VERIFICATO (Rd > Ed)

VERIFICHE A FESSURAZIONE (EFFETTO MEMBRANA + PIASTRA)

CASI DI CARICO: ->

Nome	Descrizione
30	SLE1Rara Vento dom (RARA)
31	SLE2Rara Solo Vento (RARA)
32	SLE3Rara Acc dom (RARA)
33	SLE4Neve dom (RARA)
34	SLE5Soccorso POS.1 (RARA)

DATI:

copriferro inferiore (asse armatura): 3 cm
 copriferro superiore (asse armatura): 3 cm

Af = area effettiva tesa (cm2 al metro)
 Afc = area effettiva compressa (cm2 al metro)
 Mom = momento flettente [daNcm/cm]
 Nor = sforzo normale [daN]
 sigC = tensione calcestruzzo [daN/cm2]
 valore max per combinazione rara = 149.4 daN/cm2
 " " quasi permanente = 112 daN/cm2
 sigF = tensione acciaio [daN/cm2]
 valore max per combinazione rara = 3600 daN/cm2
 wkF = apertura caratteristica per combinazione frequente (mm) - valore max = 0.4 mm
 wkP = " " quasi permanente (mm) - " " = 0.3 mm

DATI FRC (calcestruzzo fibrorinforzato, verifica secondo Linee Guida maggio 2022):

fFtsk = tensione di progetto in esercizio = 0 daN/cm2

<-

ARMATURA INFERIORE ORIZZONTALE

GUSCI	Af	Afc	COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE			
			Mom	Nor	sigC	sigF	Mom	Nor	WkF	Mom	Nor	sigC	WkP
1	6.79	8.67	0.	39	0.00	286.	0.	0.	0.000	0.	0.	0.00	0.000
2	6.79	14.33	0.	29	0.00	215.	0.	0.	0.000	0.	0.	0.00	0.000
3	6.79	8.67	0.	58	0.00	427.	0.	0.	0.000	0.	0.	0.00	0.000
4	6.79	14.33	0.	53	0.00	388.	0.	0.	0.000	0.	0.	0.00	0.000
5	6.79	8.67	0.	64	0.00	470.	0.	0.	0.000	0.	0.	0.00	0.000
6	6.79	14.33	0.	54	0.00	401.	0.	0.	0.000	0.	0.	0.00	0.000
7	6.79	8.67	0.	66	0.00	486.	0.	0.	0.000	0.	0.	0.00	0.000
8	6.79	14.33	0.	54	0.00	400.	0.	0.	0.000	0.	0.	0.00	0.000
9	6.79	8.67	0.	66	0.00	483.	0.	0.	0.000	0.	0.	0.00	0.000
10	6.79	14.33	0.	53	0.00	389.	0.	0.	0.000	0.	0.	0.00	0.000
11	6.79	8.67	0.	64	0.00	469.	0.	0.	0.000	0.	0.	0.00	0.000
12	6.79	14.33	0.	52	0.00	386.	0.	0.	0.000	0.	0.	0.00	0.000
13	6.79	8.67	0.	63	0.00	466.	0.	0.	0.000	0.	0.	0.00	0.000
14	6.79	14.33	0.	52	0.00	382.	0.	0.	0.000	0.	0.	0.00	0.000
15	6.79	8.67	0.	64	0.00	471.	0.	0.	0.000	0.	0.	0.00	0.000
16	6.79	14.33	0.	54	0.00	398.	0.	0.	0.000	0.	0.	0.00	0.000
17	6.79	8.67	0.	57	0.00	418.	0.	0.	0.000	0.	0.	0.00	0.000
18	6.79	14.33	0.	52	0.00	380.	0.	0.	0.000	0.	0.	0.00	0.000
19	6.79	8.67	0.	41	0.00	304.	0.	0.	0.000	0.	0.	0.00	0.000
20	6.79	14.33	0.	30	0.00	217.	0.	0.	0.000	0.	0.	0.00	0.000
21	6.03	6.03	0.	63	0.00	524.	0.	0.	0.000	0.	0.	0.00	0.000
22	6.03	6.03	0.	72	0.00	595.	0.	0.	0.000	0.	0.	0.00	0.000
23	6.03	6.03	0.	68	0.00	565.	0.	0.	0.000	0.	0.	0.00	0.000
24	6.03	6.03	0.	66	0.00	544.	0.	0.	0.000	0.	0.	0.00	0.000
25	6.03	6.03	0.	62	0.00	510.	0.	0.	0.000	0.	0.	0.00	0.000
26	6.03	6.03	0.	59	0.00	493.	0.	0.	0.000	0.	0.	0.00	0.000
27	6.03	6.03	0.	64	0.00	528.	0.	0.	0.000	0.	0.	0.00	0.000
28	6.03	6.03	0.	72	0.00	595.	0.	0.	0.000	0.	0.	0.00	0.000
29	6.03	6.03	0.	68	0.00	561.	0.	0.	0.000	0.	0.	0.00	0.000
30	6.03	6.03	0.	65	0.00	538.	0.	0.	0.000	0.	0.	0.00	0.000
31	6.03	6.03	0.	60	0.00	501.	0.	0.	0.000	0.	0.	0.00	0.000
32	6.03	6.03	0.	58	0.00	481.	0.	0.	0.000	0.	0.	0.00	0.000
33	6.03	7.65	0.	98	0.00	816.	0.	0.	0.000	0.	0.	0.00	0.000

34		6.03	6.03	0.	112	0.00	926.		0.	0.	0.000	0.	0.	0.00	0.000
35		6.03	6.03	0.	89	0.00	741.		0.	0.	0.000	0.	0.	0.00	0.000
36		6.03	6.03	0.	111	0.00	923.		0.	0.	0.000	0.	0.	0.00	0.000
37		6.03	6.03	0.	71	0.00	586.		0.	0.	0.000	0.	0.	0.00	0.000
38		6.03	6.03	0.	91	0.00	752.		0.	0.	0.000	0.	0.	0.00	0.000
39		6.03	6.03	0.	12	0.00	97.		0.	0.	0.000	0.	0.	0.00	0.000
40		6.03	6.03	0.	29	0.00	242.		0.	0.	0.000	0.	0.	0.00	0.000
41		6.03	6.03	0.	49	0.00	408.		0.	0.	0.000	0.	0.	0.00	0.000
42		6.03	6.03	0.	47	0.00	386.		0.	0.	0.000	0.	0.	0.00	0.000
43		6.03	6.03	0.	60	0.00	497.		0.	0.	0.000	0.	0.	0.00	0.000
44		6.03	6.03	0.	67	0.00	555.		0.	0.	0.000	0.	0.	0.00	0.000
45		6.03	6.03	0.	9	0.00	78.		0.	0.	0.000	0.	0.	0.00	0.000
46		6.03	6.03	0.	9	0.00	78.		0.	0.	0.000	0.	0.	0.00	0.000
47		6.03	6.03	0.	8	0.00	64.		0.	0.	0.000	0.	0.	0.00	0.000
48		6.03	6.03	0.	21	0.00	174.		0.	0.	0.000	0.	0.	0.00	0.000
49		6.03	6.03	0.	20	0.00	168.		0.	0.	0.000	0.	0.	0.00	0.000
50		6.03	6.03	0.	11	0.00	91.		0.	0.	0.000	0.	0.	0.00	0.000
51		6.03	6.03	0.	34	0.00	279.		0.	0.	0.000	0.	0.	0.00	0.000
52		6.03	6.03	0.	20	0.00	164.		0.	0.	0.000	0.	0.	0.00	0.000
53		6.03	6.03	0.	5	0.00	41.		0.	0.	0.000	0.	0.	0.00	0.000
54		6.03	6.03	0.	37	0.00	310.		0.	0.	0.000	0.	0.	0.00	0.000
55		6.03	6.03	0.	19	0.00	158.		0.	0.	0.000	0.	0.	0.00	0.000
56		6.03	6.03	0.	-1	0.03	0.		0.	0.	0.000	0.	0.	0.00	0.000
57		6.03	7.65	0.	41	0.00	340.		0.	0.	0.000	0.	0.	0.00	0.000
58		6.03	7.65	0.	22	0.00	183.		0.	0.	0.000	0.	0.	0.00	0.000
59		6.03	7.65	0.	-1	0.03	0.		0.	0.	0.000	0.	0.	0.00	0.000
60		6.03	12.49	0.	58	0.00	483.		0.	0.	0.000	0.	0.	0.00	0.000
61		6.03	12.49	0.	41	0.00	336.		0.	0.	0.000	0.	0.	0.00	0.000
62		6.03	12.49	0.	21	0.00	171.		0.	0.	0.000	0.	0.	0.00	0.000
63		6.03	6.03	0.	99	0.00	819.		0.	0.	0.000	0.	0.	0.00	0.000
64		6.03	6.03	0.	113	0.00	934.		0.	0.	0.000	0.	0.	0.00	0.000
65		6.03	6.03	0.	90	0.00	743.		0.	0.	0.000	0.	0.	0.00	0.000
66		6.03	6.03	0.	111	0.00	924.		0.	0.	0.000	0.	0.	0.00	0.000
67		6.03	6.03	0.	70	0.00	584.		0.	0.	0.000	0.	0.	0.00	0.000
68		6.03	6.03	0.	90	0.00	750.		0.	0.	0.000	0.	0.	0.00	0.000
69		6.03	6.03	0.	12	0.00	97.		0.	0.	0.000	0.	0.	0.00	0.000
70		6.03	6.03	0.	29	0.00	242.		0.	0.	0.000	0.	0.	0.00	0.000
71		6.03	6.03	0.	49	0.00	407.		0.	0.	0.000	0.	0.	0.00	0.000
72		6.03	6.03	0.	46	0.00	384.		0.	0.	0.000	0.	0.	0.00	0.000
73		6.03	6.03	0.	60	0.00	495.		0.	0.	0.000	0.	0.	0.00	0.000
74		6.03	6.03	0.	67	0.00	553.		0.	0.	0.000	0.	0.	0.00	0.000
75		6.03	12.63	0.	58	0.00	484.		0.	0.	0.000	0.	0.	0.00	0.000
76		6.03	12.63	0.	41	0.00	336.		0.	0.	0.000	0.	0.	0.00	0.000
77		6.03	12.63	0.	20	0.00	170.		0.	0.	0.000	0.	0.	0.00	0.000
78		6.03	7.68	0.	41	0.00	341.		0.	0.	0.000	0.	0.	0.00	0.000
79		6.03	7.68	0.	22	0.00	183.		0.	0.	0.000	0.	0.	0.00	0.000
80		6.03	7.68	0.	-1	0.03	-1.		0.	0.	0.000	0.	0.	0.00	0.000
81		6.03	6.03	0.	37	0.00	309.		0.	0.	0.000	0.	0.	0.00	0.000
82		6.03	6.03	0.	19	0.00	158.		0.	0.	0.000	0.	0.	0.00	0.000
83		6.03	6.03	0.	-1	0.03	0.		0.	0.	0.000	0.	0.	0.00	0.000
84		6.03	6.03	0.	34	0.00	278.		0.	0.	0.000	0.	0.	0.00	0.000
85		6.03	6.03	0.	20	0.00	164.		0.	0.	0.000	0.	0.	0.00	0.000
86		6.03	6.03	0.	5	0.00	41.		0.	0.	0.000	0.	0.	0.00	0.000
87		6.03	6.03	0.	21	0.00	174.		0.	0.	0.000	0.	0.	0.00	0.000
88		6.03	6.03	0.	20	0.00	168.		0.	0.	0.000	0.	0.	0.00	0.000
89		6.03	6.03	0.	11	0.00	91.		0.	0.	0.000	0.	0.	0.00	0.000
90		6.03	6.03	0.	9	0.00	78.		0.	0.	0.000	0.	0.	0.00	0.000
91		6.03	6.03	0.	9	0.00	78.		0.	0.	0.000	0.	0.	0.00	0.000
92		6.03	6.03	0.	8	0.00	64.		0.	0.	0.000	0.	0.	0.00	0.000
93		16.76	16.76	0.	61	0.00	183.		0.	0.	0.000	0.	0.	0.00	0.000
94		16.76	16.76	0.	62	0.00	185.		0.	0.	0.000	0.	0.	0.00	0.000
95		16.76	16.76	0.	110	0.00	327.		0.	0.	0.000	0.	0.	0.00	0.000
96		16.76	16.76	0.	109	0.00	325.		0.	0.	0.000	0.	0.	0.00	0.000
97		16.76	16.76	0.	80	0.00	238.		0.	0.	0.000	0.	0.	0.00	0.000
98		16.76	16.76	0.	80	0.00	238.		0.	0.	0.000	0.	0.	0.00	0.000
99		16.76	16.76	0.	99	0.00	294.		0.	0.	0.000	0.	0.	0.00	0.000
100		16.76	16.76	0.	99	0.00	294.		0.	0.	0.000	0.	0.	0.00	0.000
101		16.76	16.76	0.	99	0.00	296.		0.	0.	0.000	0.	0.	0.00	0.000
102		16.76	16.76	0.	99	0.00	296.		0.	0.	0.000	0.	0.	0.00	0.000
103		16.76	16.76	0.	97	0.00	289.		0.	0.	0.000	0.	0.	0.00	0.000
104		16.76	16.76	0.	97	0.00	289.		0.	0.	0.000	0.	0.	0.00	0.000
105		16.76	16.76	0.	94	0.00	282.		0.	0.	0.000	0.	0.	0.00	0.000
106		16.76	16.76	0.	94	0.00	282.		0.	0.	0.000	0.	0.	0.00	0.000
107		16.76	16.76	0.	79	0.00	236.		0.	0.	0.000	0.	0.	0.00	0.000
108		16.76	16.76	0.	79	0.00	236.		0.	0.	0.000	0.	0.	0.00	0.000
109		16.76	16.76	0.	108	0.00	321.		0.	0.	0.000	0.	0.	0.00	0.000

110		16.76	16.76	0.	107	0.00	320.		0.	0.	0.000	0.	0.	0.00	0.000
111		16.76	16.76	0.	62	0.00	185.		0.	0.	0.000	0.	0.	0.00	0.000
112		16.76	16.76	0.	63	0.00	187.		0.	0.	0.000	0.	0.	0.00	0.000
113		16.76	16.76	0.	62	0.00	185.		0.	0.	0.000	0.	0.	0.00	0.000
114		16.76	16.76	0.	62	0.00	185.		0.	0.	0.000	0.	0.	0.00	0.000
115		16.76	16.76	0.	62	0.00	185.		0.	0.	0.000	0.	0.	0.00	0.000
116		16.76	16.76	0.	109	0.00	325.		0.	0.	0.000	0.	0.	0.00	0.000
117		16.76	16.76	0.	109	0.00	325.		0.	0.	0.000	0.	0.	0.00	0.000
118		16.76	16.76	0.	109	0.00	325.		0.	0.	0.000	0.	0.	0.00	0.000
119		16.76	16.76	0.	80	0.00	238.		0.	0.	0.000	0.	0.	0.00	0.000
120		16.76	16.76	0.	80	0.00	238.		0.	0.	0.000	0.	0.	0.00	0.000
121		16.76	16.76	0.	80	0.00	238.		0.	0.	0.000	0.	0.	0.00	0.000
122		16.76	16.76	0.	99	0.00	294.		0.	0.	0.000	0.	0.	0.00	0.000
123		16.76	16.76	0.	99	0.00	294.		0.	0.	0.000	0.	0.	0.00	0.000
124		16.76	16.76	0.	99	0.00	294.		0.	0.	0.000	0.	0.	0.00	0.000
125		16.76	16.76	0.	99	0.00	296.		0.	0.	0.000	0.	0.	0.00	0.000
126		16.76	16.76	0.	99	0.00	296.		0.	0.	0.000	0.	0.	0.00	0.000
127		16.76	16.76	0.	99	0.00	296.		0.	0.	0.000	0.	0.	0.00	0.000
128		16.76	16.76	0.	97	0.00	289.		0.	0.	0.000	0.	0.	0.00	0.000
129		16.76	16.76	0.	97	0.00	289.		0.	0.	0.000	0.	0.	0.00	0.000
130		16.76	16.76	0.	97	0.00	289.		0.	0.	0.000	0.	0.	0.00	0.000
131		16.76	16.76	0.	94	0.00	282.		0.	0.	0.000	0.	0.	0.00	0.000
132		16.76	16.76	0.	94	0.00	282.		0.	0.	0.000	0.	0.	0.00	0.000
133		16.76	16.76	0.	94	0.00	282.		0.	0.	0.000	0.	0.	0.00	0.000
134		16.76	16.76	0.	79	0.00	236.		0.	0.	0.000	0.	0.	0.00	0.000
135		16.76	16.76	0.	79	0.00	236.		0.	0.	0.000	0.	0.	0.00	0.000
136		16.76	16.76	0.	79	0.00	236.		0.	0.	0.000	0.	0.	0.00	0.000
137		16.76	16.76	0.	107	0.00	320.		0.	0.	0.000	0.	0.	0.00	0.000
138		16.76	16.76	0.	107	0.00	320.		0.	0.	0.000	0.	0.	0.00	0.000
139		16.76	16.76	0.	107	0.00	320.		0.	0.	0.000	0.	0.	0.00	0.000
140		16.76	16.76	0.	63	0.00	187.		0.	0.	0.000	0.	0.	0.00	0.000
141		16.76	16.76	0.	63	0.00	187.		0.	0.	0.000	0.	0.	0.00	0.000
142		16.76	16.76	0.	63	0.00	187.		0.	0.	0.000	0.	0.	0.00	0.000
143		16.76	16.76	0.	62	0.00	185.		0.	0.	0.000	0.	0.	0.00	0.000
144		16.76	16.76	0.	56	0.00	169.		0.	0.	0.000	0.	0.	0.00	0.000
145		16.76	16.76	0.	109	0.00	325.		0.	0.	0.000	0.	0.	0.00	0.000
147		16.76	16.76	0.	80	0.00	238.		0.	0.	0.000	0.	0.	0.00	0.000
148		16.76	16.76	0.	67	0.00	201.		0.	0.	0.000	0.	0.	0.00	0.000
149		16.76	16.76	0.	99	0.00	294.		0.	0.	0.000	0.	0.	0.00	0.000
150		16.76	16.76	0.	86	0.00	255.		0.	0.	0.000	0.	0.	0.00	0.000
151		16.76	16.76	0.	99	0.00	296.		0.	0.	0.000	0.	0.	0.00	0.000
152		16.76	16.76	0.	85	0.00	252.		0.	0.	0.000	0.	0.	0.00	0.000
153		16.76	16.76	0.	97	0.00	289.		0.	0.	0.000	0.	0.	0.00	0.000
154		16.76	16.76	0.	83	0.00	249.		0.	0.	0.000	0.	0.	0.00	0.000
155		16.76	16.76	0.	94	0.00	282.		0.	0.	0.000	0.	0.	0.00	0.000
156		16.76	16.76	0.	81	0.00	242.		0.	0.	0.000	0.	0.	0.00	0.000
157		16.76	16.76	0.	79	0.00	236.		0.	0.	0.000	0.	0.	0.00	0.000
158		16.76	16.76	0.	67	0.00	199.		0.	0.	0.000	0.	0.	0.00	0.000
159		16.76	16.76	0.	107	0.00	320.		0.	0.	0.000	0.	0.	0.00	0.000
161		16.76	16.76	0.	63	0.00	187.		0.	0.	0.000	0.	0.	0.00	0.000
162		16.76	16.76	0.	57	0.00	169.		0.	0.	0.000	0.	0.	0.00	0.000
199		16.76	16.76	0.	101	0.00	300.		0.	0.	0.000	0.	0.	0.00	0.000
200		16.76	16.76	0.	105	0.00	313.		0.	0.	0.000	0.	0.	0.00	0.000
201		16.76	16.76	0.	42	0.00	125.		0.	0.	0.000	0.	0.	0.00	0.000
202		16.76	16.76	0.	40	0.00	120.		0.	0.	0.000	0.	0.	0.00	0.000
203		16.76	16.76	0.	106	0.00	316.		0.	0.	0.000	0.	0.	0.00	0.000
204		16.76	16.76	0.	103	0.00	309.		0.	0.	0.000	0.	0.	0.00	0.000

ARMATURA INFERIORE VERTICALE

GUSCI			COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE					
	Af	Afc	Mom	Nor	sigC	sigF	Mom	Nor	WkF	Mom	Nor	sigC	WkP		
1		5.89	5.89	0.	8	0.00	69.		0.	0.	0.000	0.	0.	0.00	0.000
2		5.89	5.89	0.	8	0.00	71.		0.	0.	0.000	0.	0.	0.00	0.000
3		5.89	5.89	0.	5	0.00	44.		0.	0.	0.000	0.	0.	0.00	0.000
4		5.89	5.89	0.	14	0.00	119.		0.	0.	0.000	0.	0.	0.00	0.000
5		5.89	5.89	0.	2	0.00	17.		0.	0.	0.000	0.	0.	0.00	0.000
6		5.89	5.89	0.	1	0.00	7.		0.	0.	0.000	0.	0.	0.00	0.000
7		5.89	5.89	0.	0.	0.00	0.		0.	0.	0.000	0.	0.	0.00	0.000
8		5.89	5.89	0.	-2	0.08	-1.		0.	0.	0.000	0.	0.	0.00	0.000
9		5.89	5.89	0.	-1	0.04	-1.		0.	0.	0.000	0.	0.	0.00	0.000
10		5.89	5.89	0.	-4	0.17	-3.		0.	0.	0.000	0.	0.	0.00	0.000
11		5.89	5.89	0.	-1	0.05	-1.		0.	0.	0.000	0.	0.	0.00	0.000
12		5.89	5.89	0.	-4	0.18	-3.		0.	0.	0.000	0.	0.	0.00	0.000
13		5.89	5.89	0.	0.	0.00	0.		0.	0.	0.000	0.	0.	0.00	0.000
14		5.89	5.89	0.	-2	0.09	-1.		0.	0.	0.000	0.	0.	0.00	0.000

15		5.89	5.89	0.	2	0.00	15.	0.	0.	0.000	0.	0.	0.00	0.000
16		5.89	5.89	0.	1	0.00	10.	0.	0.	0.000	0.	0.	0.00	0.000
17		5.89	5.89	0.	4	0.00	36.	0.	0.	0.000	0.	0.	0.00	0.000
18		5.89	5.89	0.	11	0.00	95.	0.	0.	0.000	0.	0.	0.00	0.000
19		5.89	5.89	0.	8	0.00	66.	0.	0.	0.000	0.	0.	0.00	0.000
20		5.89	5.89	0.	6	0.00	49.	0.	0.	0.000	0.	0.	0.00	0.000
21		6.09	6.09	0.	53	0.00	431.	0.	0.	0.000	0.	0.	0.00	0.000
22		6.09	6.09	0.	37	0.00	305.	0.	0.	0.000	0.	0.	0.00	0.000
23		6.09	6.09	0.	18	0.00	147.	0.	0.	0.000	0.	0.	0.00	0.000
24		6.09	6.09	0.	10	0.00	81.	0.	0.	0.000	0.	0.	0.00	0.000
25		6.09	6.09	0.	4	0.00	36.	0.	0.	0.000	0.	0.	0.00	0.000
26		6.09	6.09	0.	13	0.00	110.	0.	0.	0.000	0.	0.	0.00	0.000
27		6.09	6.09	0.	53	0.00	432.	0.	0.	0.000	0.	0.	0.00	0.000
28		6.09	6.09	0.	37	0.00	301.	0.	0.	0.000	0.	0.	0.00	0.000
29		6.09	6.09	0.	17	0.00	138.	0.	0.	0.000	0.	0.	0.00	0.000
30		6.09	6.09	0.	9	0.00	71.	0.	0.	0.000	0.	0.	0.00	0.000
31		11.98	11.98	0.	5	0.00	19.	0.	0.	0.000	0.	0.	0.00	0.000
32		9.04	9.04	0.	12	0.00	69.	0.	0.	0.000	0.	0.	0.00	0.000
33		10.18	10.18	0.	4	0.00	22.	0.	0.	0.000	0.	0.	0.00	0.000
34		10.18	10.18	0.	1	0.00	3.	0.	0.	0.000	0.	0.	0.00	0.000
35		6.09	6.09	0.	27	0.00	222.	0.	0.	0.000	0.	0.	0.00	0.000
36		6.09	6.09	0.	25	0.00	204.	0.	0.	0.000	0.	0.	0.00	0.000
37		6.09	6.09	0.	51	0.00	417.	0.	0.	0.000	0.	0.	0.00	0.000
38		6.09	6.09	0.	47	0.00	382.	0.	0.	0.000	0.	0.	0.00	0.000
39		6.09	6.09	0.	56	0.00	461.	0.	0.	0.000	0.	0.	0.00	0.000
40		6.09	6.09	0.	62	0.00	513.	0.	0.	0.000	0.	0.	0.00	0.000
41		6.09	6.09	0.	62	0.00	507.	0.	0.	0.000	0.	0.	0.00	0.000
42		6.09	6.09	0.	58	0.00	478.	0.	0.	0.000	0.	0.	0.00	0.000
43		6.09	6.09	0.	57	0.00	470.	0.	0.	0.000	0.	0.	0.00	0.000
44		6.09	6.09	0.	57	0.00	470.	0.	0.	0.000	0.	0.	0.00	0.000
45		6.09	6.09	0.	61	0.00	499.	0.	0.	0.000	0.	0.	0.00	0.000
46		6.09	6.09	0.	64	0.00	525.	0.	0.	0.000	0.	0.	0.00	0.000
47		6.09	6.09	0.	50	0.00	407.	0.	0.	0.000	0.	0.	0.00	0.000
48		6.09	6.09	0.	64	0.00	526.	0.	0.	0.000	0.	0.	0.00	0.000
49		6.09	6.09	0.	67	0.00	551.	0.	0.	0.000	0.	0.	0.00	0.000
50		6.09	6.09	0.	49	0.00	400.	0.	0.	0.000	0.	0.	0.00	0.000
51		6.09	6.09	0.	64	0.00	523.	0.	0.	0.000	0.	0.	0.00	0.000
52		6.09	6.09	0.	68	0.00	560.	0.	0.	0.000	0.	0.	0.00	0.000
53		6.09	6.09	0.	48	0.00	391.	0.	0.	0.000	0.	0.	0.00	0.000
54		6.09	6.09	0.	59	0.00	481.	0.	0.	0.000	0.	0.	0.00	0.000
55		6.09	6.09	0.	65	0.00	537.	0.	0.	0.000	0.	0.	0.00	0.000
56		6.09	6.09	0.	43	0.00	351.	0.	0.	0.000	0.	0.	0.00	0.000
57		6.09	6.09	0.	35	0.00	285.	0.	0.	0.000	0.	0.	0.00	0.000
58		6.09	7.97	0.	43	0.00	356.	0.	0.	0.000	0.	0.	0.00	0.000
59		6.09	7.97	0.	21	0.00	172.	0.	0.	0.000	0.	0.	0.00	0.000
60		10.18	10.18	0.	11	0.00	54.	0.	0.	0.000	0.	0.	0.00	0.000
61		10.18	17.72	0.	20	0.00	96.	0.	0.	0.000	0.	0.	0.00	0.000
62		10.18	17.72	0.	2	0.00	8.	0.	0.	0.000	0.	0.	0.00	0.000
63		6.09	6.09	0.	7	0.00	58.	0.	0.	0.000	0.	0.	0.00	0.000
64		6.09	6.09	0.	-4	0.08	-1.	0.	0.	0.000	0.	0.	0.00	0.000
65		6.09	6.09	0.	29	0.00	241.	0.	0.	0.000	0.	0.	0.00	0.000
66		6.09	6.09	0.	23	0.00	189.	0.	0.	0.000	0.	0.	0.00	0.000
67		6.09	6.09	0.	52	0.00	424.	0.	0.	0.000	0.	0.	0.00	0.000
68		6.09	6.09	0.	47	0.00	383.	0.	0.	0.000	0.	0.	0.00	0.000
69		6.09	6.09	0.	56	0.00	461.	0.	0.	0.000	0.	0.	0.00	0.000
70		6.09	6.09	0.	63	0.00	513.	0.	0.	0.000	0.	0.	0.00	0.000
71		6.09	6.09	0.	62	0.00	509.	0.	0.	0.000	0.	0.	0.00	0.000
72		6.09	6.09	0.	59	0.00	483.	0.	0.	0.000	0.	0.	0.00	0.000
73		6.09	6.09	0.	58	0.00	476.	0.	0.	0.000	0.	0.	0.00	0.000
74		6.09	6.09	0.	57	0.00	469.	0.	0.	0.000	0.	0.	0.00	0.000
75		6.09	6.09	0.	14	0.00	116.	0.	0.	0.000	0.	0.	0.00	0.000
76		6.09	13.63	0.	20	0.00	161.	0.	0.	0.000	0.	0.	0.00	0.000
77		6.09	13.63	0.	2	0.00	14.	0.	0.	0.000	0.	0.	0.00	0.000
78		6.09	6.09	0.	37	0.00	307.	0.	0.	0.000	0.	0.	0.00	0.000
79		6.09	6.09	0.	43	0.00	356.	0.	0.	0.000	0.	0.	0.00	0.000
80		6.09	6.09	0.	21	0.00	172.	0.	0.	0.000	0.	0.	0.00	0.000
81		6.09	6.09	0.	60	0.00	489.	0.	0.	0.000	0.	0.	0.00	0.000
82		6.09	6.09	0.	65	0.00	537.	0.	0.	0.000	0.	0.	0.00	0.000
83		6.09	6.09	0.	43	0.00	351.	0.	0.	0.000	0.	0.	0.00	0.000
84		6.09	6.09	0.	64	0.00	523.	0.	0.	0.000	0.	0.	0.00	0.000
85		6.09	6.09	0.	68	0.00	560.	0.	0.	0.000	0.	0.	0.00	0.000
86		6.09	6.09	0.	48	0.00	391.	0.	0.	0.000	0.	0.	0.00	0.000
87		6.09	6.09	0.	64	0.00	526.	0.	0.	0.000	0.	0.	0.00	0.000
88		6.09	6.09	0.	67	0.00	551.	0.	0.	0.000	0.	0.	0.00	0.000
89		6.09	6.09	0.	49	0.00	400.	0.	0.	0.000	0.	0.	0.00	0.000
90		6.09	6.09	0.	61	0.00	499.	0.	0.	0.000	0.	0.	0.00	0.000

91		6.09	6.09	0.	64	0.00	525.	0.	0.	0.000	0.	0.	0.00	0.000
92		6.09	6.09	0.	50	0.00	407.	0.	0.	0.000	0.	0.	0.00	0.000
93		16.36	16.36	0.	11	0.00	33.	0.	0.	0.000	0.	0.	0.00	0.000
94		16.36	16.36	0.	18	0.00	56.	0.	0.	0.000	0.	0.	0.00	0.000
95		16.36	16.36	0.	-11	0.07	-1.	0.	0.	0.000	0.	0.	0.00	0.000
96		16.36	16.36	0.	0.	0.00	1.	0.	0.	0.000	0.	0.	0.00	0.000
97		16.36	16.36	0.	-31	0.21	-3.	0.	0.	0.000	0.	0.	0.00	0.000
98		16.36	16.36	0.	-17	0.12	-2.	0.	0.	0.000	0.	0.	0.00	0.000
99		16.36	16.36	0.	-40	0.28	-4.	0.	0.	0.000	0.	0.	0.00	0.000
100		16.36	16.36	0.	-47	0.33	-5.	0.	0.	0.000	0.	0.	0.00	0.000
101		16.36	16.36	0.	-55	0.38	-6.	0.	0.	0.000	0.	0.	0.00	0.000
102		16.36	16.36	0.	-77	0.53	-8.	0.	0.	0.000	0.	0.	0.00	0.000
103		16.36	16.36	0.	-55	0.38	-6.	0.	0.	0.000	0.	0.	0.00	0.000
104		16.36	16.36	0.	-76	0.53	-8.	0.	0.	0.000	0.	0.	0.00	0.000
105		16.36	16.36	0.	-40	0.28	-4.	0.	0.	0.000	0.	0.	0.00	0.000
106		16.36	16.36	0.	-46	0.32	-5.	0.	0.	0.000	0.	0.	0.00	0.000
107		16.36	16.36	0.	-31	0.22	-3.	0.	0.	0.000	0.	0.	0.00	0.000
108		16.36	16.36	0.	-16	0.11	-2.	0.	0.	0.000	0.	0.	0.00	0.000
109		16.36	16.36	0.	-14	0.10	-2.	0.	0.	0.000	0.	0.	0.00	0.000
110		16.36	16.36	0.	3	0.00	9.	0.	0.	0.000	0.	0.	0.00	0.000
111		16.36	16.36	0.	4	0.00	13.	0.	0.	0.000	0.	0.	0.00	0.000
112		16.36	16.36	0.	21	0.00	66.	0.	0.	0.000	0.	0.	0.00	0.000
113		16.36	16.36	0.	17	0.00	52.	0.	0.	0.000	0.	0.	0.00	0.000
114		16.36	16.36	0.	13	0.00	40.	0.	0.	0.000	0.	0.	0.00	0.000
115		16.36	16.36	0.	-7	0.05	-1.	0.	0.	0.000	0.	0.	0.00	0.000
116		16.36	16.36	0.	-1	0.00	0.	0.	0.	0.000	0.	0.	0.00	0.000
117		16.36	16.36	0.	-5	0.04	-1.	0.	0.	0.000	0.	0.	0.00	0.000
118		16.36	16.36	0.	-26	0.18	-3.	0.	0.	0.000	0.	0.	0.00	0.000
119		16.36	16.36	0.	-23	0.16	-2.	0.	0.	0.000	0.	0.	0.00	0.000
120		16.36	16.36	0.	-31	0.21	-3.	0.	0.	0.000	0.	0.	0.00	0.000
121		16.36	16.36	0.	-53	0.37	-6.	0.	0.	0.000	0.	0.	0.00	0.000
122		16.36	16.36	0.	-62	0.43	-6.	0.	0.	0.000	0.	0.	0.00	0.000
123		16.36	16.36	0.	-75	0.52	-8.	0.	0.	0.000	0.	0.	0.00	0.000
124		16.36	16.36	0.	-98	0.68	-10.	0.	0.	0.000	0.	0.	0.00	0.000
125		16.36	16.36	0.	-96	0.66	-10.	0.	0.	0.000	0.	0.	0.00	0.000
126		16.36	16.36	0.	-107	0.74	-11.	0.	0.	0.000	0.	0.	0.00	0.000
127		16.36	16.36	0.	-115	0.79	-12.	0.	0.	0.000	0.	0.	0.00	0.000
128		16.36	16.36	0.	-97	0.67	-10.	0.	0.	0.000	0.	0.	0.00	0.000
129		16.36	16.36	0.	-108	0.74	-11.	0.	0.	0.000	0.	0.	0.00	0.000
130		16.36	16.36	0.	-115	0.79	-12.	0.	0.	0.000	0.	0.	0.00	0.000
131		16.36	16.36	0.	-62	0.43	-6.	0.	0.	0.000	0.	0.	0.00	0.000
132		16.36	16.36	0.	-75	0.52	-8.	0.	0.	0.000	0.	0.	0.00	0.000
133		16.36	16.36	0.	-98	0.68	-10.	0.	0.	0.000	0.	0.	0.00	0.000
134		16.36	16.36	0.	-22	0.15	-2.	0.	0.	0.000	0.	0.	0.00	0.000
135		16.36	16.36	0.	-31	0.21	-3.	0.	0.	0.000	0.	0.	0.00	0.000
136		16.36	16.36	0.	-53	0.37	-6.	0.	0.	0.000	0.	0.	0.00	0.000
137		16.36	16.36	0.	3	0.00	8.	0.	0.	0.000	0.	0.	0.00	0.000
138		16.36	16.36	0.	-5	0.04	-1.	0.	0.	0.000	0.	0.	0.00	0.000
139		16.36	16.36	0.	-26	0.18	-3.	0.	0.	0.000	0.	0.	0.00	0.000
140		16.36	16.36	0.	21	0.00	63.	0.	0.	0.000	0.	0.	0.00	0.000
141		16.36	18.25	0.	13	0.00	40.	0.	0.	0.000	0.	0.	0.00	0.000
142		16.36	18.25	0.	-7	0.05	-1.	0.	0.	0.000	0.	0.	0.00	0.000
143		16.36	16.36	0.	-177	1.22	-18.	0.	0.	0.000	0.	0.	0.00	0.000
144		16.36	16.36	0.	-204	1.41	-21.	0.	0.	0.000	0.	0.	0.00	0.000
145		16.36	16.36	0.	-199	1.37	-21.	0.	0.	0.000	0.	0.	0.00	0.000
147		16.36	16.36	0.	-223	1.54	-23.	0.	0.	0.000	0.	0.	0.00	0.000
148		16.36	16.36	0.	-242	1.67	-25.	0.	0.	0.000	0.	0.	0.00	0.000
149		16.36	16.36	0.	-224	1.55	-23.	0.	0.	0.000	0.	0.	0.00	0.000
150		16.36	16.36	0.	-241	1.66	-25.	0.	0.	0.000	0.	0.	0.00	0.000
151		16.36	16.36	0.	-224	1.55	-23.	0.	0.	0.000	0.	0.	0.00	0.000
152		16.36	16.36	0.	-241	1.66	-25.	0.	0.	0.000	0.	0.	0.00	0.000
153		16.36	16.36	0.	-224	1.55	-23.	0.	0.	0.000	0.	0.	0.00	0.000
154		16.36	16.36	0.	-241	1.66	-25.	0.	0.	0.000	0.	0.	0.00	0.000
155		16.36	16.36	0.	-224	1.55	-23.	0.	0.	0.000	0.	0.	0.00	0.000
156		16.36	16.36	0.	-241	1.66	-25.	0.	0.	0.000	0.	0.	0.00	0.000
157		16.36	16.36	0.	-223	1.54	-23.	0.	0.	0.000	0.	0.	0.00	0.000
158		16.36	16.36	0.	-242	1.67	-25.	0.	0.	0.000	0.	0.	0.00	0.000
159		16.36	16.36	0.	-199	1.37	-21.	0.	0.	0.000	0.	0.	0.00	0.000
161		16.36	16.36	0.	-177	1.22	-18.	0.	0.	0.000	0.	0.	0.00	0.000
162		16.36	16.36	0.	-204	1.41	-21.	0.	0.	0.000	0.	0.	0.00	0.000
199		16.36	16.36	0.	-210	1.45	-22.	0.	0.	0.000	0.	0.	0.00	0.000
200		16.36	16.36	0.	-269	1.86	-28.	0.	0.	0.000	0.	0.	0.00	0.000
201		16.36	16.36	0.	-230	1.59	-24.	0.	0.	0.000	0.	0.	0.00	0.000
202		16.36	16.36	0.	-230	1.59	-24.	0.	0.	0.000	0.	0.	0.00	0.000
203		16.36	16.36	0.	-269	1.86	-28.	0.	0.	0.000	0.	0.	0.00	0.000
204		16.36	16.36	0.	-210	1.45	-22.	0.	0.	0.000	0.	0.	0.00	0.000

ARMATURA SUPERIORE ORIZZONTALE

GUSCI	COMBINAZIONE RARA						COMB. FREQUENTE			COMB. QUASI PERMANENTE			
	Af	Afc	Mom	Nor	sigC	sigF	Mom	Nor	WkF	Mom	Nor	sigC	WkP
1	8.67	6.79	63	39	0.00	276.	0.	0.	0.000	0.	0.	0.00	0.000
2	14.33	6.79	1591	29	28.14	851.	0.	0.	0.000	0.	0.	0.00	0.000
3	8.67	6.79	32	58	0.00	361.	0.	0.	0.000	0.	0.	0.00	0.000
4	14.33	6.79	1968	53	34.03	1110.	0.	0.	0.000	0.	0.	0.00	0.000
5	8.67	6.79	30	64	0.00	393.	0.	0.	0.000	0.	0.	0.00	0.000
6	14.33	6.79	2392	54	41.82	1316.	0.	0.	0.000	0.	0.	0.00	0.000
7	8.67	6.79	31	66	0.00	406.	0.	0.	0.000	0.	0.	0.00	0.000
8	14.33	6.79	2630	54	46.23	1427.	0.	0.	0.000	0.	0.	0.00	0.000
9	8.67	6.79	32	66	0.00	404.	0.	0.	0.000	0.	0.	0.00	0.000
10	14.33	6.79	2732	53	48.18	1470.	0.	0.	0.000	0.	0.	0.00	0.000
11	8.67	6.79	34	64	0.00	396.	0.	0.	0.000	0.	0.	0.00	0.000
12	14.33	6.79	2713	52	47.86	1460.	0.	0.	0.000	0.	0.	0.00	0.000
13	8.67	6.79	34	63	0.00	393.	0.	0.	0.000	0.	0.	0.00	0.000
14	14.33	6.79	2576	52	45.35	1394.	0.	0.	0.000	0.	0.	0.00	0.000
15	8.67	6.79	32	64	0.00	395.	0.	0.	0.000	0.	0.	0.00	0.000
16	14.33	6.79	2332	54	40.72	1286.	0.	0.	0.000	0.	0.	0.00	0.000
17	8.67	6.79	33	57	0.00	355.	0.	0.	0.000	0.	0.	0.00	0.000
18	14.33	6.79	1890	52	32.63	1069.	0.	0.	0.000	0.	0.	0.00	0.000
19	8.67	6.79	64	41	0.00	290.	0.	0.	0.000	0.	0.	0.00	0.000
20	14.33	6.79	1599	30	28.27	856.	0.	0.	0.000	0.	0.	0.00	0.000
21	6.03	6.03	1456	63	35.41	2115.	0.	0.	0.000	0.	0.	0.00	0.000
22	6.03	6.03	1404	72	33.61	2134.	0.	0.	0.000	0.	0.	0.00	0.000
23	6.03	6.03	903	68	20.22	1566.	0.	0.	0.000	0.	0.	0.00	0.000
24	6.03	6.03	1510	66	36.74	2194.	0.	0.	0.000	0.	0.	0.00	0.000
25	6.03	6.03	969	62	22.49	1578.	0.	0.	0.000	0.	0.	0.00	0.000
26	6.03	6.03	236	59	0.00	773.	0.	0.	0.000	0.	0.	0.00	0.000
27	6.03	6.03	1451	64	35.28	2114.	0.	0.	0.000	0.	0.	0.00	0.000
28	6.03	6.03	1401	72	33.54	2131.	0.	0.	0.000	0.	0.	0.00	0.000
29	6.03	6.03	903	68	20.25	1562.	0.	0.	0.000	0.	0.	0.00	0.000
30	6.03	6.03	1511	65	36.79	2189.	0.	0.	0.000	0.	0.	0.00	0.000
31	6.03	6.03	970	60	22.60	1569.	0.	0.	0.000	0.	0.	0.00	0.000
32	6.03	6.03	237	58	0.00	761.	0.	0.	0.000	0.	0.	0.00	0.000
33	7.65	6.03	3892	98	22.02	2113.	0.	0.	0.000	0.	0.	0.00	0.000
34	6.03	6.03	2663	112	13.45	2205.	0.	0.	0.000	0.	0.	0.00	0.000
35	6.03	6.03	2640	89	15.18	2004.	0.	0.	0.000	0.	0.	0.00	0.000
36	6.03	6.03	2348	111	10.51	2053.	0.	0.	0.000	0.	0.	0.00	0.000
37	6.03	6.03	1708	71	8.72	1406.	0.	0.	0.000	0.	0.	0.00	0.000
38	6.03	6.03	1745	91	6.80	1595.	0.	0.	0.000	0.	0.	0.00	0.000
39	6.03	6.03	264	12	1.27	223.	0.	0.	0.000	0.	0.	0.00	0.000
40	6.03	6.03	512	29	1.62	490.	0.	0.	0.000	0.	0.	0.00	0.000
41	6.03	6.03	887	49	3.01	838.	0.	0.	0.000	0.	0.	0.00	0.000
42	6.03	6.03	1056	47	5.11	893.	0.	0.	0.000	0.	0.	0.00	0.000
43	6.03	6.03	1205	60	5.05	1078.	0.	0.	0.000	0.	0.	0.00	0.000
44	6.03	6.03	1280	67	4.94	1173.	0.	0.	0.000	0.	0.	0.00	0.000
45	6.03	6.03	247	9	1.33	196.	0.	0.	0.000	0.	0.	0.00	0.000
46	6.03	6.03	246	9	1.33	196.	0.	0.	0.000	0.	0.	0.00	0.000
47	6.03	6.03	231	8	1.33	175.	0.	0.	0.000	0.	0.	0.00	0.000
48	6.03	6.03	534	21	2.82	430.	0.	0.	0.000	0.	0.	0.00	0.000
49	6.03	6.03	529	20	2.84	422.	0.	0.	0.000	0.	0.	0.00	0.000
50	6.03	6.03	471	11	3.04	315.	0.	0.	0.000	0.	0.	0.00	0.000
51	6.03	6.03	968	34	5.49	743.	0.	0.	0.000	0.	0.	0.00	0.000
52	6.03	6.03	898	20	5.85	592.	0.	0.	0.000	0.	0.	0.00	0.000
53	6.03	6.03	806	5	5.77	425.	0.	0.	0.000	0.	0.	0.00	0.000
54	6.03	6.03	1665	37	10.82	1104.	0.	0.	0.000	0.	0.	0.00	0.000
55	6.03	6.03	1604	19	11.18	922.	0.	0.	0.000	0.	0.	0.00	0.000
56	6.03	6.03	1477	-1	10.81	697.	0.	0.	0.000	0.	0.	0.00	0.000
57	7.65	6.03	3080	41	19.19	1432.	0.	0.	0.000	0.	0.	0.00	0.000
58	7.65	6.03	3144	22	20.28	1335.	0.	0.	0.000	0.	0.	0.00	0.000
59	7.65	6.03	3175	-1	21.08	1199.	0.	0.	0.000	0.	0.	0.00	0.000
60	12.49	6.03	5763	58	29.90	1582.	0.	0.	0.000	0.	0.	0.00	0.000
61	12.49	6.03	6368	41	33.81	1657.	0.	0.	0.000	0.	0.	0.00	0.000
62	12.49	6.03	7153	21	38.68	1768.	0.	0.	0.000	0.	0.	0.00	0.000
63	6.03	6.03	3895	99	24.65	2677.	0.	0.	0.000	0.	0.	0.00	0.000
64	6.03	6.03	2667	113	13.39	2214.	0.	0.	0.000	0.	0.	0.00	0.000
65	6.03	6.03	2644	90	15.20	2008.	0.	0.	0.000	0.	0.	0.00	0.000
66	6.03	6.03	2352	111	10.53	2057.	0.	0.	0.000	0.	0.	0.00	0.000
67	6.03	6.03	1712	70	8.77	1406.	0.	0.	0.000	0.	0.	0.00	0.000
68	6.03	6.03	1749	90	6.89	1594.	0.	0.	0.000	0.	0.	0.00	0.000
69	6.03	6.03	264	12	1.28	224.	0.	0.	0.000	0.	0.	0.00	0.000
70	6.03	6.03	514	29	1.64	491.	0.	0.	0.000	0.	0.	0.00	0.000
71	6.03	6.03	890	49	3.07	837.	0.	0.	0.000	0.	0.	0.00	0.000

72		6.03	6.03	1059	46	5.16	892.	0.	0.	0.000	0.	0.	0.00	0.000
73		6.03	6.03	1208	60	5.12	1077.	0.	0.	0.000	0.	0.	0.00	0.000
74		6.03	6.03	1283	67	5.02	1172.	0.	0.	0.000	0.	0.	0.00	0.000
75		12.63	6.03	5765	58	29.79	1566.	0.	0.	0.000	0.	0.	0.00	0.000
76		12.63	6.03	6371	41	33.69	1641.	0.	0.	0.000	0.	0.	0.00	0.000
77		12.63	6.03	7154	20	38.54	1750.	0.	0.	0.000	0.	0.	0.00	0.000
78		7.68	6.03	3083	41	19.18	1427.	0.	0.	0.000	0.	0.	0.00	0.000
79		7.68	6.03	3147	22	20.26	1330.	0.	0.	0.000	0.	0.	0.00	0.000
80		7.68	6.03	3177	-1	21.06	1194.	0.	0.	0.000	0.	0.	0.00	0.000
81		6.03	6.03	1669	37	10.85	1105.	0.	0.	0.000	0.	0.	0.00	0.000
82		6.03	6.03	1607	19	11.21	925.	0.	0.	0.000	0.	0.	0.00	0.000
83		6.03	6.03	1480	-1	10.84	698.	0.	0.	0.000	0.	0.	0.00	0.000
84		6.03	6.03	970	34	5.53	743.	0.	0.	0.000	0.	0.	0.00	0.000
85		6.03	6.03	900	20	5.87	593.	0.	0.	0.000	0.	0.	0.00	0.000
86		6.03	6.03	808	5	5.79	427.	0.	0.	0.000	0.	0.	0.00	0.000
87		6.03	6.03	535	21	2.83	431.	0.	0.	0.000	0.	0.	0.00	0.000
88		6.03	6.03	530	20	2.86	422.	0.	0.	0.000	0.	0.	0.00	0.000
89		6.03	6.03	472	11	3.05	316.	0.	0.	0.000	0.	0.	0.00	0.000
90		6.03	6.03	247	9	1.34	196.	0.	0.	0.000	0.	0.	0.00	0.000
91		6.03	6.03	247	9	1.34	196.	0.	0.	0.000	0.	0.	0.00	0.000
92		6.03	6.03	231	8	1.34	175.	0.	0.	0.000	0.	0.	0.00	0.000
93		16.76	16.76	5043	61	1.43	408.	0.	0.	0.000	0.	0.	0.00	0.000
94		16.76	16.76	5120	62	1.46	413.	0.	0.	0.000	0.	0.	0.00	0.000
95		16.76	16.76	7744	110	1.25	672.	0.	0.	0.000	0.	0.	0.00	0.000
96		16.76	16.76	7877	109	1.46	676.	0.	0.	0.000	0.	0.	0.00	0.000
97		16.76	16.76	6870	80	2.14	544.	0.	0.	0.000	0.	0.	0.00	0.000
98		16.76	16.76	6870	80	2.14	544.	0.	0.	0.000	0.	0.	0.00	0.000
99		16.76	16.76	7437	99	1.66	625.	0.	0.	0.000	0.	0.	0.00	0.000
100		16.76	16.76	7437	99	1.66	625.	0.	0.	0.000	0.	0.	0.00	0.000
101		16.76	16.76	9447	99	3.37	717.	0.	0.	0.000	0.	0.	0.00	0.000
102		16.76	16.76	9447	99	3.37	717.	0.	0.	0.000	0.	0.	0.00	0.000
103		16.76	16.76	8589	97	2.79	672.	0.	0.	0.000	0.	0.	0.00	0.000
104		16.76	16.76	8589	97	2.79	672.	0.	0.	0.000	0.	0.	0.00	0.000
105		16.76	16.76	7104	94	1.57	598.	0.	0.	0.000	0.	0.	0.00	0.000
106		16.76	16.76	7104	94	1.57	598.	0.	0.	0.000	0.	0.	0.00	0.000
107		16.76	16.76	7007	79	2.28	548.	0.	0.	0.000	0.	0.	0.00	0.000
108		16.76	16.76	7007	79	2.28	548.	0.	0.	0.000	0.	0.	0.00	0.000
109		16.76	16.76	7049	108	0.37	635.	0.	0.	0.000	0.	0.	0.00	0.000
110		16.76	16.76	7209	107	0.69	642.	0.	0.	0.000	0.	0.	0.00	0.000
111		16.76	16.76	4685	62	1.06	393.	0.	0.	0.000	0.	0.	0.00	0.000
112		16.76	16.76	4760	63	1.09	399.	0.	0.	0.000	0.	0.	0.00	0.000
113		16.76	16.76	5120	62	1.46	413.	0.	0.	0.000	0.	0.	0.00	0.000
114		16.76	16.76	5120	62	1.46	413.	0.	0.	0.000	0.	0.	0.00	0.000
115		16.76	16.76	5120	62	1.46	413.	0.	0.	0.000	0.	0.	0.00	0.000
116		16.76	16.76	7877	109	1.46	676.	0.	0.	0.000	0.	0.	0.00	0.000
117		16.76	16.76	7877	109	1.46	676.	0.	0.	0.000	0.	0.	0.00	0.000
118		16.76	16.76	7877	109	1.46	676.	0.	0.	0.000	0.	0.	0.00	0.000
119		16.76	16.76	6870	80	2.14	544.	0.	0.	0.000	0.	0.	0.00	0.000
120		16.76	16.76	6870	80	2.14	544.	0.	0.	0.000	0.	0.	0.00	0.000
121		16.76	16.76	6870	80	2.14	544.	0.	0.	0.000	0.	0.	0.00	0.000
122		16.76	16.76	7437	99	1.66	625.	0.	0.	0.000	0.	0.	0.00	0.000
123		16.76	16.76	7437	99	1.66	625.	0.	0.	0.000	0.	0.	0.00	0.000
124		16.76	16.76	7437	99	1.66	625.	0.	0.	0.000	0.	0.	0.00	0.000
125		16.76	16.76	9447	99	3.37	717.	0.	0.	0.000	0.	0.	0.00	0.000
126		16.76	16.76	9447	99	3.37	717.	0.	0.	0.000	0.	0.	0.00	0.000
127		16.76	16.76	9447	99	3.37	717.	0.	0.	0.000	0.	0.	0.00	0.000
128		16.76	16.76	8589	97	2.79	672.	0.	0.	0.000	0.	0.	0.00	0.000
129		16.76	16.76	8589	97	2.79	672.	0.	0.	0.000	0.	0.	0.00	0.000
130		16.76	16.76	8589	97	2.79	672.	0.	0.	0.000	0.	0.	0.00	0.000
131		16.76	16.76	7104	94	1.57	598.	0.	0.	0.000	0.	0.	0.00	0.000
132		16.76	16.76	7104	94	1.57	598.	0.	0.	0.000	0.	0.	0.00	0.000
133		16.76	16.76	7104	94	1.57	598.	0.	0.	0.000	0.	0.	0.00	0.000
134		16.76	16.76	7007	79	2.28	548.	0.	0.	0.000	0.	0.	0.00	0.000
135		16.76	16.76	7007	79	2.28	548.	0.	0.	0.000	0.	0.	0.00	0.000
136		16.76	16.76	7007	79	2.28	548.	0.	0.	0.000	0.	0.	0.00	0.000
137		16.76	16.76	7209	107	0.69	642.	0.	0.	0.000	0.	0.	0.00	0.000
138		16.76	16.76	7209	107	0.69	642.	0.	0.	0.000	0.	0.	0.00	0.000
139		16.76	16.76	7209	107	0.69	642.	0.	0.	0.000	0.	0.	0.00	0.000
140		16.76	16.76	4760	63	1.09	399.	0.	0.	0.000	0.	0.	0.00	0.000
141		16.76	16.76	4760	63	1.09	399.	0.	0.	0.000	0.	0.	0.00	0.000
142		16.76	16.76	4760	63	1.09	399.	0.	0.	0.000	0.	0.	0.00	0.000
143		16.76	16.76	5120	62	1.46	413.	0.	0.	0.000	0.	0.	0.00	0.000
144		16.76	16.76	5273	56	1.84	403.	0.	0.	0.000	0.	0.	0.00	0.000
145		16.76	16.76	7877	109	1.46	676.	0.	0.	0.000	0.	0.	0.00	0.000
147		16.76	16.76	6870	80	2.14	544.	0.	0.	0.000	0.	0.	0.00	0.000
148		16.76	16.76	7077	67	2.78	516.	0.	0.	0.000	0.	0.	0.00	0.000

149	16.76	16.76	7437	99	1.66	625.	0.	0.	0.000	0.	0.	0.00	0.000
150	16.76	16.76	7660	86	2.53	596.	0.	0.	0.000	0.	0.	0.00	0.000
151	16.76	16.76	9447	99	3.37	717.	0.	0.	0.000	0.	0.	0.00	0.000
152	16.76	16.76	9731	85	4.09	687.	0.	0.	0.000	0.	0.	0.00	0.000
153	16.76	16.76	8589	97	2.79	672.	0.	0.	0.000	0.	0.	0.00	0.000
154	16.76	16.76	8847	83	3.50	643.	0.	0.	0.000	0.	0.	0.00	0.000
155	16.76	16.76	7104	94	1.57	598.	0.	0.	0.000	0.	0.	0.00	0.000
156	16.76	16.76	7317	81	2.44	568.	0.	0.	0.000	0.	0.	0.00	0.000
157	16.76	16.76	7007	79	2.28	548.	0.	0.	0.000	0.	0.	0.00	0.000
158	16.76	16.76	7217	67	2.91	520.	0.	0.	0.000	0.	0.	0.00	0.000
159	16.76	16.76	7209	107	0.69	642.	0.	0.	0.000	0.	0.	0.00	0.000
161	16.76	16.76	4760	63	1.09	399.	0.	0.	0.000	0.	0.	0.00	0.000
162	16.76	16.76	4902	57	1.53	387.	0.	0.	0.000	0.	0.	0.00	0.000
199	16.76	16.76	6435	101	0.00	587.	0.	0.	0.000	0.	0.	0.00	0.000
200	16.76	16.76	7536	105	1.36	648.	0.	0.	0.000	0.	0.	0.00	0.000
201	16.76	16.76	6784	42	3.31	429.	0.	0.	0.000	0.	0.	0.00	0.000
202	16.76	16.76	6322	40	3.05	403.	0.	0.	0.000	0.	0.	0.00	0.000
203	16.76	16.76	8019	106	1.81	673.	0.	0.	0.000	0.	0.	0.00	0.000
204	16.76	16.76	7082	103	0.88	624.	0.	0.	0.000	0.	0.	0.00	0.000

ARMATURA SUPERIORE VERTICALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE			COMB. QUASI PERMANENTE							
	Af	Afc	Mom	Nor	sigC	sigF	Mom	Nor	WkF	Mom	Nor	sigC	WkP
1	5.89	5.89	38	8	0.00	115.	0.	0.	0.000	0.	0.	0.00	0.000
2	5.89	5.89	110	8	2.48	195.	0.	0.	0.000	0.	0.	0.00	0.000
3	5.89	5.89	32	5	0.39	83.	0.	0.	0.000	0.	0.	0.00	0.000
4	5.89	5.89	100	14	1.56	236.	0.	0.	0.000	0.	0.	0.00	0.000
5	5.89	5.89	25	2	0.56	45.	0.	0.	0.000	0.	0.	0.00	0.000
6	5.89	5.89	111	1	2.87	129.	0.	0.	0.000	0.	0.	0.00	0.000
7	5.89	5.89	22	0.	0.56	23.	0.	0.	0.000	0.	0.	0.00	0.000
8	5.89	5.89	115	-2	3.01	113.	0.	0.	0.000	0.	0.	0.00	0.000
9	5.89	5.89	18	-1	0.48	13.	0.	0.	0.000	0.	0.	0.00	0.000
10	5.89	5.89	117	-4	3.08	98.	0.	0.	0.000	0.	0.	0.00	0.000
11	5.89	5.89	21	-1	0.56	15.	0.	0.	0.000	0.	0.	0.00	0.000
12	5.89	5.89	119	-4	3.11	99.	0.	0.	0.000	0.	0.	0.00	0.000
13	5.89	5.89	23	0.	0.61	25.	0.	0.	0.000	0.	0.	0.00	0.000
14	5.89	5.89	118	-2	3.08	113.	0.	0.	0.000	0.	0.	0.00	0.000
15	5.89	5.89	26	2	0.60	44.	0.	0.	0.000	0.	0.	0.00	0.000
16	5.89	5.89	112	1	2.90	134.	0.	0.	0.000	0.	0.	0.00	0.000
17	5.89	5.89	33	4	0.57	74.	0.	0.	0.000	0.	0.	0.00	0.000
18	5.89	5.89	100	11	1.95	211.	0.	0.	0.000	0.	0.	0.00	0.000
19	5.89	5.89	38	8	0.06	112.	0.	0.	0.000	0.	0.	0.00	0.000
20	5.89	5.89	110	6	2.65	173.	0.	0.	0.000	0.	0.	0.00	0.000
21	6.09	6.09	130	53	0.00	584.	0.	0.	0.000	0.	0.	0.00	0.000
22	6.09	6.09	179	37	0.00	515.	0.	0.	0.000	0.	0.	0.00	0.000
23	6.09	6.09	141	18	2.43	306.	0.	0.	0.000	0.	0.	0.00	0.000
24	6.09	6.09	155	10	3.59	250.	0.	0.	0.000	0.	0.	0.00	0.000
25	6.09	6.09	140	4	3.46	187.	0.	0.	0.000	0.	0.	0.00	0.000
26	6.09	6.09	59	13	0.00	179.	0.	0.	0.000	0.	0.	0.00	0.000
27	6.09	6.09	130	53	0.00	584.	0.	0.	0.000	0.	0.	0.00	0.000
28	6.09	6.09	178	37	0.00	511.	0.	0.	0.000	0.	0.	0.00	0.000
29	6.09	6.09	140	17	2.55	296.	0.	0.	0.000	0.	0.	0.00	0.000
30	6.09	6.09	155	9	3.65	240.	0.	0.	0.000	0.	0.	0.00	0.000
31	11.98	11.98	140	5	2.42	98.	0.	0.	0.000	0.	0.	0.00	0.000
32	9.04	9.04	58	12	0.00	115.	0.	0.	0.000	0.	0.	0.00	0.000
33	10.18	10.18	1474	4	8.21	444.	0.	0.	0.000	0.	0.	0.00	0.000
34	10.18	10.18	1123	1	6.32	326.	0.	0.	0.000	0.	0.	0.00	0.000
35	6.09	6.09	1298	27	8.50	835.	0.	0.	0.000	0.	0.	0.00	0.000
36	6.09	6.09	977	25	6.15	665.	0.	0.	0.000	0.	0.	0.00	0.000
37	6.09	6.09	1023	51	4.29	905.	0.	0.	0.000	0.	0.	0.00	0.000
38	6.09	6.09	802	47	2.39	767.	0.	0.	0.000	0.	0.	0.00	0.000
39	6.09	6.09	667	56	0.00	783.	0.	0.	0.000	0.	0.	0.00	0.000
40	6.09	6.09	835	62	0.00	916.	0.	0.	0.000	0.	0.	0.00	0.000
41	6.09	6.09	958	62	1.58	969.	0.	0.	0.000	0.	0.	0.00	0.000
42	6.09	6.09	902	58	1.49	913.	0.	0.	0.000	0.	0.	0.00	0.000
43	6.09	6.09	1002	57	3.14	951.	0.	0.	0.000	0.	0.	0.00	0.000
44	6.09	6.09	864	57	0.99	887.	0.	0.	0.000	0.	0.	0.00	0.000
45	6.09	6.09	838	61	0.00	903.	0.	0.	0.000	0.	0.	0.00	0.000
46	6.09	6.09	1149	64	3.87	1075.	0.	0.	0.000	0.	0.	0.00	0.000
47	6.09	6.09	1704	50	10.32	1213.	0.	0.	0.000	0.	0.	0.00	0.000
48	6.09	6.09	1012	64	1.94	1014.	0.	0.	0.000	0.	0.	0.00	0.000
49	6.09	6.09	1337	67	5.50	1190.	0.	0.	0.000	0.	0.	0.00	0.000
50	6.09	6.09	1800	49	11.14	1251.	0.	0.	0.000	0.	0.	0.00	0.000
51	6.09	6.09	1178	64	4.24	1087.	0.	0.	0.000	0.	0.	0.00	0.000
52	6.09	6.09	1591	68	7.85	1316.	0.	0.	0.000	0.	0.	0.00	0.000

53		6.09	6.09	2064	48	13.27	1366.		0.	0.	0.000	0.	0.	0.00	0.000
54		6.09	6.09	1360	59	6.68	1128.		0.	0.	0.000	0.	0.	0.00	0.000
55		6.09	6.09	1848	65	10.35	1414.		0.	0.	0.000	0.	0.	0.00	0.000
56		6.09	6.09	2495	43	16.77	1530.		0.	0.	0.000	0.	0.	0.00	0.000
57		6.09	6.09	1792	35	11.86	1131.		0.	0.	0.000	0.	0.	0.00	0.000
58		7.97	6.09	2441	43	14.47	1156.		0.	0.	0.000	0.	0.	0.00	0.000
59		7.97	6.09	3179	21	20.18	1287.		0.	0.	0.000	0.	0.	0.00	0.000
60		10.18	10.18	2122	11	11.70	662.		0.	0.	0.000	0.	0.	0.00	0.000
61		17.72	10.18	3049	20	13.51	564.		0.	0.	0.000	0.	0.	0.00	0.000
62		17.72	10.18	4150	2	19.06	703.		0.	0.	0.000	0.	0.	0.00	0.000
63		6.09	6.09	1668	7	11.97	848.		0.	0.	0.000	0.	0.	0.00	0.000
64		6.09	6.09	1274	-4	9.33	577.		0.	0.	0.000	0.	0.	0.00	0.000
65		6.09	6.09	1378	29	8.99	892.		0.	0.	0.000	0.	0.	0.00	0.000
66		6.09	6.09	1028	23	6.65	674.		0.	0.	0.000	0.	0.	0.00	0.000
67		6.09	6.09	1028	52	4.22	915.		0.	0.	0.000	0.	0.	0.00	0.000
68		6.09	6.09	808	47	2.44	770.		0.	0.	0.000	0.	0.	0.00	0.000
69		6.09	6.09	668	56	0.00	783.		0.	0.	0.000	0.	0.	0.00	0.000
70		6.09	6.09	837	63	0.00	917.		0.	0.	0.000	0.	0.	0.00	0.000
71		6.09	6.09	961	62	1.57	973.		0.	0.	0.000	0.	0.	0.00	0.000
72		6.09	6.09	904	59	1.37	919.		0.	0.	0.000	0.	0.	0.00	0.000
73		6.09	6.09	1006	58	3.06	958.		0.	0.	0.000	0.	0.	0.00	0.000
74		6.09	6.09	868	57	1.13	888.		0.	0.	0.000	0.	0.	0.00	0.000
75		6.09	6.09	2363	14	16.85	1234.		0.	0.	0.000	0.	0.	0.00	0.000
76		13.63	6.09	3304	20	16.99	785.		0.	0.	0.000	0.	0.	0.00	0.000
77		13.63	6.09	4387	2	23.22	960.		0.	0.	0.000	0.	0.	0.00	0.000
78		6.09	6.09	1890	37	12.47	1200.		0.	0.	0.000	0.	0.	0.00	0.000
79		6.09	6.09	2548	43	17.15	1560.		0.	0.	0.000	0.	0.	0.00	0.000
80		6.09	6.09	3274	21	23.31	1721.		0.	0.	0.000	0.	0.	0.00	0.000
81		6.09	6.09	1362	60	6.60	1138.		0.	0.	0.000	0.	0.	0.00	0.000
82		6.09	6.09	1849	65	10.35	1414.		0.	0.	0.000	0.	0.	0.00	0.000
83		6.09	6.09	2495	43	16.78	1530.		0.	0.	0.000	0.	0.	0.00	0.000
84		6.09	6.09	1179	64	4.25	1087.		0.	0.	0.000	0.	0.	0.00	0.000
85		6.09	6.09	1590	68	7.85	1316.		0.	0.	0.000	0.	0.	0.00	0.000
86		6.09	6.09	2064	48	13.27	1366.		0.	0.	0.000	0.	0.	0.00	0.000
87		6.09	6.09	1012	64	1.95	1014.		0.	0.	0.000	0.	0.	0.00	0.000
88		6.09	6.09	1337	67	5.49	1190.		0.	0.	0.000	0.	0.	0.00	0.000
89		6.09	6.09	1800	49	11.14	1251.		0.	0.	0.000	0.	0.	0.00	0.000
90		6.09	6.09	838	61	0.00	904.		0.	0.	0.000	0.	0.	0.00	0.000
91		6.09	6.09	1149	64	3.86	1075.		0.	0.	0.000	0.	0.	0.00	0.000
92		6.09	6.09	1703	50	10.32	1213.		0.	0.	0.000	0.	0.	0.00	0.000
93		16.36	16.36	815	11	0.19	70.		0.	0.	0.000	0.	0.	0.00	0.000
94		16.36	16.36	1266	18	0.16	114.		0.	0.	0.000	0.	0.	0.00	0.000
95		16.36	16.36	865	-11	0.50	14.		0.	0.	0.000	0.	0.	0.00	0.000
96		16.36	16.36	1317	0.	0.77	62.		0.	0.	0.000	0.	0.	0.00	0.000
97		16.36	16.36	961	-31	0.49	1.		0.	0.	0.000	0.	0.	0.00	0.000
98		16.36	16.36	1404	-17	0.80	23.		0.	0.	0.000	0.	0.	0.00	0.000
99		16.36	16.36	953	-40	0.01	-8.		0.	0.	0.000	0.	0.	0.00	0.000
100		16.36	16.36	1456	-47	0.74	1.		0.	0.	0.000	0.	0.	0.00	0.000
101		16.36	16.36	992	-55	0.10	-10.		0.	0.	0.000	0.	0.	0.00	0.000
102		16.36	16.36	1541	-77	0.10	-14.		0.	0.	0.000	0.	0.	0.00	0.000
103		16.36	16.36	1062	-55	0.08	-10.		0.	0.	0.000	0.	0.	0.00	0.000
104		16.36	16.36	1625	-76	0.07	-14.		0.	0.	0.000	0.	0.	0.00	0.000
105		16.36	16.36	1138	-40	0.60	0.		0.	0.	0.000	0.	0.	0.00	0.000
106		16.36	16.36	1689	-46	0.83	3.		0.	0.	0.000	0.	0.	0.00	0.000
107		16.36	16.36	1210	-31	0.59	3.		0.	0.	0.000	0.	0.	0.00	0.000
108		16.36	16.36	1726	-16	1.03	40.		0.	0.	0.000	0.	0.	0.00	0.000
109		16.36	16.36	1245	-14	0.72	22.		0.	0.	0.000	0.	0.	0.00	0.000
110		16.36	16.36	1793	3	1.03	92.		0.	0.	0.000	0.	0.	0.00	0.000
111		16.36	16.36	1235	4	0.68	70.		0.	0.	0.000	0.	0.	0.00	0.000
112		16.36	16.36	1812	21	0.55	148.		0.	0.	0.000	0.	0.	0.00	0.000
113		16.36	16.36	2143	17	0.96	150.		0.	0.	0.000	0.	0.	0.00	0.000
114		16.36	16.36	3492	13	1.89	201.		0.	0.	0.000	0.	0.	0.00	0.000
115		16.36	16.36	5422	-7	3.25	235.		0.	0.	0.000	0.	0.	0.00	0.000
116		16.36	16.36	2222	-1	1.32	102.		0.	0.	0.000	0.	0.	0.00	0.000
117		16.36	16.36	3603	-5	2.17	154.		0.	0.	0.000	0.	0.	0.00	0.000
118		16.36	16.36	5545	-26	3.39	188.		0.	0.	0.000	0.	0.	0.00	0.000
119		16.36	16.36	2383	-23	1.42	52.		0.	0.	0.000	0.	0.	0.00	0.000
120		16.36	16.36	3793	-31	2.29	96.		0.	0.	0.000	0.	0.	0.00	0.000
121		16.36	16.36	5727	-53	3.42	129.		0.	0.	0.000	0.	0.	0.00	0.000
122		16.36	16.36	2469	-62	1.20	7.		0.	0.	0.000	0.	0.	0.00	0.000
123		16.36	16.36	3891	-75	1.96	24.		0.	0.	0.000	0.	0.	0.00	0.000
124		16.36	16.36	5870	-98	3.08	52.		0.	0.	0.000	0.	0.	0.00	0.000
125		16.36	16.36	2568	-96	1.38	0.		0.	0.	0.000	0.	0.	0.00	0.000
126		16.36	16.36	4009	-107	1.96	8.		0.	0.	0.000	0.	0.	0.00	0.000
127		16.36	16.36	5987	-115	3.02	37.		0.	0.	0.000	0.	0.	0.00	0.000
128		16.36	16.36	2652	-97	1.41	1.		0.	0.	0.000	0.	0.	0.00	0.000

129		16.36	16.36	4085	-108	1.99	9.	0.	0.	0.000	0.	0.	0.00	0.000
130		16.36	16.36	6045	-115	3.05	38.	0.	0.	0.000	0.	0.	0.00	0.000
131		16.36	16.36	2715	-62	1.33	10.	0.	0.	0.000	0.	0.	0.00	0.000
132		16.36	16.36	4143	-75	2.12	30.	0.	0.	0.000	0.	0.	0.00	0.000
133		16.36	16.36	6103	-98	3.24	59.	0.	0.	0.000	0.	0.	0.00	0.000
134		16.36	16.36	2730	-22	1.65	70.	0.	0.	0.000	0.	0.	0.00	0.000
135		16.36	16.36	4152	-31	2.52	112.	0.	0.	0.000	0.	0.	0.00	0.000
136		16.36	16.36	6120	-53	3.67	146.	0.	0.	0.000	0.	0.	0.00	0.000
137		16.36	16.36	2708	3	1.57	134.	0.	0.	0.000	0.	0.	0.00	0.000
138		16.36	16.36	4072	-5	2.44	176.	0.	0.	0.000	0.	0.	0.00	0.000
139		16.36	16.36	5876	-26	3.59	204.	0.	0.	0.000	0.	0.	0.00	0.000
140		16.36	16.36	2674	21	1.22	185.	0.	0.	0.000	0.	0.	0.00	0.000
141		18.25	16.36	3993	13	2.10	202.	0.	0.	0.000	0.	0.	0.00	0.000
142		18.25	16.36	5731	-7	3.29	224.	0.	0.	0.000	0.	0.	0.00	0.000
143		16.36	16.36	12377	-177	6.81	154.	0.	0.	0.000	0.	0.	0.00	0.000
144		16.36	16.36	17590	-204	10.16	307.	0.	0.	0.000	0.	0.	0.00	0.000
145		16.36	16.36	12130	-199	6.40	112.	0.	0.	0.000	0.	0.	0.00	0.000
147		16.36	16.36	11745	-223	5.94	74.	0.	0.	0.000	0.	0.	0.00	0.000
148		16.36	16.36	17658	-242	9.82	237.	0.	0.	0.000	0.	0.	0.00	0.000
149		16.36	16.36	11718	-224	5.91	73.	0.	0.	0.000	0.	0.	0.00	0.000
150		16.36	16.36	17599	-241	9.79	236.	0.	0.	0.000	0.	0.	0.00	0.000
151		16.36	16.36	11718	-224	5.91	73.	0.	0.	0.000	0.	0.	0.00	0.000
152		16.36	16.36	17599	-241	9.79	236.	0.	0.	0.000	0.	0.	0.00	0.000
153		16.36	16.36	11718	-224	5.91	73.	0.	0.	0.000	0.	0.	0.00	0.000
154		16.36	16.36	17599	-241	9.79	236.	0.	0.	0.000	0.	0.	0.00	0.000
155		16.36	16.36	11718	-224	5.91	73.	0.	0.	0.000	0.	0.	0.00	0.000
156		16.36	16.36	17599	-241	9.79	236.	0.	0.	0.000	0.	0.	0.00	0.000
157		16.36	16.36	11700	-223	5.91	73.	0.	0.	0.000	0.	0.	0.00	0.000
158		16.36	16.36	17626	-242	9.80	236.	0.	0.	0.000	0.	0.	0.00	0.000
159		16.36	16.36	11515	-199	5.98	94.	0.	0.	0.000	0.	0.	0.00	0.000
161		16.36	16.36	11523	-177	6.21	124.	0.	0.	0.000	0.	0.	0.00	0.000
162		16.36	16.36	16484	-204	9.40	262.	0.	0.	0.000	0.	0.	0.00	0.000
199		16.36	16.36	16643	-210	9.44	256.	0.	0.	0.000	0.	0.	0.00	0.000
200		16.36	16.36	18485	-269	10.11	221.	0.	0.	0.000	0.	0.	0.00	0.000
201		16.36	16.36	16309	-230	9.00	208.	0.	0.	0.000	0.	0.	0.00	0.000
202		16.36	16.36	16928	-230	9.44	231.	0.	0.	0.000	0.	0.	0.00	0.000
203		16.36	16.36	19201	-269	10.61	247.	0.	0.	0.000	0.	0.	0.00	0.000
204		16.36	16.36	17645	-210	10.14	297.	0.	0.	0.000	0.	0.	0.00	0.000

MACROGUSCIO spalla_02

COEF.	INFERIORE ORIZZONTALE							INFERIORE VERTICALE							
	GUSCI	spess	Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF	
205		140	16.76	16.76	0.	120.	0.00	0.18	16.36	16.36	0.	100.	0.00	0.15	
8															
206		140	16.76	16.76	0.	238.	0.00	0.35	16.36	16.36	0.	94.	0.00	0.14	
16															
207		140	16.76	16.76	0.	256.	0.00	0.38	16.36	16.36	0.	74.	0.00	0.11	
17															
208		140	16.76	16.76	0.	256.	0.00	0.38	16.36	16.36	0.	87.	0.00	0.13	
17															
209		140	16.76	16.76	0.	268.	0.00	0.40	16.36	16.36	0.	56.	0.00	0.09	
18															
210		140	16.76	16.76	0.	268.	0.00	0.40	16.36	16.36	0.	57.	0.00	0.09	
18															
211		140	16.76	16.76	0.	279.	0.00	0.42	16.36	16.36	0.	25.	0.00	0.04	
19															
212		140	16.76	16.76	0.	279.	0.00	0.42	16.36	16.36	0.	22.	0.00	0.03	
19															
213		140	16.76	16.76	0.	269.	0.00	0.40	16.36	16.36	0.	10.	0.00	0.01	
18															
214		140	16.76	16.76	0.	269.	0.00	0.40	16.36	16.36	0.	-12.	0.00	0.00	
18															
215		140	16.76	16.76	0.	264.	0.00	0.39	16.36	16.36	0.	41.	0.00	0.06	
17															
216		140	16.76	16.76	0.	264.	0.00	0.39	16.36	16.36	0.	34.	0.00	0.05	
17															
217		140	16.76	16.76	0.	255.	0.00	0.38	16.36	16.36	0.	58.	0.00	0.09	
17															
218		140	16.76	16.76	0.	255.	0.00	0.38	16.36	16.36	0.	65.	0.00	0.10	
17															

219		140		16.76	16.76	0.	281.	0.00	0.42		16.36	16.36	0.	69.	0.00	0.11	
19																	
220		140		16.76	16.76	0.	158.	0.00	0.24		16.36	16.36	0.	79.	0.00	0.12	
10																	
221		140		16.76	16.76	0.	120.	0.00	0.18		16.36	16.36	0.	126.	0.00	0.19	
9																	
222		140		16.76	16.76	0.	120.	0.00	0.18		16.36	16.36	0.	141.	0.00	0.22	
10																	
223		140		16.76	16.76	0.	120.	0.00	0.18		16.36	16.36	0.	97.	0.00	0.15	
8																	
224		140		16.76	16.76	0.	238.	0.00	0.35		16.36	16.36	0.	117.	0.00	0.18	
16																	
225		140		16.76	16.76	0.	238.	0.00	0.35		16.36	16.36	0.	131.	0.00	0.20	
16																	
226		140		16.76	16.76	0.	238.	0.00	0.35		16.36	16.36	0.	90.	0.00	0.14	
16																	
227		140		16.76	16.76	0.	256.	0.00	0.38		16.36	16.36	0.	107.	0.00	0.16	
17																	
228		140		16.76	16.76	0.	256.	0.00	0.38		16.36	16.36	0.	119.	0.00	0.18	
17																	
229		140		16.76	16.76	0.	256.	0.00	0.38		16.36	16.36	0.	81.	0.00	0.12	
17																	
230		140		16.76	16.76	0.	268.	0.00	0.40		16.36	16.36	0.	66.	0.00	0.10	
18																	
231		140		16.76	16.76	0.	268.	0.00	0.40		16.36	16.36	0.	73.	0.00	0.11	
18																	
232		140		16.76	16.76	0.	268.	0.00	0.40		16.36	16.36	0.	32.	0.00	0.05	
18																	
233		140		16.76	16.76	0.	279.	0.00	0.42		16.36	16.36	0.	20.	0.00	0.03	
19																	
234		140		16.76	16.76	0.	279.	0.00	0.42		16.36	16.36	0.	8.	0.00	0.01	
19																	
235		140		16.76	16.76	0.	279.	0.00	0.42		16.36	16.36	0.	25.	0.00	0.04	
19																	
236		140		16.76	16.76	0.	269.	0.00	0.40		16.36	16.36	0.	-18.	0.00	0.00	
18																	
237		140		16.76	16.76	0.	269.	0.00	0.40		16.36	16.36	0.	-13.	0.00	0.00	
18																	
238		140		16.76	16.76	0.	269.	0.00	0.40		16.36	16.36	0.	24.	0.00	0.04	
18																	
239		140		16.76	16.76	0.	264.	0.00	0.39		16.36	16.36	0.	42.	0.00	0.06	
17																	
240		140		16.76	16.76	0.	264.	0.00	0.39		16.36	16.36	0.	39.	0.00	0.06	
17																	
241		140		16.76	16.76	0.	264.	0.00	0.39		16.36	16.36	0.	29.	0.00	0.04	
17																	
242		140		16.76	16.76	0.	255.	0.00	0.38		16.36	16.36	0.	81.	0.00	0.12	
17																	
243		140		16.76	16.76	0.	255.	0.00	0.38		16.36	16.36	0.	95.	0.00	0.15	
17																	
244		140		16.76	16.76	0.	255.	0.00	0.38		16.36	16.36	0.	64.	0.00	0.10	
17																	
245		140		16.76	16.76	0.	281.	0.00	0.42		16.36	16.36	0.	90.	0.00	0.14	
19																	
246		140		16.76	16.76	0.	281.	0.00	0.42		16.36	16.36	0.	103.	0.00	0.16	
19																	
247		140		16.76	16.76	0.	281.	0.00	0.42		16.36	16.36	0.	73.	0.00	0.11	
19																	
248		140		16.76	16.76	0.	158.	0.00	0.24		16.36	16.36	0.	96.	0.00	0.15	
10																	
249		140		16.76	16.76	0.	158.	0.00	0.24		16.36	23.90	0.	111.	0.00	0.17	
10																	
250		140		16.76	16.76	0.	158.	0.00	0.24		16.36	23.90	0.	77.	0.00	0.12	
10																	
251		140		16.76	16.76	0.	120.	0.00	0.18		16.36	16.36	251.	28.	0.00	0.05	
8																	
252		140		16.76	16.76	0.	115.	0.00	0.17		16.36	16.36	0.	-60.	0.00	0.01	
8																	
253		140		16.76	16.76	0.	238.	0.00	0.35		16.36	16.36	372.	25.	0.00	0.05	
16																	
254		140		16.76	16.76	0.	256.	0.00	0.38		16.36	16.36	449.	23.	0.00	0.05	
17																	
255		140		16.76	16.76	0.	249.	0.00	0.37		16.36	16.36	0.	-96.	0.00	0.00	
17																	
256		140		16.76	16.76	0.	268.	0.00	0.40		16.36	16.36	449.	23.	0.00	0.05	
18																	

257		140		16.76	16.76	0.	258.	0.00	0.39		16.36	16.36	0.	-96.	0.00	0.00	
17																	
258		140		16.76	16.76	0.	279.	0.00	0.42		16.36	16.36	449.	23.	0.00	0.05	
19																	
259		140		16.76	16.76	0.	270.	0.00	0.40		16.36	16.36	0.	-96.	0.00	0.00	
18																	
260		140		16.76	16.76	0.	269.	0.00	0.40		16.36	16.36	449.	23.	0.00	0.05	
18																	
261		140		16.76	16.76	0.	251.	0.00	0.37		16.36	16.36	0.	-96.	0.00	0.00	
17																	
262		140		16.76	16.76	0.	264.	0.00	0.39		16.36	16.36	449.	23.	0.00	0.05	
17																	
263		140		16.76	16.76	0.	245.	0.00	0.37		16.36	16.36	0.	-96.	0.00	0.00	
16																	
264		140		16.76	16.76	0.	255.	0.00	0.38		16.36	16.36	449.	23.	0.00	0.05	
17																	
265		140		16.76	16.76	0.	246.	0.00	0.37		16.36	16.36	0.	-96.	0.00	0.00	
16																	
266		140		16.76	16.76	0.	281.	0.00	0.42		16.36	16.36	486.	23.	0.00	0.05	
19																	
267		140		16.76	16.76	0.	158.	0.00	0.24		16.36	16.36	518.	22.	0.00	0.05	
10																	
268		140		16.76	16.76	0.	158.	0.00	0.24		16.36	16.36	0.	-87.	0.00	0.00	
10																	
293		140		16.76	16.76	0.	255.	0.00	0.38		16.36	16.36	0.	-59.	0.00	0.00	
17																	
294		140		16.76	16.76	0.	274.	0.00	0.41		16.36	16.36	0.	-18.	0.00	0.00	
18																	
295		140		16.76	16.76	0.	196.	0.00	0.29		16.36	16.36	0.	-71.	0.00	0.00	
13																	
296		140		16.76	16.76	0.	136.	0.00	0.20		16.36	16.36	0.	-65.	0.00	0.00	
9																	
297		140		16.76	16.76	0.	235.	0.00	0.35		16.36	16.36	0.	-8.	0.00	0.00	
16																	
298		140		16.76	16.76	0.	218.	0.00	0.32		16.36	16.36	0.	-25.	0.00	0.00	
14																	
299		140		16.76	16.76	0.	119.	0.00	0.18		16.36	16.36	0.	84.	0.00	0.13	
8																	
300		140		16.76	16.76	0.	238.	0.00	0.35		16.36	16.36	0.	78.	0.00	0.12	
16																	
301		140		16.76	16.76	0.	282.	0.00	0.42		16.36	16.36	0.	62.	0.00	0.09	
19																	
302		140		16.76	16.76	0.	157.	0.00	0.23		16.36	16.36	0.	71.	0.00	0.11	
10																	
303		20		6.79	6.79	0.	60.	0.00	0.22		5.89	5.89	0.	14.	0.00	0.06	
10																	
304		20		6.79	6.79	0.	85.	0.00	0.31		5.89	5.89	0.	11.	0.00	0.05	
14																	
305		20		6.79	6.79	0.	93.	0.00	0.34		5.89	5.89	0.	9.	0.00	0.04	
15																	
306		20		6.79	14.33	0.	86.	0.00	0.32		5.89	5.89	0.	20.	0.00	0.08	
9																	
307		20		6.79	6.79	0.	99.	0.00	0.37		5.89	5.89	0.	5.	0.00	0.02	
16																	
308		20		6.79	14.33	0.	90.	0.00	0.33		5.89	5.89	0.	7.	0.00	0.03	
9																	
309		20		6.79	6.79	0.	107.	0.00	0.39		5.89	5.89	0.	4.	0.00	0.02	
17																	
310		20		6.79	14.33	0.	96.	0.00	0.35		5.89	5.89	0.	4.	0.00	0.02	
10																	
311		20		6.79	6.79	0.	112.	0.00	0.41		5.89	5.89	0.	-2.	0.00	0.01	
18																	
312		20		6.79	14.33	0.	100.	0.00	0.37		5.89	5.89	0.	3.	0.00	0.01	
11																	
313		20		6.79	6.79	0.	111.	0.00	0.41		5.89	5.89	0.	3.	0.00	0.01	
18																	
314		20		6.79	14.33	0.	100.	0.00	0.37		5.89	5.89	0.	8.	0.00	0.03	
11																	
315		20		6.79	6.79	0.	115.	0.00	0.42		5.89	5.89	0.	8.	0.00	0.04	
19																	
316		20		6.79	14.33	0.	104.	0.00	0.38		5.89	5.89	0.	20.	0.00	0.09	
11																	
317		20		6.79	6.79	0.	119.	0.00	0.44		5.89	5.89	0.	13.	0.00	0.05	
19																	
318		20		6.79	6.79	0.	81.	0.00	0.30		5.89	5.89	0.	18.	0.00	0.08	
13																	

319		20		6.03	6.03	0.	85.	0.00	0.35		6.09	6.09	0.	72.	0.00	0.30	
16																	
320		20		6.03	6.03	0.	100.	0.00	0.41		6.09	6.09	0.	62.	0.00	0.26	
18																	
321		20		6.03	6.03	0.	101.	0.00	0.42		6.09	6.09	0.	42.	0.00	0.17	
19																	
322		20		6.03	6.03	0.	94.	0.00	0.39		6.09	6.09	0.	21.	0.00	0.09	
17																	
323		20		6.03	6.03	0.	90.	0.00	0.37		6.09	6.09	0.	21.	0.00	0.09	
17																	
324		20		6.03	6.03	0.	90.	0.00	0.37		6.09	6.09	0.	30.	0.00	0.12	
17																	
325		20		6.03	6.03	0.	85.	0.00	0.35		6.09	6.09	0.	70.	0.00	0.29	
16																	
326		20		6.03	6.03	0.	98.	0.00	0.40		6.09	6.09	0.	60.	0.00	0.25	
18																	
327		20		6.03	6.03	0.	97.	0.00	0.40		6.09	6.09	0.	35.	0.00	0.15	
18																	
328		20		6.03	6.03	0.	87.	0.00	0.36		6.09	6.09	0.	18.	0.00	0.07	
16																	
329		20		6.03	6.03	0.	83.	0.00	0.34		11.98	11.98	0.	19.	0.00	0.04	
15																	
330		20		6.03	6.03	0.	83.	0.00	0.34		11.98	11.98	0.	24.	0.00	0.09	
15																	
331		20		6.79	14.33	0.	43.	0.00	0.16		5.89	5.89	0.	29.	0.00	0.12	
5																	
332		20		6.79	14.33	0.	80.	0.00	0.29		5.89	5.89	0.	30.	0.00	0.13	
8																	
333		20		6.79	14.33	0.	117.	0.00	0.43		5.89	5.89	0.	30.	0.00	0.13	
12																	
334		20		6.79	14.33	0.	64.	0.00	0.23		5.89	5.89	0.	31.	0.00	0.13	
7																	
335		40		6.03	6.03	0.	151.	0.00	0.63		6.09	6.09	0.	45.	0.00	0.18	
28																	
336		40		6.03	6.03	0.	167.	0.00	0.69		6.09	6.09	0.	36.	0.00	0.15	
31																	
337		40		6.03	6.03	0.	135.	0.00	0.56		6.09	6.09	0.	65.	0.00	0.27	
25																	
338		40		6.03	6.03	0.	158.	0.00	0.65		6.09	6.09	0.	56.	0.00	0.23	
29																	
339		40		6.03	6.03	0.	107.	0.00	0.44		6.09	6.09	0.	79.	0.00	0.33	
20																	
340		40		6.03	6.03	0.	133.	0.00	0.55		6.09	6.09	0.	75.	0.00	0.31	
25																	
341		40		6.03	6.03	0.	16.	0.00	0.07		6.09	6.09	0.	76.	0.00	0.31	
14																	
342		40		6.03	6.03	0.	45.	0.00	0.19		6.09	6.09	0.	88.	0.00	0.36	
16																	
343		40		6.03	6.03	0.	73.	0.00	0.30		6.09	6.09	0.	89.	0.00	0.36	
16																	
344		40		6.03	6.03	0.	64.	0.00	0.27		6.09	6.09	0.	79.	0.00	0.33	
14																	
345		40		6.03	6.03	0.	79.	0.00	0.33		6.09	6.09	0.	79.	0.00	0.32	
15																	
346		40		6.03	6.03	0.	101.	0.00	0.42		6.09	6.09	0.	82.	0.00	0.34	
19																	
347		40		6.03	12.63	0.	116.	0.00	0.48		6.09	6.09	0.	49.	0.00	0.20	
14																	
348		40		6.03	12.63	0.	88.	0.00	0.37		6.09	13.63	0.	54.	0.00	0.22	
11																	
349		40		6.03	12.63	0.	70.	0.00	0.29		6.09	13.63	0.	31.	0.00	0.13	
8																	
350		40		6.03	6.03	0.	92.	0.00	0.38		6.09	6.09	0.	70.	0.00	0.29	
17																	
351		40		6.03	6.03	0.	66.	0.00	0.27		6.09	6.09	0.	74.	0.00	0.31	
14																	
352		40		6.03	6.03	0.	44.	0.00	0.18		6.09	6.09	0.	44.	0.00	0.18	
8																	
353		40		6.03	6.03	0.	79.	0.00	0.33		6.09	6.09	0.	88.	0.00	0.36	
16																	
354		40		6.03	6.03	0.	52.	0.00	0.21		6.09	6.09	0.	89.	0.00	0.36	
16																	
355		40		6.03	6.03	0.	31.	0.00	0.13		6.09	6.09	0.	60.	0.00	0.25	
11																	
356		40		6.03	6.03	0.	60.	0.00	0.25		6.09	6.09	0.	90.	0.00	0.37	
16																	

357		40		6.03	6.03	0.	43.	0.00	0.18		6.09	6.09	0.	89.	0.00	0.37	
16																	
358		40		6.03	6.03	0.	25.	0.00	0.10		6.09	6.09	0.	62.	0.00	0.26	
11																	
359		40		6.03	6.03	0.	43.	0.00	0.18		6.09	6.09	0.	89.	0.00	0.36	
16																	
360		40		6.03	6.03	0.	37.	0.00	0.15		6.09	6.09	0.	89.	0.00	0.36	
16																	
361		40		6.03	6.03	0.	21.	0.00	0.09		6.09	6.09	0.	63.	0.00	0.26	
11																	
362		40		6.03	6.03	0.	17.	0.00	0.07		6.09	6.09	0.	84.	0.00	0.34	
15																	
363		40		6.03	6.03	0.	17.	0.00	0.07		6.09	6.09	0.	86.	0.00	0.35	
16																	
364		40		6.03	6.03	0.	13.	0.00	0.05		6.09	6.09	0.	64.	0.00	0.26	
12																	
365		40		6.03	6.03	0.	141.	0.00	0.59		22.45	22.45	0.	42.	0.00	0.17	
26																	
366		40		6.03	6.03	0.	156.	0.00	0.65		22.45	22.45	0.	38.	0.00	0.15	
29																	
367		40		6.03	6.03	0.	132.	0.00	0.55		6.09	6.09	0.	61.	0.00	0.25	
24																	
368		40		6.03	6.03	0.	156.	0.00	0.65		6.09	6.09	0.	55.	0.00	0.23	
29																	
369		40		6.03	6.03	0.	106.	0.00	0.44		6.09	6.09	0.	77.	0.00	0.31	
20																	
370		40		6.03	6.03	0.	133.	0.00	0.55		6.09	6.09	0.	72.	0.00	0.30	
24																	
371		40		6.03	6.03	0.	16.	0.00	0.07		6.09	6.09	0.	76.	0.00	0.31	
14																	
372		40		6.03	6.03	0.	45.	0.00	0.19		6.09	6.09	0.	88.	0.00	0.36	
16																	
373		40		6.03	6.03	0.	73.	0.00	0.30		6.09	6.09	0.	89.	0.00	0.36	
16																	
374		40		6.03	6.03	0.	64.	0.00	0.27		6.09	6.09	0.	79.	0.00	0.32	
14																	
375		40		6.03	6.03	0.	79.	0.00	0.33		6.09	6.09	0.	78.	0.00	0.32	
15																	
376		40		6.03	6.03	0.	101.	0.00	0.42		6.09	6.09	0.	82.	0.00	0.34	
19																	
377		40		6.03	6.03	0.	17.	0.00	0.07		6.09	6.09	0.	84.	0.00	0.34	
15																	
378		40		6.03	6.03	0.	17.	0.00	0.07		6.09	6.09	0.	86.	0.00	0.35	
16																	
379		40		6.03	6.03	0.	13.	0.00	0.05		6.09	6.09	0.	64.	0.00	0.26	
12																	
380		40		6.03	6.03	0.	43.	0.00	0.18		6.09	6.09	0.	89.	0.00	0.36	
16																	
381		40		6.03	6.03	0.	37.	0.00	0.15		6.09	6.09	0.	89.	0.00	0.36	
16																	
382		40		6.03	6.03	0.	21.	0.00	0.09		6.09	6.09	0.	63.	0.00	0.26	
11																	
383		40		6.03	6.03	0.	60.	0.00	0.25		6.09	6.09	0.	90.	0.00	0.37	
16																	
384		40		6.03	6.03	0.	43.	0.00	0.18		6.09	6.09	0.	89.	0.00	0.37	
16																	
385		40		6.03	6.03	0.	25.	0.00	0.10		6.09	6.09	0.	62.	0.00	0.26	
11																	
386		40		6.03	6.03	0.	79.	0.00	0.33		6.09	6.09	0.	88.	0.00	0.36	
16																	
387		40		6.03	6.03	0.	51.	0.00	0.21		6.09	6.09	0.	89.	0.00	0.37	
16																	
388		40		6.03	6.03	0.	31.	0.00	0.13		6.09	6.09	0.	60.	0.00	0.25	
11																	
389		40		6.03	12.49	0.	89.	0.00	0.37		6.09	6.09	0.	70.	0.00	0.29	
16																	
390		40		6.03	12.49	0.	63.	0.00	0.26		6.09	13.63	0.	76.	0.00	0.31	
14																	
391		40		6.03	12.49	0.	41.	0.00	0.17		6.09	13.63	0.	45.	0.00	0.19	
8																	
392		40		6.03	12.49	0.	106.	0.00	0.44		22.45	22.45	0.	50.	0.00	0.20	
13																	
393		40		6.03	12.49	0.	81.	0.00	0.33		22.45	29.99	0.	57.	0.00	0.23	
10																	
394		40		6.03	12.49	0.	60.	0.00	0.25		22.45	29.99	0.	34.	0.00	0.14	
7																	

COEF. GUSCI MAX %	SUPERIORE ORIZZONTALE								SUPERIORE VERTICALE					
	spess	Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF	
205	140	16.76	16.76	7782.	120.	0.00	0.36	16.36	16.36	3352.	100.	0.00	0.23	
16														
206	140	16.76	16.76	11035.	238.	0.00	0.60	16.36	16.36	3569.	94.	0.00	0.23	
28														
207	140	16.76	16.76	9423.	249.	0.00	0.59	16.36	16.36	2158.	74.	0.00	0.16	
27														
208	140	16.76	16.76	9423.	249.	0.00	0.59	16.36	16.36	3352.	87.	0.00	0.21	
27														
209	140	16.76	16.76	9439.	258.	0.00	0.60	16.36	16.36	2031.	56.	0.00	0.13	
28														
210	140	16.76	16.76	9439.	258.	0.00	0.60	16.36	16.36	3336.	56.	0.00	0.16	
28														
211	140	16.76	16.76	11989.	270.	0.00	0.68	16.36	16.36	2175.	24.	0.00	0.09	
31														
212	140	16.76	16.76	11989.	270.	0.00	0.68	16.36	16.36	3189.	22.	0.01	0.11	
31														
213	140	16.76	16.76	14884.	224.	0.00	0.67	16.36	16.36	2082.	-5.	0.01	0.06	
31														
214	140	16.76	16.76	14884.	224.	0.00	0.67	16.36	16.36	3134.	-12.	0.01	0.07	
31														
215	140	16.76	16.76	11256.	244.	0.00	0.62	16.36	16.36	1738.	41.	0.00	0.10	
29														
216	140	16.76	16.76	11256.	244.	0.00	0.62	16.36	16.36	2889.	34.	0.00	0.12	
29														
217	140	16.76	16.76	10931.	246.	0.00	0.61	16.36	16.36	1785.	58.	0.00	0.13	
28														
218	140	16.76	16.76	10931.	246.	0.00	0.61	16.36	16.36	2919.	63.	0.00	0.16	
28														
219	140	16.76	16.76	13086.	278.	0.00	0.71	16.36	16.36	3149.	66.	0.00	0.18	
33														
220	140	16.76	16.76	8567.	157.	0.00	0.43	16.36	16.36	3080.	79.	0.00	0.19	
20														
221	140	16.76	16.76	7782.	120.	0.00	0.36	16.36	16.36	5131.	126.	0.00	0.31	
16														
222	140	16.76	16.76	7782.	120.	0.00	0.36	16.36	16.36	7956.	141.	0.00	0.40	
18														
223	140	16.76	16.76	7782.	120.	0.00	0.36	16.36	16.36	11254.	90.	0.00	0.40	
19														
224	140	16.76	16.76	11035.	238.	0.00	0.60	16.36	16.36	5457.	117.	0.00	0.31	
28														
225	140	16.76	16.76	11035.	238.	0.00	0.60	16.36	16.36	8327.	131.	0.00	0.39	
28														
226	140	16.76	16.76	11035.	238.	0.00	0.60	16.36	16.36	11713.	84.	0.00	0.40	
28														
227	140	16.76	16.76	9423.	249.	0.00	0.59	16.36	16.36	5733.	107.	0.00	0.30	
27														
228	140	16.76	16.76	9423.	249.	0.00	0.59	16.36	16.36	8798.	119.	0.00	0.39	
27														
229	140	16.76	16.76	9423.	249.	0.00	0.59	16.36	16.36	12181.	80.	0.00	0.41	
27														
230	140	16.76	16.76	9439.	258.	0.00	0.60	16.36	16.36	5854.	66.	0.00	0.24	
28														
231	140	16.76	16.76	9439.	258.	0.00	0.60	16.36	16.36	8622.	73.	0.00	0.31	
28														
232	140	16.76	16.76	9439.	258.	0.00	0.60	16.36	16.36	12357.	29.	0.03	0.33	
28														
233	140	16.76	16.76	11989.	270.	0.00	0.68	16.36	16.36	5792.	20.	0.02	0.17	
31														
234	140	16.76	16.76	11989.	270.	0.00	0.68	16.36	16.36	8698.	5.	0.04	0.21	
31														
235	140	16.76	16.76	11989.	270.	0.00	0.68	16.36	16.36	12002.	25.	0.04	0.32	
31														
236	140	16.76	16.76	14884.	224.	0.00	0.67	16.36	16.36	5693.	-17.	0.03	0.13	
31														
237	140	16.76	16.76	14884.	224.	0.00	0.67	16.36	16.36	8613.	0.	0.04	0.20	
31														
238	140	16.76	16.76	14884.	224.	0.00	0.67	16.36	16.36	11943.	24.	0.04	0.32	
31														
239	140	16.76	16.76	11256.	244.	0.00	0.62	16.36	16.36	5463.	42.	0.01	0.19	
29														
240	140	16.76	16.76	11256.	244.	0.00	0.62	16.36	16.36	8202.	39.	0.03	0.25	

29														
241	140	16.76	16.76	11256.	244.	0.00	0.62	16.36	16.36	11838.	29.	0.04	0.32	
29														
242	140	16.76	16.76	10931.	246.	0.00	0.61	16.36	16.36	5406.	77.	0.00	0.25	
28														
243	140	16.76	16.76	10931.	246.	0.00	0.61	16.36	16.36	8169.	95.	0.00	0.34	
28														
244	140	16.76	16.76	10931.	246.	0.00	0.61	16.36	16.36	11548.	64.	0.00	0.37	
28														
245	140	16.76	16.76	13086.	278.	0.00	0.71	16.36	16.36	5321.	90.	0.00	0.26	
33														
246	140	16.76	16.76	13086.	278.	0.00	0.71	16.36	16.36	8101.	99.	0.00	0.34	
33														
247	140	16.76	16.76	13086.	278.	0.00	0.71	16.36	16.36	11414.	66.	0.00	0.37	
33														
248	140	16.76	16.76	8567.	157.	0.00	0.43	16.36	16.36	5216.	96.	0.00	0.27	
20														
249	140	16.76	16.76	8567.	157.	0.00	0.43	23.90	16.36	7925.	105.	0.00	0.35	
20														
250	140	16.76	16.76	8567.	157.	0.00	0.43	23.90	16.36	11252.	70.	0.00	0.37	
20														
251	140	16.76	16.76	7782.	120.	0.00	0.36	16.36	16.36	24618.	29.	0.07	0.62	
30														
252	140	16.76	16.76	8015.	113.	0.00	0.35	16.36	16.36	34550.	9.	0.14	0.82	
40														
253	140	16.76	16.76	11035.	238.	0.00	0.60	16.36	16.36	24382.	26.	0.08	0.61	
29														
254	140	16.76	16.76	9423.	249.	0.00	0.59	16.36	16.36	24661.	23.	0.08	0.61	
30														
255	140	16.76	16.76	9423.	249.	0.00	0.58	16.36	16.36	35867.	-2.	0.15	0.84	
41														
256	140	16.76	16.76	9439.	258.	0.00	0.60	16.36	16.36	24696.	23.	0.08	0.61	
30														
257	140	16.76	16.76	9439.	258.	0.00	0.60	16.36	16.36	35805.	-2.	0.15	0.84	
41														
258	140	16.76	16.76	11989.	270.	0.00	0.68	16.36	16.36	24696.	23.	0.08	0.61	
31														
259	140	16.76	16.76	11989.	270.	0.00	0.67	16.36	16.36	35805.	-2.	0.15	0.84	
41														
260	140	16.76	16.76	14884.	224.	0.00	0.67	16.36	16.36	24696.	23.	0.08	0.61	
31														
261	140	16.76	16.76	16008.	176.	0.00	0.67	16.36	16.36	35805.	-2.	0.15	0.84	
41														
262	140	16.76	16.76	11256.	244.	0.00	0.62	16.36	16.36	24696.	23.	0.08	0.61	
30														
263	140	16.76	16.76	11256.	244.	0.00	0.62	16.36	16.36	35805.	-2.	0.15	0.84	
41														
264	140	16.76	16.76	10931.	246.	0.00	0.61	16.36	16.36	24729.	23.	0.08	0.61	
30														
265	140	16.76	16.76	10931.	246.	0.00	0.61	16.36	16.36	35921.	-2.	0.15	0.84	
41														
266	140	16.76	16.76	13086.	278.	0.00	0.71	16.36	16.36	25016.	24.	0.08	0.62	
33														
267	140	16.76	16.76	8567.	157.	0.00	0.43	16.36	16.36	25540.	20.	0.09	0.63	
30														
268	140	16.76	16.76	8824.	146.	0.00	0.42	16.36	16.36	34439.	-41.	0.15	0.81	
39														
293	140	16.76	16.76	11678.	255.	0.00	0.64	16.36	16.36	33244.	-59.	0.15	0.74	
36														
294	140	16.76	16.76	13317.	274.	0.00	0.71	16.36	16.36	35767.	-18.	0.15	0.83	
40														
295	140	16.76	16.76	8981.	196.	0.00	0.50	16.36	16.36	31832.	-71.	0.14	0.71	
35														
296	140	16.76	16.76	9333.	136.	0.00	0.41	16.36	16.36	30685.	-65.	0.14	0.68	
33														
297	140	16.76	16.76	11225.	235.	0.00	0.60	16.36	16.36	34430.	-8.	0.15	0.80	
39														
298	140	16.76	16.76	10063.	218.	0.00	0.55	16.36	16.36	29159.	-25.	0.13	0.67	
33														
299	140	16.76	16.76	7735.	119.	0.00	0.35	16.36	16.36	2485.	84.	0.00	0.19	
16														
300	140	16.76	16.76	10980.	238.	0.00	0.60	16.36	16.36	2334.	78.	0.00	0.17	
28														
301	140	16.76	16.76	13008.	277.	0.00	0.71	16.36	16.36	1918.	62.	0.00	0.14	
33														
302	140	16.76	16.76	8505.	157.	0.00	0.43	16.36	16.36	2049.	71.	0.00	0.16	

20													
303	20	14.33	6.79	105.	60.	0.00	0.27	5.89	5.89	40.	14.	0.00	0.08
12													
304	20	14.33	6.79	83.	82.	0.00	0.34	5.89	5.89	34.	11.	0.00	0.07
15													
305	20	14.33	6.79	98.	89.	0.00	0.36	5.89	5.89	32.	9.	0.00	0.05
16													
306	20	14.33	6.79	4916.	70.	0.54	1.28	5.89	5.89	289.	16.	0.01	0.23
62													
307	20	14.33	6.79	107.	93.	0.00	0.39	5.89	5.89	15.	5.	0.00	0.03
17													
308	20	14.33	6.79	5293.	74.	0.60	1.37	5.89	5.89	362.	7.	0.04	0.23
67													
309	20	14.33	6.79	111.	99.	0.00	0.41	5.89	5.89	5.	4.	0.00	0.02
18													
310	20	14.33	6.79	5500.	79.	0.63	1.43	5.89	5.89	366.	2.	0.06	0.21
70													
311	20	14.33	6.79	113.	104.	0.00	0.43	5.89	5.89	17.	-2.	0.00	0.01
19													
312	20	14.33	6.79	5484.	83.	0.62	1.43	5.89	5.89	365.	1.	0.07	0.21
70													
313	20	14.33	6.79	109.	103.	0.00	0.43	5.89	5.89	20.	2.	0.00	0.02
19													
314	20	14.33	6.79	5237.	82.	0.58	1.37	5.89	5.89	360.	8.	0.04	0.23
67													
315	20	14.33	6.79	100.	107.	0.00	0.44	5.89	5.89	34.	8.	0.00	0.05
20													
316	20	14.33	6.79	4761.	86.	0.49	1.27	5.89	5.89	311.	17.	0.02	0.25
62													
317	20	14.33	6.79	86.	119.	0.00	0.45	5.89	5.89	52.	13.	0.00	0.08
20													
318	20	14.33	6.79	106.	81.	0.00	0.35	5.89	5.89	76.	18.	0.00	0.12
16													
319	20	6.03	6.03	2118.	85.	0.29	1.50	6.09	6.09	183.	72.	0.00	0.39
73													
320	20	6.03	6.03	2397.	94.	0.37	1.69	6.09	6.09	317.	51.	0.00	0.39
82													
321	20	6.03	6.03	1755.	95.	0.16	1.35	6.09	6.09	315.	42.	0.00	0.34
65													
322	20	6.03	6.03	2311.	94.	0.34	1.65	6.09	6.09	256.	21.	0.00	0.23
80													
323	20	6.03	6.03	1497.	90.	0.09	1.19	6.09	6.09	238.	21.	0.00	0.21
57													
324	20	6.03	6.03	697.	89.	0.00	0.75	6.09	6.09	121.	30.	0.00	0.19
34													
325	20	6.03	6.03	2115.	85.	0.28	1.50	6.09	6.09	182.	70.	0.00	0.39
73													
326	20	6.03	6.03	2395.	93.	0.37	1.68	6.09	6.09	316.	47.	0.00	0.37
82													
327	20	6.03	6.03	1753.	90.	0.17	1.32	6.09	6.09	279.	35.	0.00	0.29
64													
328	20	6.03	6.03	2310.	87.	0.34	1.61	6.09	6.09	242.	18.	0.00	0.20
78													
329	20	6.03	6.03	1496.	83.	0.10	1.15	11.98	11.98	183.	19.	0.00	0.09
55													
330	20	6.03	6.03	694.	81.	0.00	0.71	11.98	11.98	89.	24.	0.00	0.14
33													
331	20	14.33	6.79	3361.	38.	0.36	0.86	5.89	5.89	174.	25.	0.00	0.20
42													
332	20	14.33	6.79	4260.	72.	0.43	1.13	5.89	5.89	177.	29.	0.00	0.22
55													
333	20	14.33	6.79	3889.	103.	0.30	1.09	5.89	5.89	249.	27.	0.00	0.25
54													
334	20	14.33	6.79	3625.	52.	0.36	0.94	5.89	5.89	230.	28.	0.00	0.25
46													
335	40	6.03	6.03	6650.	130.	1.24	16.96	6.09	6.09	1431.	45.	0.00	0.52
93													
336	40	6.03	6.03	4456.	157.	0.08	1.71	6.09	6.09	1005.	31.	0.00	0.36
84													
337	40	6.03	6.03	4089.	126.	0.05	1.50	6.09	6.09	1506.	52.	0.00	0.58
73													
338	40	6.03	6.03	3608.	142.	0.00	1.46	6.09	6.09	1017.	56.	0.00	0.47
71													
339	40	6.03	6.03	2563.	107.	0.00	1.05	6.09	6.09	1390.	78.	0.00	0.65
50													
340	40	6.03	6.03	2573.	133.	0.00	1.16	6.09	6.09	1169.	75.	0.00	0.58

55													
341	40	6.03	6.03	240.	16.	0.00	0.12	6.09	6.09	829.	76.	0.00	0.51
23													
342	40	6.03	6.03	764.	45.	0.00	0.37	6.09	6.09	1195.	86.	0.00	0.64
30													
343	40	6.03	6.03	1411.	72.	0.00	0.64	6.09	6.09	1320.	84.	0.00	0.66
31													
344	40	6.03	6.03	1384.	64.	0.00	0.60	6.09	6.09	1202.	79.	0.00	0.61
28													
345	40	6.03	6.03	1666.	79.	0.00	0.72	6.09	6.09	1365.	79.	0.00	0.65
34													
346	40	6.03	6.03	1811.	101.	0.00	0.85	6.09	6.09	1218.	82.	0.00	0.62
40													
347	40	12.63	6.03	8830.	92.	0.17	1.22	6.09	6.09	3435.	34.	0.10	0.95
60													
348	40	12.63	6.03	9742.	73.	0.26	1.28	13.63	6.09	6204.	40.	0.13	0.74
63													
349	40	12.63	6.03	10976.	51.	0.36	1.38	13.63	6.09	9086.	23.	0.30	1.03
68													
350	40	12.63	6.03	4784.	85.	0.10	1.41	6.09	6.09	2298.	69.	0.00	0.82
68													
351	40	12.63	6.03	4905.	66.	0.13	1.27	6.09	6.09	4029.	61.	0.10	1.20
62													
352	40	12.63	6.03	4987.	44.	0.15	1.17	6.09	6.09	5605.	35.	0.25	1.47
71													
353	40	6.03	6.03	2333.	79.	0.00	0.88	6.09	6.09	1859.	88.	0.00	0.80
42													
354	40	6.03	6.03	2202.	49.	0.00	0.73	6.09	6.09	2728.	81.	0.00	0.98
47													
355	40	6.03	6.03	1971.	31.	0.04	0.60	6.09	6.09	3570.	59.	0.08	1.08
52													
356	40	6.03	6.03	1309.	60.	0.00	0.56	6.09	6.09	1680.	86.	0.00	0.75
35													
357	40	6.03	6.03	1133.	40.	0.00	0.44	6.09	6.09	2264.	89.	0.00	0.90
43													
358	40	6.03	6.03	881.	25.	0.00	0.31	6.09	6.09	2939.	60.	0.00	0.94
45													
359	40	6.03	6.03	686.	43.	0.00	0.34	6.09	6.09	1382.	85.	0.00	0.68
31													
360	40	6.03	6.03	623.	37.	0.00	0.30	6.09	6.09	1802.	89.	0.00	0.79
37													
361	40	6.03	6.03	520.	21.	0.00	0.21	6.09	6.09	2359.	62.	0.00	0.81
38													
362	40	6.03	6.03	229.	17.	0.00	0.12	6.09	6.09	1118.	83.	0.00	0.60
28													
363	40	6.03	6.03	228.	17.	0.00	0.12	6.09	6.09	1485.	86.	0.00	0.70
33													
364	40	6.03	6.03	183.	13.	0.00	0.10	6.09	6.09	2307.	63.	0.00	0.80
38													
365	40	12.49	6.03	6644.	120.	0.26	1.94	22.45	22.45	1482.	40.	0.01	0.51
96													
366	40	6.03	6.03	4449.	146.	0.07	1.67	22.45	22.45	1026.	38.	0.00	0.40
81													
367	40	6.03	6.03	4085.	122.	0.06	1.48	6.09	6.09	1338.	61.	0.00	0.57
72													
368	40	6.03	6.03	3604.	139.	0.00	1.44	6.09	6.09	1024.	54.	0.00	0.46
69													
369	40	6.03	6.03	2559.	106.	0.00	1.05	6.09	6.09	1387.	77.	0.00	0.64
50													
370	40	6.03	6.03	2569.	133.	0.00	1.16	6.09	6.09	1200.	72.	0.00	0.58
55													
371	40	6.03	6.03	239.	16.	0.00	0.12	6.09	6.09	828.	76.	0.00	0.51
23													
372	40	6.03	6.03	762.	45.	0.00	0.37	6.09	6.09	1193.	86.	0.00	0.64
29													
373	40	6.03	6.03	1408.	73.	0.00	0.64	6.09	6.09	1317.	84.	0.00	0.66
30													
374	40	6.03	6.03	1381.	64.	0.00	0.60	6.09	6.09	1199.	79.	0.00	0.61
28													
375	40	6.03	6.03	1663.	79.	0.00	0.72	6.09	6.09	1361.	78.	0.00	0.64
34													
376	40	6.03	6.03	1808.	101.	0.00	0.85	6.09	6.09	1222.	82.	0.00	0.62
40													
377	40	6.03	6.03	227.	17.	0.00	0.12	6.09	6.09	1117.	83.	0.00	0.60
28													
378	40	6.03	6.03	226.	17.	0.00	0.12	6.09	6.09	1485.	86.	0.00	0.70

211		16.76	16.76	0.	85	0.00	254.		0.	0.	0.000	0.	0.	0.00	0.000
212		16.76	16.76	0.	85	0.00	254.		0.	0.	0.000	0.	0.	0.00	0.000
213		16.76	16.76	0.	112	0.00	334.		0.	0.	0.000	0.	0.	0.00	0.000
214		16.76	16.76	0.	112	0.00	334.		0.	0.	0.000	0.	0.	0.00	0.000
215		16.76	16.76	0.	113	0.00	339.		0.	0.	0.000	0.	0.	0.00	0.000
216		16.76	16.76	0.	113	0.00	339.		0.	0.	0.000	0.	0.	0.00	0.000
217		16.76	16.76	0.	85	0.00	254.		0.	0.	0.000	0.	0.	0.00	0.000
218		16.76	16.76	0.	85	0.00	254.		0.	0.	0.000	0.	0.	0.00	0.000
219		16.76	16.76	0.	104	0.00	311.		0.	0.	0.000	0.	0.	0.00	0.000
220		16.76	16.76	0.	64	0.00	192.		0.	0.	0.000	0.	0.	0.00	0.000
221		16.76	16.76	0.	61	0.00	183.		0.	0.	0.000	0.	0.	0.00	0.000
222		16.76	16.76	0.	61	0.00	183.		0.	0.	0.000	0.	0.	0.00	0.000
223		16.76	16.76	0.	61	0.00	183.		0.	0.	0.000	0.	0.	0.00	0.000
224		16.76	16.76	0.	100	0.00	297.		0.	0.	0.000	0.	0.	0.00	0.000
225		16.76	16.76	0.	100	0.00	297.		0.	0.	0.000	0.	0.	0.00	0.000
226		16.76	16.76	0.	100	0.00	297.		0.	0.	0.000	0.	0.	0.00	0.000
227		16.76	16.76	0.	70	0.00	208.		0.	0.	0.000	0.	0.	0.00	0.000
228		16.76	16.76	0.	70	0.00	208.		0.	0.	0.000	0.	0.	0.00	0.000
229		16.76	16.76	0.	70	0.00	208.		0.	0.	0.000	0.	0.	0.00	0.000
230		16.76	16.76	0.	82	0.00	245.		0.	0.	0.000	0.	0.	0.00	0.000
231		16.76	16.76	0.	82	0.00	245.		0.	0.	0.000	0.	0.	0.00	0.000
232		16.76	16.76	0.	82	0.00	245.		0.	0.	0.000	0.	0.	0.00	0.000
233		16.76	16.76	0.	85	0.00	254.		0.	0.	0.000	0.	0.	0.00	0.000
234		16.76	16.76	0.	85	0.00	254.		0.	0.	0.000	0.	0.	0.00	0.000
235		16.76	16.76	0.	85	0.00	254.		0.	0.	0.000	0.	0.	0.00	0.000
236		16.76	16.76	0.	112	0.00	334.		0.	0.	0.000	0.	0.	0.00	0.000
237		16.76	16.76	0.	112	0.00	334.		0.	0.	0.000	0.	0.	0.00	0.000
238		16.76	16.76	0.	112	0.00	334.		0.	0.	0.000	0.	0.	0.00	0.000
239		16.76	16.76	0.	113	0.00	339.		0.	0.	0.000	0.	0.	0.00	0.000
240		16.76	16.76	0.	113	0.00	339.		0.	0.	0.000	0.	0.	0.00	0.000
241		16.76	16.76	0.	113	0.00	339.		0.	0.	0.000	0.	0.	0.00	0.000
242		16.76	16.76	0.	85	0.00	254.		0.	0.	0.000	0.	0.	0.00	0.000
243		16.76	16.76	0.	85	0.00	254.		0.	0.	0.000	0.	0.	0.00	0.000
244		16.76	16.76	0.	85	0.00	254.		0.	0.	0.000	0.	0.	0.00	0.000
245		16.76	16.76	0.	104	0.00	311.		0.	0.	0.000	0.	0.	0.00	0.000
246		16.76	16.76	0.	104	0.00	311.		0.	0.	0.000	0.	0.	0.00	0.000
247		16.76	16.76	0.	104	0.00	311.		0.	0.	0.000	0.	0.	0.00	0.000
248		16.76	16.76	0.	64	0.00	192.		0.	0.	0.000	0.	0.	0.00	0.000
249		16.76	16.76	0.	64	0.00	192.		0.	0.	0.000	0.	0.	0.00	0.000
250		16.76	16.76	0.	64	0.00	192.		0.	0.	0.000	0.	0.	0.00	0.000
251		16.76	16.76	0.	61	0.00	183.		0.	0.	0.000	0.	0.	0.00	0.000
252		16.76	16.76	0.	55	0.00	165.		0.	0.	0.000	0.	0.	0.00	0.000
253		16.76	16.76	0.	100	0.00	297.		0.	0.	0.000	0.	0.	0.00	0.000
254		16.76	16.76	0.	70	0.00	208.		0.	0.	0.000	0.	0.	0.00	0.000
255		16.76	16.76	0.	58	0.00	173.		0.	0.	0.000	0.	0.	0.00	0.000
256		16.76	16.76	0.	82	0.00	245.		0.	0.	0.000	0.	0.	0.00	0.000
257		16.76	16.76	0.	69	0.00	207.		0.	0.	0.000	0.	0.	0.00	0.000
258		16.76	16.76	0.	85	0.00	254.		0.	0.	0.000	0.	0.	0.00	0.000
259		16.76	16.76	0.	73	0.00	217.		0.	0.	0.000	0.	0.	0.00	0.000
260		16.76	16.76	0.	112	0.00	334.		0.	0.	0.000	0.	0.	0.00	0.000
261		16.76	16.76	0.	98	0.00	291.		0.	0.	0.000	0.	0.	0.00	0.000
262		16.76	16.76	0.	113	0.00	339.		0.	0.	0.000	0.	0.	0.00	0.000
263		16.76	16.76	0.	100	0.00	297.		0.	0.	0.000	0.	0.	0.00	0.000
264		16.76	16.76	0.	85	0.00	254.		0.	0.	0.000	0.	0.	0.00	0.000
265		16.76	16.76	0.	73	0.00	217.		0.	0.	0.000	0.	0.	0.00	0.000
266		16.76	16.76	0.	104	0.00	311.		0.	0.	0.000	0.	0.	0.00	0.000
267		16.76	16.76	0.	64	0.00	192.		0.	0.	0.000	0.	0.	0.00	0.000
268		16.76	16.76	0.	58	0.00	174.		0.	0.	0.000	0.	0.	0.00	0.000
293		16.76	16.76	0.	99	0.00	295.		0.	0.	0.000	0.	0.	0.00	0.000
294		16.76	16.76	0.	102	0.00	304.		0.	0.	0.000	0.	0.	0.00	0.000
295		16.76	16.76	0.	52	0.00	154.		0.	0.	0.000	0.	0.	0.00	0.000
296		16.76	16.76	0.	27	0.00	82.		0.	0.	0.000	0.	0.	0.00	0.000
297		16.76	16.76	0.	97	0.00	290.		0.	0.	0.000	0.	0.	0.00	0.000
298		16.76	16.76	0.	93	0.00	276.		0.	0.	0.000	0.	0.	0.00	0.000
299		16.76	16.76	0.	60	0.00	180.		0.	0.	0.000	0.	0.	0.00	0.000
300		16.76	16.76	0.	100	0.00	297.		0.	0.	0.000	0.	0.	0.00	0.000
301		16.76	16.76	0.	104	0.00	311.		0.	0.	0.000	0.	0.	0.00	0.000
302		16.76	16.76	0.	63	0.00	189.		0.	0.	0.000	0.	0.	0.00	0.000
303		6.79	8.67	0.	40	0.00	297.		0.	0.	0.000	0.	0.	0.00	0.000
304		6.79	8.67	0.	56	0.00	416.		0.	0.	0.000	0.	0.	0.00	0.000
305		6.79	8.67	0.	60	0.00	442.		0.	0.	0.000	0.	0.	0.00	0.000
306		6.79	14.33	0.	53	0.00	388.		0.	0.	0.000	0.	0.	0.00	0.000
307		6.79	8.67	0.	59	0.00	432.		0.	0.	0.000	0.	0.	0.00	0.000
308		6.79	14.33	0.	51	0.00	376.		0.	0.	0.000	0.	0.	0.00	0.000
309		6.79	8.67	0.	58	0.00	431.		0.	0.	0.000	0.	0.	0.00	0.000
310		6.79	14.33	0.	51	0.00	373.		0.	0.	0.000	0.	0.	0.00	0.000

311		6.79	8.67	0.	68	0.00	502.		0.	0.	0.000	0.	0.	0.00	0.000
312		6.79	14.33	0.	55	0.00	406.		0.	0.	0.000	0.	0.	0.00	0.000
313		6.79	8.67	0.	67	0.00	494.		0.	0.	0.000	0.	0.	0.00	0.000
314		6.79	14.33	0.	53	0.00	392.		0.	0.	0.000	0.	0.	0.00	0.000
315		6.79	8.67	0.	62	0.00	456.		0.	0.	0.000	0.	0.	0.00	0.000
316		6.79	14.33	0.	50	0.00	371.		0.	0.	0.000	0.	0.	0.00	0.000
317		6.79	8.67	0.	56	0.00	412.		0.	0.	0.000	0.	0.	0.00	0.000
318		6.79	8.67	0.	41	0.00	305.		0.	0.	0.000	0.	0.	0.00	0.000
319		6.03	6.03	0.	64	0.00	528.		0.	0.	0.000	0.	0.	0.00	0.000
320		6.03	6.03	0.	72	0.00	594.		0.	0.	0.000	0.	0.	0.00	0.000
321		6.03	6.03	0.	68	0.00	565.		0.	0.	0.000	0.	0.	0.00	0.000
322		6.03	6.03	0.	66	0.00	545.		0.	0.	0.000	0.	0.	0.00	0.000
323		6.03	6.03	0.	62	0.00	512.		0.	0.	0.000	0.	0.	0.00	0.000
324		6.03	6.03	0.	60	0.00	494.		0.	0.	0.000	0.	0.	0.00	0.000
325		6.03	6.03	0.	64	0.00	527.		0.	0.	0.000	0.	0.	0.00	0.000
326		6.03	6.03	0.	72	0.00	597.		0.	0.	0.000	0.	0.	0.00	0.000
327		6.03	6.03	0.	68	0.00	567.		0.	0.	0.000	0.	0.	0.00	0.000
328		6.03	6.03	0.	66	0.00	544.		0.	0.	0.000	0.	0.	0.00	0.000
329		6.03	6.03	0.	61	0.00	508.		0.	0.	0.000	0.	0.	0.00	0.000
330		6.03	6.03	0.	59	0.00	492.		0.	0.	0.000	0.	0.	0.00	0.000
331		6.79	14.33	0.	29	0.00	217.		0.	0.	0.000	0.	0.	0.00	0.000
332		6.79	14.33	0.	51	0.00	377.		0.	0.	0.000	0.	0.	0.00	0.000
333		6.79	14.33	0.	46	0.00	338.		0.	0.	0.000	0.	0.	0.00	0.000
334		6.79	14.33	0.	30	0.00	218.		0.	0.	0.000	0.	0.	0.00	0.000
335		6.03	6.03	0.	97	0.00	808.		0.	0.	0.000	0.	0.	0.00	0.000
336		6.03	6.03	0.	112	0.00	932.		0.	0.	0.000	0.	0.	0.00	0.000
337		6.03	6.03	0.	89	0.00	735.		0.	0.	0.000	0.	0.	0.00	0.000
338		6.03	6.03	0.	111	0.00	920.		0.	0.	0.000	0.	0.	0.00	0.000
339		6.03	6.03	0.	70	0.00	583.		0.	0.	0.000	0.	0.	0.00	0.000
340		6.03	6.03	0.	91	0.00	751.		0.	0.	0.000	0.	0.	0.00	0.000
341		6.03	6.03	0.	12	0.00	97.		0.	0.	0.000	0.	0.	0.00	0.000
342		6.03	6.03	0.	29	0.00	242.		0.	0.	0.000	0.	0.	0.00	0.000
343		6.03	6.03	0.	49	0.00	407.		0.	0.	0.000	0.	0.	0.00	0.000
344		6.03	6.03	0.	46	0.00	384.		0.	0.	0.000	0.	0.	0.00	0.000
345		6.03	6.03	0.	60	0.00	496.		0.	0.	0.000	0.	0.	0.00	0.000
346		6.03	6.03	0.	67	0.00	554.		0.	0.	0.000	0.	0.	0.00	0.000
347		6.03	12.63	0.	57	0.00	470.		0.	0.	0.000	0.	0.	0.00	0.000
348		6.03	12.63	0.	38	0.00	318.		0.	0.	0.000	0.	0.	0.00	0.000
349		6.03	12.63	0.	17	0.00	145.		0.	0.	0.000	0.	0.	0.00	0.000
350		6.03	7.68	0.	40	0.00	331.		0.	0.	0.000	0.	0.	0.00	0.000
351		6.03	7.68	0.	21	0.00	172.		0.	0.	0.000	0.	0.	0.00	0.000
352		6.03	7.68	0.	-3	0.07	-1.		0.	0.	0.000	0.	0.	0.00	0.000
353		6.03	6.03	0.	37	0.00	307.		0.	0.	0.000	0.	0.	0.00	0.000
354		6.03	6.03	0.	19	0.00	155.		0.	0.	0.000	0.	0.	0.00	0.000
355		6.03	6.03	0.	-2	0.04	-1.		0.	0.	0.000	0.	0.	0.00	0.000
356		6.03	6.03	0.	34	0.00	278.		0.	0.	0.000	0.	0.	0.00	0.000
357		6.03	6.03	0.	20	0.00	162.		0.	0.	0.000	0.	0.	0.00	0.000
358		6.03	6.03	0.	5	0.00	38.		0.	0.	0.000	0.	0.	0.00	0.000
359		6.03	6.03	0.	21	0.00	174.		0.	0.	0.000	0.	0.	0.00	0.000
360		6.03	6.03	0.	20	0.00	168.		0.	0.	0.000	0.	0.	0.00	0.000
361		6.03	6.03	0.	11	0.00	90.		0.	0.	0.000	0.	0.	0.00	0.000
362		6.03	6.03	0.	9	0.00	78.		0.	0.	0.000	0.	0.	0.00	0.000
363		6.03	6.03	0.	9	0.00	78.		0.	0.	0.000	0.	0.	0.00	0.000
364		6.03	6.03	0.	8	0.00	65.		0.	0.	0.000	0.	0.	0.00	0.000
365		6.03	7.65	0.	98	0.00	816.		0.	0.	0.000	0.	0.	0.00	0.000
366		6.03	6.03	0.	113	0.00	933.		0.	0.	0.000	0.	0.	0.00	0.000
367		6.03	6.03	0.	90	0.00	743.		0.	0.	0.000	0.	0.	0.00	0.000
368		6.03	6.03	0.	112	0.00	926.		0.	0.	0.000	0.	0.	0.00	0.000
369		6.03	6.03	0.	71	0.00	585.		0.	0.	0.000	0.	0.	0.00	0.000
370		6.03	6.03	0.	91	0.00	752.		0.	0.	0.000	0.	0.	0.00	0.000
371		6.03	6.03	0.	12	0.00	96.		0.	0.	0.000	0.	0.	0.00	0.000
372		6.03	6.03	0.	29	0.00	241.		0.	0.	0.000	0.	0.	0.00	0.000
373		6.03	6.03	0.	49	0.00	407.		0.	0.	0.000	0.	0.	0.00	0.000
374		6.03	6.03	0.	46	0.00	384.		0.	0.	0.000	0.	0.	0.00	0.000
375		6.03	6.03	0.	60	0.00	495.		0.	0.	0.000	0.	0.	0.00	0.000
376		6.03	6.03	0.	67	0.00	553.		0.	0.	0.000	0.	0.	0.00	0.000
377		6.03	6.03	0.	9	0.00	78.		0.	0.	0.000	0.	0.	0.00	0.000
378		6.03	6.03	0.	9	0.00	78.		0.	0.	0.000	0.	0.	0.00	0.000
379		6.03	6.03	0.	8	0.00	64.		0.	0.	0.000	0.	0.	0.00	0.000
380		6.03	6.03	0.	21	0.00	174.		0.	0.	0.000	0.	0.	0.00	0.000
381		6.03	6.03	0.	20	0.00	168.		0.	0.	0.000	0.	0.	0.00	0.000
382		6.03	6.03	0.	11	0.00	90.		0.	0.	0.000	0.	0.	0.00	0.000
383		6.03	6.03	0.	34	0.00	278.		0.	0.	0.000	0.	0.	0.00	0.000
384		6.03	6.03	0.	20	0.00	164.		0.	0.	0.000	0.	0.	0.00	0.000
385		6.03	6.03	0.	5	0.00	41.		0.	0.	0.000	0.	0.	0.00	0.000
386		6.03	6.03	0.	37	0.00	309.		0.	0.	0.000	0.	0.	0.00	0.000

387		6.03	6.03	0.	19	0.00	157.	0.	0.	0.000	0.	0.	0.00	0.000
388		6.03	6.03	0.	-1	0.04	-1.	0.	0.	0.000	0.	0.	0.00	0.000
389		6.03	7.65	0.	41	0.00	340.	0.	0.	0.000	0.	0.	0.00	0.000
390		6.03	7.65	0.	22	0.00	182.	0.	0.	0.000	0.	0.	0.00	0.000
391		6.03	7.65	0.	-2	0.04	-1.	0.	0.	0.000	0.	0.	0.00	0.000
392		6.03	12.49	0.	58	0.00	480.	0.	0.	0.000	0.	0.	0.00	0.000
393		6.03	12.49	0.	40	0.00	330.	0.	0.	0.000	0.	0.	0.00	0.000
394		6.03	12.49	0.	19	0.00	161.	0.	0.	0.000	0.	0.	0.00	0.000

ARMATURA INFERIORE VERTICALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE			COMB. QUASI PERMANENTE								
	Af	Afc	Mom	Nor	sigC	sigF	Mom	Nor	WkF	Mom	Nor	sigC	WkP	
205		16.36	16.36	0.	21	0.00	65.	0.	0.	0.000	0.	0.	0.00	0.000
206		16.36	16.36	0.	1	0.00	4.	0.	0.	0.000	0.	0.	0.00	0.000
207		16.36	16.36	0.	-30	0.21	-3.	0.	0.	0.000	0.	0.	0.00	0.000
208		16.36	16.36	0.	-18	0.13	-2.	0.	0.	0.000	0.	0.	0.00	0.000
209		16.36	16.36	0.	-39	0.27	-4.	0.	0.	0.000	0.	0.	0.00	0.000
210		16.36	16.36	0.	-49	0.34	-5.	0.	0.	0.000	0.	0.	0.00	0.000
211		16.36	16.36	0.	-54	0.37	-6.	0.	0.	0.000	0.	0.	0.00	0.000
212		16.36	16.36	0.	-79	0.54	-8.	0.	0.	0.000	0.	0.	0.00	0.000
213		16.36	16.36	0.	-59	0.41	-6.	0.	0.	0.000	0.	0.	0.00	0.000
214		16.36	16.36	0.	-78	0.54	-8.	0.	0.	0.000	0.	0.	0.00	0.000
215		16.36	16.36	0.	-45	0.31	-5.	0.	0.	0.000	0.	0.	0.00	0.000
216		16.36	16.36	0.	-48	0.33	-5.	0.	0.	0.000	0.	0.	0.00	0.000
217		16.36	16.36	0.	-36	0.25	-4.	0.	0.	0.000	0.	0.	0.00	0.000
218		16.36	16.36	0.	-18	0.13	-2.	0.	0.	0.000	0.	0.	0.00	0.000
219		16.36	16.36	0.	-2	0.01	0.	0.	0.	0.000	0.	0.	0.00	0.000
220		16.36	16.36	0.	15	0.00	47.	0.	0.	0.000	0.	0.	0.00	0.000
221		16.36	16.36	0.	9	0.00	28.	0.	0.	0.000	0.	0.	0.00	0.000
222		16.36	16.36	0.	-2	0.01	0.	0.	0.	0.000	0.	0.	0.00	0.000
223		16.36	16.36	0.	-22	0.15	-2.	0.	0.	0.000	0.	0.	0.00	0.000
224		16.36	16.36	0.	-10	0.07	-1.	0.	0.	0.000	0.	0.	0.00	0.000
225		16.36	16.36	0.	-19	0.13	-2.	0.	0.	0.000	0.	0.	0.00	0.000
226		16.36	16.36	0.	-39	0.27	-4.	0.	0.	0.000	0.	0.	0.00	0.000
227		16.36	16.36	0.	-34	0.24	-4.	0.	0.	0.000	0.	0.	0.00	0.000
228		16.36	16.36	0.	-46	0.32	-5.	0.	0.	0.000	0.	0.	0.00	0.000
229		16.36	16.36	0.	-65	0.45	-7.	0.	0.	0.000	0.	0.	0.00	0.000
230		16.36	16.36	0.	-75	0.52	-8.	0.	0.	0.000	0.	0.	0.00	0.000
231		16.36	16.36	0.	-88	0.61	-9.	0.	0.	0.000	0.	0.	0.00	0.000
232		16.36	16.36	0.	-109	0.75	-11.	0.	0.	0.000	0.	0.	0.00	0.000
233		16.36	16.36	0.	-109	0.75	-11.	0.	0.	0.000	0.	0.	0.00	0.000
234		16.36	16.36	0.	-120	0.83	-12.	0.	0.	0.000	0.	0.	0.00	0.000
235		16.36	16.36	0.	-114	0.79	-12.	0.	0.	0.000	0.	0.	0.00	0.000
236		16.36	16.36	0.	-91	0.63	-9.	0.	0.	0.000	0.	0.	0.00	0.000
237		16.36	16.36	0.	-100	0.69	-10.	0.	0.	0.000	0.	0.	0.00	0.000
238		16.36	16.36	0.	-105	0.72	-11.	0.	0.	0.000	0.	0.	0.00	0.000
239		16.36	16.36	0.	-57	0.39	-6.	0.	0.	0.000	0.	0.	0.00	0.000
240		16.36	16.36	0.	-68	0.47	-7.	0.	0.	0.000	0.	0.	0.00	0.000
241		16.36	16.36	0.	-88	0.61	-9.	0.	0.	0.000	0.	0.	0.00	0.000
242		16.36	16.36	0.	-18	0.13	-2.	0.	0.	0.000	0.	0.	0.00	0.000
243		16.36	16.36	0.	-23	0.16	-2.	0.	0.	0.000	0.	0.	0.00	0.000
244		16.36	16.36	0.	-43	0.30	-4.	0.	0.	0.000	0.	0.	0.00	0.000
245		16.36	16.36	0.	4	0.00	11.	0.	0.	0.000	0.	0.	0.00	0.000
246		16.36	16.36	0.	3	0.00	9.	0.	0.	0.000	0.	0.	0.00	0.000
247		16.36	16.36	0.	-15	0.11	-2.	0.	0.	0.000	0.	0.	0.00	0.000
248		16.36	16.36	0.	21	0.00	64.	0.	0.	0.000	0.	0.	0.00	0.000
249		16.36	18.25	0.	22	0.00	67.	0.	0.	0.000	0.	0.	0.00	0.000
250		16.36	18.25	0.	-32	0.22	-3.	0.	0.	0.000	0.	0.	0.00	0.000
251		16.36	16.36	0.	-204	1.41	-21.	0.	0.	0.000	0.	0.	0.00	0.000
252		16.36	16.36	0.	-226	1.56	-23.	0.	0.	0.000	0.	0.	0.00	0.000
253		16.36	16.36	0.	-220	1.51	-23.	0.	0.	0.000	0.	0.	0.00	0.000
254		16.36	16.36	0.	-210	1.45	-22.	0.	0.	0.000	0.	0.	0.00	0.000
255		16.36	16.36	0.	-227	1.57	-24.	0.	0.	0.000	0.	0.	0.00	0.000
256		16.36	16.36	0.	-209	1.44	-22.	0.	0.	0.000	0.	0.	0.00	0.000
257		16.36	16.36	0.	-226	1.56	-23.	0.	0.	0.000	0.	0.	0.00	0.000
258		16.36	16.36	0.	-209	1.44	-22.	0.	0.	0.000	0.	0.	0.00	0.000
259		16.36	16.36	0.	-226	1.56	-23.	0.	0.	0.000	0.	0.	0.00	0.000
260		16.36	16.36	0.	-209	1.44	-22.	0.	0.	0.000	0.	0.	0.00	0.000
261		16.36	16.36	0.	-226	1.56	-23.	0.	0.	0.000	0.	0.	0.00	0.000
262		16.36	16.36	0.	-209	1.44	-22.	0.	0.	0.000	0.	0.	0.00	0.000
263		16.36	16.36	0.	-226	1.56	-23.	0.	0.	0.000	0.	0.	0.00	0.000
264		16.36	16.36	0.	-208	1.44	-22.	0.	0.	0.000	0.	0.	0.00	0.000
265		16.36	16.36	0.	-227	1.57	-23.	0.	0.	0.000	0.	0.	0.00	0.000
266		16.36	16.36	0.	-180	1.25	-19.	0.	0.	0.000	0.	0.	0.00	0.000
267		16.36	16.36	0.	-153	1.06	-16.	0.	0.	0.000	0.	0.	0.00	0.000

268		16.36	16.36	0.	-177	1.22	-18.		0.	0.	0.000	0.	0.	0.00	0.000
293		16.36	16.36	0.	-191	1.31	-20.		0.	0.	0.000	0.	0.	0.00	0.000
294		16.36	16.36	0.	-251	1.73	-26.		0.	0.	0.000	0.	0.	0.00	0.000
295		16.36	16.36	0.	-215	1.48	-22.		0.	0.	0.000	0.	0.	0.00	0.000
296		16.36	16.36	0.	-225	1.55	-23.		0.	0.	0.000	0.	0.	0.00	0.000
297		16.36	16.36	0.	-265	1.83	-27.		0.	0.	0.000	0.	0.	0.00	0.000
298		16.36	16.36	0.	-232	1.60	-24.		0.	0.	0.000	0.	0.	0.00	0.000
299		16.36	16.36	0.	6	0.00	18.		0.	0.	0.000	0.	0.	0.00	0.000
300		16.36	16.36	0.	-11	0.08	-1.		0.	0.	0.000	0.	0.	0.00	0.000
301		16.36	16.36	0.	-17	0.11	-2.		0.	0.	0.000	0.	0.	0.00	0.000
302		16.36	16.36	0.	6	0.00	18.		0.	0.	0.000	0.	0.	0.00	0.000
303		5.89	5.89	0.	8	0.00	67.		0.	0.	0.000	0.	0.	0.00	0.000
304		5.89	5.89	0.	4	0.00	36.		0.	0.	0.000	0.	0.	0.00	0.000
305		5.89	5.89	0.	1	0.00	9.		0.	0.	0.000	0.	0.	0.00	0.000
306		5.89	5.89	0.	-1	0.03	0.		0.	0.	0.000	0.	0.	0.00	0.000
307		5.89	5.89	0.	-1	0.05	-1.		0.	0.	0.000	0.	0.	0.00	0.000
308		5.89	5.89	0.	-4	0.19	-3.		0.	0.	0.000	0.	0.	0.00	0.000
309		5.89	5.89	0.	-2	0.07	-1.		0.	0.	0.000	0.	0.	0.00	0.000
310		5.89	5.89	0.	-5	0.23	-3.		0.	0.	0.000	0.	0.	0.00	0.000
311		5.89	5.89	0.	-1	0.04	-1.		0.	0.	0.000	0.	0.	0.00	0.000
312		5.89	5.89	0.	-4	0.19	-3.		0.	0.	0.000	0.	0.	0.00	0.000
313		5.89	5.89	0.	0.	0.00	0.		0.	0.	0.000	0.	0.	0.00	0.000
314		5.89	5.89	0.	-2	0.08	-1.		0.	0.	0.000	0.	0.	0.00	0.000
315		5.89	5.89	0.	2	0.00	14.		0.	0.	0.000	0.	0.	0.00	0.000
316		5.89	5.89	0.	1	0.00	6.		0.	0.	0.000	0.	0.	0.00	0.000
317		5.89	5.89	0.	4	0.00	35.		0.	0.	0.000	0.	0.	0.00	0.000
318		5.89	5.89	0.	8	0.00	65.		0.	0.	0.000	0.	0.	0.00	0.000
319		6.09	6.09	0.	53	0.00	432.		0.	0.	0.000	0.	0.	0.00	0.000
320		6.09	6.09	0.	37	0.00	305.		0.	0.	0.000	0.	0.	0.00	0.000
321		6.09	6.09	0.	18	0.00	147.		0.	0.	0.000	0.	0.	0.00	0.000
322		6.09	6.09	0.	10	0.00	81.		0.	0.	0.000	0.	0.	0.00	0.000
323		6.09	6.09	0.	4	0.00	35.		0.	0.	0.000	0.	0.	0.00	0.000
324		6.09	6.09	0.	13	0.00	110.		0.	0.	0.000	0.	0.	0.00	0.000
325		6.09	6.09	0.	53	0.00	435.		0.	0.	0.000	0.	0.	0.00	0.000
326		6.09	6.09	0.	37	0.00	308.		0.	0.	0.000	0.	0.	0.00	0.000
327		6.09	6.09	0.	18	0.00	149.		0.	0.	0.000	0.	0.	0.00	0.000
328		6.09	6.09	0.	10	0.00	80.		0.	0.	0.000	0.	0.	0.00	0.000
329		11.98	11.98	0.	5	0.00	22.		0.	0.	0.000	0.	0.	0.00	0.000
330		9.04	9.04	0.	13	0.00	72.		0.	0.	0.000	0.	0.	0.00	0.000
331		5.89	5.89	0.	7	0.00	63.		0.	0.	0.000	0.	0.	0.00	0.000
332		5.89	5.89	0.	12	0.00	102.		0.	0.	0.000	0.	0.	0.00	0.000
333		5.89	5.89	0.	10	0.00	87.		0.	0.	0.000	0.	0.	0.00	0.000
334		5.89	5.89	0.	5	0.00	45.		0.	0.	0.000	0.	0.	0.00	0.000
335		6.09	6.09	0.	3	0.00	22.		0.	0.	0.000	0.	0.	0.00	0.000
336		6.09	6.09	0.	-2	0.04	-1.		0.	0.	0.000	0.	0.	0.00	0.000
337		6.09	6.09	0.	26	0.00	217.		0.	0.	0.000	0.	0.	0.00	0.000
338		6.09	6.09	0.	23	0.00	191.		0.	0.	0.000	0.	0.	0.00	0.000
339		6.09	6.09	0.	51	0.00	417.		0.	0.	0.000	0.	0.	0.00	0.000
340		6.09	6.09	0.	47	0.00	383.		0.	0.	0.000	0.	0.	0.00	0.000
341		6.09	6.09	0.	57	0.00	464.		0.	0.	0.000	0.	0.	0.00	0.000
342		6.09	6.09	0.	63	0.00	515.		0.	0.	0.000	0.	0.	0.00	0.000
343		6.09	6.09	0.	62	0.00	507.		0.	0.	0.000	0.	0.	0.00	0.000
344		6.09	6.09	0.	58	0.00	480.		0.	0.	0.000	0.	0.	0.00	0.000
345		6.09	6.09	0.	57	0.00	469.		0.	0.	0.000	0.	0.	0.00	0.000
346		6.09	6.09	0.	57	0.00	469.		0.	0.	0.000	0.	0.	0.00	0.000
347		6.09	6.09	0.	10	0.00	81.		0.	0.	0.000	0.	0.	0.00	0.000
348		6.09	13.63	0.	19	0.00	159.		0.	0.	0.000	0.	0.	0.00	0.000
349		6.09	13.63	0.	4	0.00	29.		0.	0.	0.000	0.	0.	0.00	0.000
350		6.09	6.09	0.	34	0.00	281.		0.	0.	0.000	0.	0.	0.00	0.000
351		6.09	6.09	0.	43	0.00	352.		0.	0.	0.000	0.	0.	0.00	0.000
352		6.09	6.09	0.	22	0.00	179.		0.	0.	0.000	0.	0.	0.00	0.000
353		6.09	6.09	0.	58	0.00	476.		0.	0.	0.000	0.	0.	0.00	0.000
354		6.09	6.09	0.	66	0.00	541.		0.	0.	0.000	0.	0.	0.00	0.000
355		6.09	6.09	0.	43	0.00	352.		0.	0.	0.000	0.	0.	0.00	0.000
356		6.09	6.09	0.	63	0.00	519.		0.	0.	0.000	0.	0.	0.00	0.000
357		6.09	6.09	0.	68	0.00	561.		0.	0.	0.000	0.	0.	0.00	0.000
358		6.09	6.09	0.	48	0.00	391.		0.	0.	0.000	0.	0.	0.00	0.000
359		6.09	6.09	0.	64	0.00	526.		0.	0.	0.000	0.	0.	0.00	0.000
360		6.09	6.09	0.	67	0.00	552.		0.	0.	0.000	0.	0.	0.00	0.000
361		6.09	6.09	0.	49	0.00	400.		0.	0.	0.000	0.	0.	0.00	0.000
362		6.09	6.09	0.	61	0.00	500.		0.	0.	0.000	0.	0.	0.00	0.000
363		6.09	6.09	0.	64	0.00	526.		0.	0.	0.000	0.	0.	0.00	0.000
364		6.09	6.09	0.	50	0.00	407.		0.	0.	0.000	0.	0.	0.00	0.000
365		10.18	10.18	0.	8	0.00	39.		0.	0.	0.000	0.	0.	0.00	0.000
366		10.18	10.18	0.	-3	0.08	-1.		0.	0.	0.000	0.	0.	0.00	0.000
367		6.09	6.09	0.	30	0.00	249.		0.	0.	0.000	0.	0.	0.00	0.000

368		6.09	6.09	0.	23	0.00	186.		0.	0.	0.000	0.	0.	0.00	0.000
369		6.09	6.09	0.	52	0.00	429.		0.	0.	0.000	0.	0.	0.00	0.000
370		6.09	6.09	0.	47	0.00	384.		0.	0.	0.000	0.	0.	0.00	0.000
371		6.09	6.09	0.	56	0.00	461.		0.	0.	0.000	0.	0.	0.00	0.000
372		6.09	6.09	0.	63	0.00	514.		0.	0.	0.000	0.	0.	0.00	0.000
373		6.09	6.09	0.	62	0.00	511.		0.	0.	0.000	0.	0.	0.00	0.000
374		6.09	6.09	0.	59	0.00	485.		0.	0.	0.000	0.	0.	0.00	0.000
375		6.09	6.09	0.	58	0.00	478.		0.	0.	0.000	0.	0.	0.00	0.000
376		6.09	6.09	0.	57	0.00	471.		0.	0.	0.000	0.	0.	0.00	0.000
377		6.09	6.09	0.	61	0.00	500.		0.	0.	0.000	0.	0.	0.00	0.000
378		6.09	6.09	0.	64	0.00	525.		0.	0.	0.000	0.	0.	0.00	0.000
379		6.09	6.09	0.	50	0.00	407.		0.	0.	0.000	0.	0.	0.00	0.000
380		6.09	6.09	0.	64	0.00	527.		0.	0.	0.000	0.	0.	0.00	0.000
381		6.09	6.09	0.	67	0.00	551.		0.	0.	0.000	0.	0.	0.00	0.000
382		6.09	6.09	0.	49	0.00	400.		0.	0.	0.000	0.	0.	0.00	0.000
383		6.09	6.09	0.	64	0.00	525.		0.	0.	0.000	0.	0.	0.00	0.000
384		6.09	6.09	0.	68	0.00	560.		0.	0.	0.000	0.	0.	0.00	0.000
385		6.09	6.09	0.	48	0.00	390.		0.	0.	0.000	0.	0.	0.00	0.000
386		6.09	6.09	0.	60	0.00	492.		0.	0.	0.000	0.	0.	0.00	0.000
387		6.09	6.09	0.	65	0.00	534.		0.	0.	0.000	0.	0.	0.00	0.000
388		6.09	6.09	0.	43	0.00	351.		0.	0.	0.000	0.	0.	0.00	0.000
389		6.09	6.09	0.	38	0.00	310.		0.	0.	0.000	0.	0.	0.00	0.000
390		6.09	7.97	0.	43	0.00	350.		0.	0.	0.000	0.	0.	0.00	0.000
391		6.09	7.97	0.	21	0.00	169.		0.	0.	0.000	0.	0.	0.00	0.000
392		10.18	10.18	0.	14	0.00	69.		0.	0.	0.000	0.	0.	0.00	0.000
393		10.18	17.72	0.	18	0.00	88.		0.	0.	0.000	0.	0.	0.00	0.000
394		10.18	17.72	0.	0.	0.00	0.		0.	0.	0.000	0.	0.	0.00	0.000

ARMATURA SUPERIORE ORIZZONTALE

GUSCI	COMBINAZIONE RARA		COMB. FREQUENTE			COMB. QUASI PERMANENTE									
	Af	Afc	Mom	Nor	sigC	sigF	Mom	Nor	WkF	Mom	Nor	sigC	WkP		
205		16.76	16.76	4859	61	1.27	399.		0.	0.	0.000	0.	0.	0.00	0.000
206		16.76	16.76	7289	100	1.43	622.		0.	0.	0.000	0.	0.	0.00	0.000
207		16.76	16.76	6441	70	2.21	495.		0.	0.	0.000	0.	0.	0.00	0.000
208		16.76	16.76	6441	70	2.21	495.		0.	0.	0.000	0.	0.	0.00	0.000
209		16.76	16.76	6828	82	1.99	548.		0.	0.	0.000	0.	0.	0.00	0.000
210		16.76	16.76	6828	82	1.99	548.		0.	0.	0.000	0.	0.	0.00	0.000
211		16.76	16.76	8707	85	3.34	642.		0.	0.	0.000	0.	0.	0.00	0.000
212		16.76	16.76	8707	85	3.34	642.		0.	0.	0.000	0.	0.	0.00	0.000
213		16.76	16.76	8420	112	1.87	709.		0.	0.	0.000	0.	0.	0.00	0.000
214		16.76	16.76	8420	112	1.87	709.		0.	0.	0.000	0.	0.	0.00	0.000
215		16.76	16.76	6736	113	0.00	639.		0.	0.	0.000	0.	0.	0.00	0.000
216		16.76	16.76	6736	113	0.00	639.		0.	0.	0.000	0.	0.	0.00	0.000
217		16.76	16.76	6739	85	1.74	554.		0.	0.	0.000	0.	0.	0.00	0.000
218		16.76	16.76	6739	85	1.74	554.		0.	0.	0.000	0.	0.	0.00	0.000
219		16.76	16.76	7111	104	0.84	628.		0.	0.	0.000	0.	0.	0.00	0.000
220		16.76	16.76	4778	64	1.01	404.		0.	0.	0.000	0.	0.	0.00	0.000
221		16.76	16.76	4859	61	1.27	399.		0.	0.	0.000	0.	0.	0.00	0.000
222		16.76	16.76	4859	61	1.27	399.		0.	0.	0.000	0.	0.	0.00	0.000
223		16.76	16.76	4859	61	1.27	399.		0.	0.	0.000	0.	0.	0.00	0.000
224		16.76	16.76	7289	100	1.43	622.		0.	0.	0.000	0.	0.	0.00	0.000
225		16.76	16.76	7289	100	1.43	622.		0.	0.	0.000	0.	0.	0.00	0.000
226		16.76	16.76	7289	100	1.43	622.		0.	0.	0.000	0.	0.	0.00	0.000
227		16.76	16.76	6441	70	2.21	495.		0.	0.	0.000	0.	0.	0.00	0.000
228		16.76	16.76	6441	70	2.21	495.		0.	0.	0.000	0.	0.	0.00	0.000
229		16.76	16.76	6441	70	2.21	495.		0.	0.	0.000	0.	0.	0.00	0.000
230		16.76	16.76	6828	82	1.99	548.		0.	0.	0.000	0.	0.	0.00	0.000
231		16.76	16.76	6828	82	1.99	548.		0.	0.	0.000	0.	0.	0.00	0.000
232		16.76	16.76	6828	82	1.99	548.		0.	0.	0.000	0.	0.	0.00	0.000
233		16.76	16.76	8707	85	3.34	642.		0.	0.	0.000	0.	0.	0.00	0.000
234		16.76	16.76	8707	85	3.34	642.		0.	0.	0.000	0.	0.	0.00	0.000
235		16.76	16.76	8707	85	3.34	642.		0.	0.	0.000	0.	0.	0.00	0.000
236		16.76	16.76	8420	112	1.87	709.		0.	0.	0.000	0.	0.	0.00	0.000
237		16.76	16.76	8420	112	1.87	709.		0.	0.	0.000	0.	0.	0.00	0.000
238		16.76	16.76	8420	112	1.87	709.		0.	0.	0.000	0.	0.	0.00	0.000
239		16.76	16.76	6736	113	0.00	639.		0.	0.	0.000	0.	0.	0.00	0.000
240		16.76	16.76	6736	113	0.00	639.		0.	0.	0.000	0.	0.	0.00	0.000
241		16.76	16.76	6736	113	0.00	639.		0.	0.	0.000	0.	0.	0.00	0.000
242		16.76	16.76	6739	85	1.74	554.		0.	0.	0.000	0.	0.	0.00	0.000
243		16.76	16.76	6739	85	1.74	554.		0.	0.	0.000	0.	0.	0.00	0.000
244		16.76	16.76	6739	85	1.74	554.		0.	0.	0.000	0.	0.	0.00	0.000
245		16.76	16.76	7111	104	0.84	628.		0.	0.	0.000	0.	0.	0.00	0.000
246		16.76	16.76	7111	104	0.84	628.		0.	0.	0.000	0.	0.	0.00	0.000
247		16.76	16.76	7111	104	0.84	628.		0.	0.	0.000	0.	0.	0.00	0.000
248		16.76	16.76	4778	64	1.01	404.		0.	0.	0.000	0.	0.	0.00	0.000

249		16.76	16.76	4778	64	1.01	404.		0.	0.	0.000	0.	0.	0.00	0.000
250		16.76	16.76	4778	64	1.01	404.		0.	0.	0.000	0.	0.	0.00	0.000
251		16.76	16.76	4859	61	1.27	399.		0.	0.	0.000	0.	0.	0.00	0.000
252		16.76	16.76	5004	55	1.67	388.		0.	0.	0.000	0.	0.	0.00	0.000
253		16.76	16.76	7289	100	1.43	622.		0.	0.	0.000	0.	0.	0.00	0.000
254		16.76	16.76	6441	70	2.21	495.		0.	0.	0.000	0.	0.	0.00	0.000
255		16.76	16.76	6634	58	2.78	469.		0.	0.	0.000	0.	0.	0.00	0.000
256		16.76	16.76	6828	82	1.99	548.		0.	0.	0.000	0.	0.	0.00	0.000
257		16.76	16.76	7033	69	2.68	520.		0.	0.	0.000	0.	0.	0.00	0.000
258		16.76	16.76	8707	85	3.34	642.		0.	0.	0.000	0.	0.	0.00	0.000
259		16.76	16.76	8968	73	3.92	618.		0.	0.	0.000	0.	0.	0.00	0.000
260		16.76	16.76	8420	112	1.87	709.		0.	0.	0.000	0.	0.	0.00	0.000
261		16.76	16.76	8673	98	2.83	677.		0.	0.	0.000	0.	0.	0.00	0.000
262		16.76	16.76	6736	113	0.00	639.		0.	0.	0.000	0.	0.	0.00	0.000
263		16.76	16.76	6938	100	1.01	606.		0.	0.	0.000	0.	0.	0.00	0.000
264		16.76	16.76	6739	85	1.74	554.		0.	0.	0.000	0.	0.	0.00	0.000
265		16.76	16.76	6941	73	2.48	527.		0.	0.	0.000	0.	0.	0.00	0.000
266		16.76	16.76	7111	104	0.84	628.		0.	0.	0.000	0.	0.	0.00	0.000
267		16.76	16.76	4778	64	1.01	404.		0.	0.	0.000	0.	0.	0.00	0.000
268		16.76	16.76	4920	58	1.48	393.		0.	0.	0.000	0.	0.	0.00	0.000
293		16.76	16.76	6462	99	0.32	582.		0.	0.	0.000	0.	0.	0.00	0.000
294		16.76	16.76	7403	102	1.41	634.		0.	0.	0.000	0.	0.	0.00	0.000
295		16.76	16.76	6700	52	3.00	454.		0.	0.	0.000	0.	0.	0.00	0.000
296		16.76	16.76	6409	27	3.37	370.		0.	0.	0.000	0.	0.	0.00	0.000
297		16.76	16.76	7419	97	1.73	620.		0.	0.	0.000	0.	0.	0.00	0.000
298		16.76	16.76	6593	93	1.13	570.		0.	0.	0.000	0.	0.	0.00	0.000
299		16.76	16.76	4786	60	1.25	393.		0.	0.	0.000	0.	0.	0.00	0.000
300		16.76	16.76	7172	100	1.30	617.		0.	0.	0.000	0.	0.	0.00	0.000
301		16.76	16.76	7004	104	0.69	623.		0.	0.	0.000	0.	0.	0.00	0.000
302		16.76	16.76	4705	63	0.98	399.		0.	0.	0.000	0.	0.	0.00	0.000
303		8.67	6.79	62	40	0.00	284.		0.	0.	0.000	0.	0.	0.00	0.000
304		8.67	6.79	31	56	0.00	351.		0.	0.	0.000	0.	0.	0.00	0.000
305		8.67	6.79	30	60	0.00	370.		0.	0.	0.000	0.	0.	0.00	0.000
306		14.33	6.79	2185	53	38.06	1212.		0.	0.	0.000	0.	0.	0.00	0.000
307		8.67	6.79	31	59	0.00	363.		0.	0.	0.000	0.	0.	0.00	0.000
308		14.33	6.79	2384	51	41.83	1300.		0.	0.	0.000	0.	0.	0.00	0.000
309		8.67	6.79	31	58	0.00	363.		0.	0.	0.000	0.	0.	0.00	0.000
310		14.33	6.79	2487	51	43.75	1347.		0.	0.	0.000	0.	0.	0.00	0.000
311		8.67	6.79	32	68	0.00	419.		0.	0.	0.000	0.	0.	0.00	0.000
312		14.33	6.79	2509	55	43.96	1373.		0.	0.	0.000	0.	0.	0.00	0.000
313		8.67	6.79	32	67	0.00	413.		0.	0.	0.000	0.	0.	0.00	0.000
314		14.33	6.79	2445	53	42.85	1336.		0.	0.	0.000	0.	0.	0.00	0.000
315		8.67	6.79	32	62	0.00	383.		0.	0.	0.000	0.	0.	0.00	0.000
316		14.33	6.79	2311	50	40.51	1264.		0.	0.	0.000	0.	0.	0.00	0.000
317		8.67	6.79	34	56	0.00	351.		0.	0.	0.000	0.	0.	0.00	0.000
318		8.67	6.79	66	41	0.00	293.		0.	0.	0.000	0.	0.	0.00	0.000
319		6.03	6.03	1453	64	35.33	2116.		0.	0.	0.000	0.	0.	0.00	0.000
320		6.03	6.03	1404	72	33.60	2132.		0.	0.	0.000	0.	0.	0.00	0.000
321		6.03	6.03	907	68	20.31	1570.		0.	0.	0.000	0.	0.	0.00	0.000
322		6.03	6.03	1518	66	36.94	2203.		0.	0.	0.000	0.	0.	0.00	0.000
323		6.03	6.03	976	62	22.68	1587.		0.	0.	0.000	0.	0.	0.00	0.000
324		6.03	6.03	239	60	0.00	777.		0.	0.	0.000	0.	0.	0.00	0.000
325		6.03	6.03	1451	64	35.27	2112.		0.	0.	0.000	0.	0.	0.00	0.000
326		6.03	6.03	1400	72	33.47	2131.		0.	0.	0.000	0.	0.	0.00	0.000
327		6.03	6.03	901	68	20.15	1566.		0.	0.	0.000	0.	0.	0.00	0.000
328		6.03	6.03	1507	66	36.67	2191.		0.	0.	0.000	0.	0.	0.00	0.000
329		6.03	6.03	968	61	22.47	1574.		0.	0.	0.000	0.	0.	0.00	0.000
330		6.03	6.03	236	59	0.00	771.		0.	0.	0.000	0.	0.	0.00	0.000
331		14.33	6.79	1525	29	26.90	821.		0.	0.	0.000	0.	0.	0.00	0.000
332		14.33	6.79	1890	51	32.65	1068.		0.	0.	0.000	0.	0.	0.00	0.000
333		14.33	6.79	1940	46	33.83	1073.		0.	0.	0.000	0.	0.	0.00	0.000
334		14.33	6.79	1663	30	29.46	886.		0.	0.	0.000	0.	0.	0.00	0.000
335		6.03	6.03	3897	97	24.74	2667.		0.	0.	0.000	0.	0.	0.00	0.000
336		6.03	6.03	2670	112	13.44	2215.		0.	0.	0.000	0.	0.	0.00	0.000
337		6.03	6.03	2642	89	15.26	1999.		0.	0.	0.000	0.	0.	0.00	0.000
338		6.03	6.03	2351	111	10.58	2051.		0.	0.	0.000	0.	0.	0.00	0.000
339		6.03	6.03	1710	70	8.77	1404.		0.	0.	0.000	0.	0.	0.00	0.000
340		6.03	6.03	1747	91	6.85	1594.		0.	0.	0.000	0.	0.	0.00	0.000
341		6.03	6.03	264	12	1.27	224.		0.	0.	0.000	0.	0.	0.00	0.000
342		6.03	6.03	513	29	1.63	490.		0.	0.	0.000	0.	0.	0.00	0.000
343		6.03	6.03	889	49	3.06	837.		0.	0.	0.000	0.	0.	0.00	0.000
344		6.03	6.03	1058	46	5.15	892.		0.	0.	0.000	0.	0.	0.00	0.000
345		6.03	6.03	1207	60	5.09	1078.		0.	0.	0.000	0.	0.	0.00	0.000
346		6.03	6.03	1282	67	4.98	1173.		0.	0.	0.000	0.	0.	0.00	0.000
347		12.63	6.03	5767	57	29.86	1560.		0.	0.	0.000	0.	0.	0.00	0.000
348		12.63	6.03	6370	38	33.75	1632.		0.	0.	0.000	0.	0.	0.00	0.000

349		12.63	6.03	7152	17	38.60	1738.		0.	0.	0.000	0.	0.	0.00	0.000
350		7.68	6.03	3082	40	19.22	1419.		0.	0.	0.000	0.	0.	0.00	0.000
351		7.68	6.03	3146	21	20.30	1322.		0.	0.	0.000	0.	0.	0.00	0.000
352		7.68	6.03	3177	-3	21.09	1184.		0.	0.	0.000	0.	0.	0.00	0.000
353		6.03	6.03	1668	37	10.86	1103.		0.	0.	0.000	0.	0.	0.00	0.000
354		6.03	6.03	1607	19	11.22	921.		0.	0.	0.000	0.	0.	0.00	0.000
355		6.03	6.03	1481	-2	10.85	695.		0.	0.	0.000	0.	0.	0.00	0.000
356		6.03	6.03	970	34	5.53	742.		0.	0.	0.000	0.	0.	0.00	0.000
357		6.03	6.03	901	20	5.88	592.		0.	0.	0.000	0.	0.	0.00	0.000
358		6.03	6.03	809	5	5.80	425.		0.	0.	0.000	0.	0.	0.00	0.000
359		6.03	6.03	535	21	2.83	431.		0.	0.	0.000	0.	0.	0.00	0.000
360		6.03	6.03	530	20	2.86	422.		0.	0.	0.000	0.	0.	0.00	0.000
361		6.03	6.03	473	11	3.06	315.		0.	0.	0.000	0.	0.	0.00	0.000
362		6.03	6.03	247	9	1.34	196.		0.	0.	0.000	0.	0.	0.00	0.000
363		6.03	6.03	247	9	1.34	196.		0.	0.	0.000	0.	0.	0.00	0.000
364		6.03	6.03	232	8	1.33	175.		0.	0.	0.000	0.	0.	0.00	0.000
365		7.65	6.03	3889	98	22.00	2111.		0.	0.	0.000	0.	0.	0.00	0.000
366		6.03	6.03	2661	113	13.35	2211.		0.	0.	0.000	0.	0.	0.00	0.000
367		6.03	6.03	2640	90	15.16	2006.		0.	0.	0.000	0.	0.	0.00	0.000
368		6.03	6.03	2347	112	10.45	2056.		0.	0.	0.000	0.	0.	0.00	0.000
369		6.03	6.03	1709	71	8.74	1406.		0.	0.	0.000	0.	0.	0.00	0.000
370		6.03	6.03	1745	91	6.82	1594.		0.	0.	0.000	0.	0.	0.00	0.000
371		6.03	6.03	264	12	1.28	223.		0.	0.	0.000	0.	0.	0.00	0.000
372		6.03	6.03	512	29	1.63	490.		0.	0.	0.000	0.	0.	0.00	0.000
373		6.03	6.03	888	49	3.05	837.		0.	0.	0.000	0.	0.	0.00	0.000
374		6.03	6.03	1057	46	5.14	892.		0.	0.	0.000	0.	0.	0.00	0.000
375		6.03	6.03	1206	60	5.09	1076.		0.	0.	0.000	0.	0.	0.00	0.000
376		6.03	6.03	1280	67	4.98	1171.		0.	0.	0.000	0.	0.	0.00	0.000
377		6.03	6.03	247	9	1.34	196.		0.	0.	0.000	0.	0.	0.00	0.000
378		6.03	6.03	247	9	1.34	196.		0.	0.	0.000	0.	0.	0.00	0.000
379		6.03	6.03	231	8	1.33	175.		0.	0.	0.000	0.	0.	0.00	0.000
380		6.03	6.03	534	21	2.83	430.		0.	0.	0.000	0.	0.	0.00	0.000
381		6.03	6.03	530	20	2.85	422.		0.	0.	0.000	0.	0.	0.00	0.000
382		6.03	6.03	472	11	3.05	316.		0.	0.	0.000	0.	0.	0.00	0.000
383		6.03	6.03	969	34	5.51	742.		0.	0.	0.000	0.	0.	0.00	0.000
384		6.03	6.03	900	20	5.87	593.		0.	0.	0.000	0.	0.	0.00	0.000
385		6.03	6.03	808	5	5.79	427.		0.	0.	0.000	0.	0.	0.00	0.000
386		6.03	6.03	1667	37	10.83	1104.		0.	0.	0.000	0.	0.	0.00	0.000
387		6.03	6.03	1606	19	11.20	923.		0.	0.	0.000	0.	0.	0.00	0.000
388		6.03	6.03	1480	-1	10.84	697.		0.	0.	0.000	0.	0.	0.00	0.000
389		7.65	6.03	3080	41	19.20	1431.		0.	0.	0.000	0.	0.	0.00	0.000
390		7.65	6.03	3146	22	20.29	1334.		0.	0.	0.000	0.	0.	0.00	0.000
391		7.65	6.03	3177	-2	21.10	1197.		0.	0.	0.000	0.	0.	0.00	0.000
392		12.49	6.03	5761	58	29.91	1580.		0.	0.	0.000	0.	0.	0.00	0.000
393		12.49	6.03	6368	40	33.83	1655.		0.	0.	0.000	0.	0.	0.00	0.000
394		12.49	6.03	7154	19	38.72	1764.		0.	0.	0.000	0.	0.	0.00	0.000

ARMATURA SUPERIORE VERTICALE

GUSCI	COMBINAZIONE RARA						COMB. FREQUENTE			COMB. QUASI PERMANENTE					
	Af	Afc	Mom	Nor	sigC	sigF	Mom	Nor	WkF	Mom	Nor	sigC	WkP		
205		16.36	16.36	1126	21	0.00	116.		0.	0.	0.000	0.	0.	0.00	0.000
206		16.36	16.36	1081	1	0.62	54.		0.	0.	0.000	0.	0.	0.00	0.000
207		16.36	16.36	874	-30	0.46	0.		0.	0.	0.000	0.	0.	0.00	0.000
208		16.36	16.36	1086	-18	0.57	9.		0.	0.	0.000	0.	0.	0.00	0.000
209		16.36	16.36	872	-39	0.03	-8.		0.	0.	0.000	0.	0.	0.00	0.000
210		16.36	16.36	1140	-49	0.02	-10.		0.	0.	0.000	0.	0.	0.00	0.000
211		16.36	16.36	913	-54	0.12	-9.		0.	0.	0.000	0.	0.	0.00	0.000
212		16.36	16.36	1225	-79	0.20	-13.		0.	0.	0.000	0.	0.	0.00	0.000
213		16.36	16.36	983	-59	0.13	-10.		0.	0.	0.000	0.	0.	0.00	0.000
214		16.36	16.36	1308	-78	0.17	-13.		0.	0.	0.000	0.	0.	0.00	0.000
215		16.36	16.36	1056	-45	0.01	-9.		0.	0.	0.000	0.	0.	0.00	0.000
216		16.36	16.36	1372	-48	0.72	1.		0.	0.	0.000	0.	0.	0.00	0.000
217		16.36	16.36	1121	-36	0.57	1.		0.	0.	0.000	0.	0.	0.00	0.000
218		16.36	16.36	1407	-18	0.79	21.		0.	0.	0.000	0.	0.	0.00	0.000
219		16.36	16.36	1468	-2	0.88	64.		0.	0.	0.000	0.	0.	0.00	0.000
220		16.36	16.36	1497	15	0.56	115.		0.	0.	0.000	0.	0.	0.00	0.000
221		16.36	16.36	1990	9	1.05	120.		0.	0.	0.000	0.	0.	0.00	0.000
222		16.36	16.36	3196	-2	1.90	145.		0.	0.	0.000	0.	0.	0.00	0.000
223		16.36	16.36	4791	-22	2.93	164.		0.	0.	0.000	0.	0.	0.00	0.000
224		16.36	16.36	1966	-10	1.20	64.		0.	0.	0.000	0.	0.	0.00	0.000
225		16.36	16.36	3233	-19	1.98	100.		0.	0.	0.000	0.	0.	0.00	0.000
226		16.36	16.36	4892	-39	2.95	124.		0.	0.	0.000	0.	0.	0.00	0.000
227		16.36	16.36	1935	-34	1.00	15.		0.	0.	0.000	0.	0.	0.00	0.000
228		16.36	16.36	3231	-46	1.78	41.		0.	0.	0.000	0.	0.	0.00	0.000
229		16.36	16.36	5066	-65	2.87	77.		0.	0.	0.000	0.	0.	0.00	0.000

230		16.36	16.36	1915	-75	0.02	-15.	0.	0.	0.000	0.	0.	0.00	0.000
231		16.36	16.36	3214	-88	1.58	6.	0.	0.	0.000	0.	0.	0.00	0.000
232		16.36	16.36	5041	-109	2.48	22.	0.	0.	0.000	0.	0.	0.00	0.000
233		16.36	16.36	1963	-109	0.21	-19.	0.	0.	0.000	0.	0.	0.00	0.000
234		16.36	16.36	3201	-120	1.73	0.	0.	0.	0.000	0.	0.	0.00	0.000
235		16.36	16.36	5028	-114	2.46	19.	0.	0.	0.000	0.	0.	0.00	0.000
236		16.36	16.36	2047	-91	0.06	-18.	0.	0.	0.000	0.	0.	0.00	0.000
237		16.36	16.36	3277	-100	1.64	4.	0.	0.	0.000	0.	0.	0.00	0.000
238		16.36	16.36	5086	-105	2.52	26.	0.	0.	0.000	0.	0.	0.00	0.000
239		16.36	16.36	2109	-57	1.03	4.	0.	0.	0.000	0.	0.	0.00	0.000
240		16.36	16.36	3336	-68	1.66	17.	0.	0.	0.000	0.	0.	0.00	0.000
241		16.36	16.36	5145	-88	2.68	43.	0.	0.	0.000	0.	0.	0.00	0.000
242		16.36	16.36	2128	-18	1.28	51.	0.	0.	0.000	0.	0.	0.00	0.000
243		16.36	16.36	3351	-23	2.04	96.	0.	0.	0.000	0.	0.	0.00	0.000
244		16.36	16.36	5170	-43	3.11	128.	0.	0.	0.000	0.	0.	0.00	0.000
245		16.36	16.36	2143	4	1.23	110.	0.	0.	0.000	0.	0.	0.00	0.000
246		16.36	16.36	3331	3	1.93	165.	0.	0.	0.000	0.	0.	0.00	0.000
247		16.36	16.36	4994	-15	3.04	192.	0.	0.	0.000	0.	0.	0.00	0.000
248		16.36	16.36	2151	21	0.84	162.	0.	0.	0.000	0.	0.	0.00	0.000
249		18.25	16.36	3294	22	1.51	196.	0.	0.	0.000	0.	0.	0.00	0.000
250		18.25	16.36	4894	-32	2.87	129.	0.	0.	0.000	0.	0.	0.00	0.000
251		16.36	16.36	10688	-204	5.39	67.	0.	0.	0.000	0.	0.	0.00	0.000
252		16.36	16.36	15436	-226	8.43	183.	0.	0.	0.000	0.	0.	0.00	0.000
253		16.36	16.36	10458	-220	5.17	50.	0.	0.	0.000	0.	0.	0.00	0.000
254		16.36	16.36	10090	-210	4.99	49.	0.	0.	0.000	0.	0.	0.00	0.000
255		16.36	16.36	15571	-227	8.51	185.	0.	0.	0.000	0.	0.	0.00	0.000
256		16.36	16.36	10063	-209	4.98	49.	0.	0.	0.000	0.	0.	0.00	0.000
257		16.36	16.36	15543	-226	8.50	186.	0.	0.	0.000	0.	0.	0.00	0.000
258		16.36	16.36	10063	-209	4.98	49.	0.	0.	0.000	0.	0.	0.00	0.000
259		16.36	16.36	15543	-226	8.50	186.	0.	0.	0.000	0.	0.	0.00	0.000
260		16.36	16.36	10063	-209	4.98	49.	0.	0.	0.000	0.	0.	0.00	0.000
261		16.36	16.36	15543	-226	8.50	186.	0.	0.	0.000	0.	0.	0.00	0.000
262		16.36	16.36	10063	-209	4.98	49.	0.	0.	0.000	0.	0.	0.00	0.000
263		16.36	16.36	15543	-226	8.50	186.	0.	0.	0.000	0.	0.	0.00	0.000
264		16.36	16.36	10045	-208	4.98	50.	0.	0.	0.000	0.	0.	0.00	0.000
265		16.36	16.36	15594	-227	8.53	187.	0.	0.	0.000	0.	0.	0.00	0.000
266		16.36	16.36	10287	-180	5.32	81.	0.	0.	0.000	0.	0.	0.00	0.000
267		16.36	16.36	10509	-153	5.74	125.	0.	0.	0.000	0.	0.	0.00	0.000
268		16.36	16.36	15480	-177	8.96	275.	0.	0.	0.000	0.	0.	0.00	0.000
293		16.36	16.36	15544	-191	8.88	250.	0.	0.	0.000	0.	0.	0.00	0.000
294		16.36	16.36	16925	-251	9.20	195.	0.	0.	0.000	0.	0.	0.00	0.000
295		16.36	16.36	14918	-215	8.19	183.	0.	0.	0.000	0.	0.	0.00	0.000
296		16.36	16.36	14964	-225	8.11	168.	0.	0.	0.000	0.	0.	0.00	0.000
297		16.36	16.36	16959	-265	9.08	175.	0.	0.	0.000	0.	0.	0.00	0.000
298		16.36	16.36	15591	-232	8.48	179.	0.	0.	0.000	0.	0.	0.00	0.000
299		16.36	16.36	709	6	0.31	50.	0.	0.	0.000	0.	0.	0.00	0.000
300		16.36	16.36	778	-11	0.42	9.	0.	0.	0.000	0.	0.	0.00	0.000
301		16.36	16.36	1122	-17	0.61	13.	0.	0.	0.000	0.	0.	0.00	0.000
302		16.36	16.36	1117	6	0.58	69.	0.	0.	0.000	0.	0.	0.00	0.000
303		5.89	5.89	37	8	0.00	112.	0.	0.	0.000	0.	0.	0.00	0.000
304		5.89	5.89	32	4	0.53	73.	0.	0.	0.000	0.	0.	0.00	0.000
305		5.89	5.89	24	1	0.60	36.	0.	0.	0.000	0.	0.	0.00	0.000
306		5.89	5.89	110	-1	2.88	116.	0.	0.	0.000	0.	0.	0.00	0.000
307		5.89	5.89	22	-1	0.56	15.	0.	0.	0.000	0.	0.	0.00	0.000
308		5.89	5.89	115	-4	3.01	93.	0.	0.	0.000	0.	0.	0.00	0.000
309		5.89	5.89	19	-2	0.48	9.	0.	0.	0.000	0.	0.	0.00	0.000
310		5.89	5.89	117	-5	3.05	88.	0.	0.	0.000	0.	0.	0.00	0.000
311		5.89	5.89	20	-1	0.52	14.	0.	0.	0.000	0.	0.	0.00	0.000
312		5.89	5.89	119	-4	3.10	97.	0.	0.	0.000	0.	0.	0.00	0.000
313		5.89	5.89	23	0.	0.59	25.	0.	0.	0.000	0.	0.	0.00	0.000
314		5.89	5.89	117	-2	3.05	114.	0.	0.	0.000	0.	0.	0.00	0.000
315		5.89	5.89	26	2	0.61	44.	0.	0.	0.000	0.	0.	0.00	0.000
316		5.89	5.89	112	1	2.91	130.	0.	0.	0.000	0.	0.	0.00	0.000
317		5.89	5.89	33	4	0.60	74.	0.	0.	0.000	0.	0.	0.00	0.000
318		5.89	5.89	39	8	0.14	113.	0.	0.	0.000	0.	0.	0.00	0.000
319		6.09	6.09	129	53	0.00	584.	0.	0.	0.000	0.	0.	0.00	0.000
320		6.09	6.09	179	37	0.00	515.	0.	0.	0.000	0.	0.	0.00	0.000
321		6.09	6.09	142	18	2.45	308.	0.	0.	0.000	0.	0.	0.00	0.000
322		6.09	6.09	157	10	3.62	252.	0.	0.	0.000	0.	0.	0.00	0.000
323		6.09	6.09	142	4	3.51	188.	0.	0.	0.000	0.	0.	0.00	0.000
324		6.09	6.09	60	13	0.00	180.	0.	0.	0.000	0.	0.	0.00	0.000
325		6.09	6.09	129	53	0.00	586.	0.	0.	0.000	0.	0.	0.00	0.000
326		6.09	6.09	178	37	0.00	516.	0.	0.	0.000	0.	0.	0.00	0.000
327		6.09	6.09	140	18	2.36	307.	0.	0.	0.000	0.	0.	0.00	0.000
328		6.09	6.09	154	10	3.57	249.	0.	0.	0.000	0.	0.	0.00	0.000
329		11.98	11.98	139	5	2.38	100.	0.	0.	0.000	0.	0.	0.00	0.000

330		9.04	9.04	58	13	0.00	117.	0.	0.	0.000	0.	0.	0.00	0.000
331		5.89	5.89	109	7	2.52	186.	0.	0.	0.000	0.	0.	0.00	0.000
332		5.89	5.89	98	12	1.80	216.	0.	0.	0.000	0.	0.	0.00	0.000
333		5.89	5.89	102	10	2.10	204.	0.	0.	0.000	0.	0.	0.00	0.000
334		5.89	5.89	112	5	2.74	171.	0.	0.	0.000	0.	0.	0.00	0.000
335		6.09	6.09	1540	3	11.14	752.	0.	0.	0.000	0.	0.	0.00	0.000
336		6.09	6.09	1258	-2	9.17	584.	0.	0.	0.000	0.	0.	0.00	0.000
337		6.09	6.09	1312	26	8.63	837.	0.	0.	0.000	0.	0.	0.00	0.000
338		6.09	6.09	1010	23	6.50	668.	0.	0.	0.000	0.	0.	0.00	0.000
339		6.09	6.09	1019	51	4.24	903.	0.	0.	0.000	0.	0.	0.00	0.000
340		6.09	6.09	802	47	2.36	768.	0.	0.	0.000	0.	0.	0.00	0.000
341		6.09	6.09	662	57	0.00	784.	0.	0.	0.000	0.	0.	0.00	0.000
342		6.09	6.09	830	63	0.00	916.	0.	0.	0.000	0.	0.	0.00	0.000
343		6.09	6.09	954	62	1.50	967.	0.	0.	0.000	0.	0.	0.00	0.000
344		6.09	6.09	897	58	1.32	912.	0.	0.	0.000	0.	0.	0.00	0.000
345		6.09	6.09	998	57	3.09	948.	0.	0.	0.000	0.	0.	0.00	0.000
346		6.09	6.09	862	57	1.01	884.	0.	0.	0.000	0.	0.	0.00	0.000
347		6.09	6.09	2097	10	15.03	1074.	0.	0.	0.000	0.	0.	0.00	0.000
348		13.63	6.09	2903	19	14.86	697.	0.	0.	0.000	0.	0.	0.00	0.000
349		13.63	6.09	3888	4	20.53	858.	0.	0.	0.000	0.	0.	0.00	0.000
350		6.09	6.09	1762	34	11.66	1113.	0.	0.	0.000	0.	0.	0.00	0.000
351		6.09	6.09	2366	43	15.80	1469.	0.	0.	0.000	0.	0.	0.00	0.000
352		6.09	6.09	3047	22	21.62	1620.	0.	0.	0.000	0.	0.	0.00	0.000
353		6.09	6.09	1351	58	6.66	1119.	0.	0.	0.000	0.	0.	0.00	0.000
354		6.09	6.09	1840	66	10.24	1413.	0.	0.	0.000	0.	0.	0.00	0.000
355		6.09	6.09	2491	43	16.74	1529.	0.	0.	0.000	0.	0.	0.00	0.000
356		6.09	6.09	1171	63	4.23	1079.	0.	0.	0.000	0.	0.	0.00	0.000
357		6.09	6.09	1584	68	7.77	1315.	0.	0.	0.000	0.	0.	0.00	0.000
358		6.09	6.09	2061	48	13.24	1364.	0.	0.	0.000	0.	0.	0.00	0.000
359		6.09	6.09	1005	64	1.84	1011.	0.	0.	0.000	0.	0.	0.00	0.000
360		6.09	6.09	1331	67	5.42	1188.	0.	0.	0.000	0.	0.	0.00	0.000
361		6.09	6.09	1796	49	11.11	1250.	0.	0.	0.000	0.	0.	0.00	0.000
362		6.09	6.09	832	61	0.00	902.	0.	0.	0.000	0.	0.	0.00	0.000
363		6.09	6.09	1144	64	3.78	1074.	0.	0.	0.000	0.	0.	0.00	0.000
364		6.09	6.09	1700	50	10.29	1212.	0.	0.	0.000	0.	0.	0.00	0.000
365		10.18	10.18	1406	8	7.74	442.	0.	0.	0.000	0.	0.	0.00	0.000
366		10.18	10.18	1167	-3	6.65	320.	0.	0.	0.000	0.	0.	0.00	0.000
367		6.09	6.09	1254	30	7.98	841.	0.	0.	0.000	0.	0.	0.00	0.000
368		6.09	6.09	972	23	6.23	645.	0.	0.	0.000	0.	0.	0.00	0.000
369		6.09	6.09	1017	52	4.03	915.	0.	0.	0.000	0.	0.	0.00	0.000
370		6.09	6.09	799	47	2.30	768.	0.	0.	0.000	0.	0.	0.00	0.000
371		6.09	6.09	662	56	0.00	781.	0.	0.	0.000	0.	0.	0.00	0.000
372		6.09	6.09	829	63	0.00	915.	0.	0.	0.000	0.	0.	0.00	0.000
373		6.09	6.09	952	62	1.34	971.	0.	0.	0.000	0.	0.	0.00	0.000
374		6.09	6.09	896	59	1.13	917.	0.	0.	0.000	0.	0.	0.00	0.000
375		6.09	6.09	996	58	2.88	957.	0.	0.	0.000	0.	0.	0.00	0.000
376		6.09	6.09	860	57	0.85	886.	0.	0.	0.000	0.	0.	0.00	0.000
377		6.09	6.09	833	61	0.00	902.	0.	0.	0.000	0.	0.	0.00	0.000
378		6.09	6.09	1144	64	3.79	1074.	0.	0.	0.000	0.	0.	0.00	0.000
379		6.09	6.09	1701	50	10.30	1212.	0.	0.	0.000	0.	0.	0.00	0.000
380		6.09	6.09	1005	64	1.80	1012.	0.	0.	0.000	0.	0.	0.00	0.000
381		6.09	6.09	1331	67	5.43	1188.	0.	0.	0.000	0.	0.	0.00	0.000
382		6.09	6.09	1797	49	11.12	1250.	0.	0.	0.000	0.	0.	0.00	0.000
383		6.09	6.09	1171	64	4.12	1085.	0.	0.	0.000	0.	0.	0.00	0.000
384		6.09	6.09	1584	68	7.79	1313.	0.	0.	0.000	0.	0.	0.00	0.000
385		6.09	6.09	2061	48	13.25	1364.	0.	0.	0.000	0.	0.	0.00	0.000
386		6.09	6.09	1351	60	6.45	1136.	0.	0.	0.000	0.	0.	0.00	0.000
387		6.09	6.09	1839	65	10.30	1406.	0.	0.	0.000	0.	0.	0.00	0.000
388		6.09	6.09	2491	43	16.75	1527.	0.	0.	0.000	0.	0.	0.00	0.000
389		6.09	6.09	1719	38	11.15	1122.	0.	0.	0.000	0.	0.	0.00	0.000
390		7.97	6.09	2338	43	13.82	1114.	0.	0.	0.000	0.	0.	0.00	0.000
391		7.97	6.09	3031	21	19.22	1231.	0.	0.	0.000	0.	0.	0.00	0.000
392		10.18	10.18	1998	14	10.92	640.	0.	0.	0.000	0.	0.	0.00	0.000
393		17.72	10.18	2848	18	12.64	526.	0.	0.	0.000	0.	0.	0.00	0.000
394		17.72	10.18	3849	0.	17.72	648.	0.	0.	0.000	0.	0.	0.00	0.000

MACROGUSCIO fond

COEF.							INFERIORE ORIZZONTALE							INFERIORE VERTICALE						
GUSCI	spess	Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF	
MAX %																				

175		40		5.65	5.65	0.	42.	0.00	0.19		5.65	5.65	63.	5.	0.00	0.04	
10																	
176		40		5.65	5.65	102.	22.	0.00	0.13		5.65	5.65	63.	5.	0.00	0.04	
7																	
177		40		5.65	5.65	0.	40.	0.00	0.17		5.65	5.65	164.	25.	0.00	0.15	
9																	
178		40		5.65	5.65	134.	17.	0.00	0.14		5.65	5.65	164.	25.	0.00	0.15	
8																	
179		40		5.65	5.65	0.	24.	0.00	0.11		5.65	5.65	417.	47.	0.00	0.31	
16																	
180		40		5.65	5.65	112.	14.	0.00	0.11		5.65	5.65	417.	47.	0.00	0.31	
16																	
181		40		5.65	5.65	0.	-19.	0.00	0.08		5.65	5.65	653.	68.	0.00	0.46	
23																	
182		40		5.65	5.65	74.	4.	0.00	0.04		5.65	5.65	653.	68.	0.00	0.46	
23																	
183		40		5.65	5.65	0.	22.	0.00	0.10		5.65	5.65	564.	69.	0.00	0.45	
22																	
184		40		5.65	5.65	0.	12.	0.00	0.05		5.65	5.65	564.	69.	0.00	0.45	
22																	
185		40		5.65	5.65	0.	43.	0.00	0.19		5.65	5.65	620.	140.	0.00	0.78	
39																	
186		40		5.65	5.65	0.	25.	0.00	0.11		5.65	5.65	620.	140.	0.00	0.78	
39																	
187		40		5.65	5.65	0.	42.	0.00	0.19		5.65	5.65	622.	140.	0.00	0.78	
39																	
188		40		5.65	5.65	0.	25.	0.00	0.11		5.65	5.65	622.	140.	0.00	0.78	
39																	
189		40		5.65	5.65	0.	21.	0.00	0.09		5.65	5.65	559.	69.	0.00	0.45	
22																	
190		40		5.65	5.65	0.	12.	0.00	0.05		5.65	5.65	559.	69.	0.00	0.45	
22																	
191		40		5.65	5.65	0.	-19.	0.00	0.08		5.65	5.65	644.	68.	0.00	0.46	
23																	
192		40		5.65	5.65	73.	4.	0.00	0.04		5.65	5.65	644.	68.	0.00	0.46	
23																	
193		40		5.65	5.65	0.	24.	0.00	0.11		5.65	5.65	412.	47.	0.00	0.31	
15																	
194		40		5.65	5.65	111.	14.	0.00	0.11		5.65	5.65	412.	47.	0.00	0.31	
15																	
195		40		5.65	5.65	0.	39.	0.00	0.17		5.65	5.65	162.	25.	0.00	0.15	
9																	
196		40		5.65	5.65	134.	17.	0.00	0.14		5.65	5.65	162.	25.	0.00	0.15	
8																	
197		40		5.65	5.65	0.	42.	0.00	0.19		5.65	5.65	64.	5.	0.00	0.04	
10																	
198		40		5.65	5.65	102.	22.	0.00	0.13		5.65	5.65	64.	5.	0.00	0.04	
7																	
269		40		5.65	5.65	0.	42.	0.00	0.19		5.65	5.65	64.	5.	0.00	0.04	
10																	
270		40		5.65	5.65	103.	22.	0.00	0.13		5.65	5.65	64.	5.	0.00	0.04	
7																	
271		40		5.65	5.65	0.	39.	0.00	0.17		5.65	5.65	164.	25.	0.00	0.15	
9																	
272		40		5.65	5.65	135.	17.	0.00	0.14		5.65	5.65	164.	25.	0.00	0.15	
8																	
273		40		5.65	5.65	0.	31.	0.00	0.14		5.65	5.65	416.	47.	0.00	0.31	
16																	
274		40		5.65	5.65	113.	14.	0.00	0.11		5.65	5.65	416.	47.	0.00	0.31	
16																	
275		40		5.65	5.65	0.	49.	0.00	0.22		5.65	5.65	648.	68.	0.00	0.46	
23																	
276		40		5.65	5.65	74.	4.	0.00	0.04		5.65	5.65	648.	68.	0.00	0.46	
23																	
277		40		5.65	5.65	0.	55.	0.00	0.24		5.65	5.65	559.	69.	0.00	0.45	
22																	
278		40		5.65	5.65	0.	12.	0.00	0.05		5.65	5.65	559.	69.	0.00	0.45	
22																	
279		40		5.65	5.65	0.	77.	0.00	0.34		5.65	5.65	629.	140.	0.00	0.78	
39																	
280		40		5.65	5.65	0.	25.	0.00	0.11		5.65	5.65	629.	140.	0.00	0.78	
39																	
281		40		5.65	5.65	0.	62.	0.00	0.27		5.65	5.65	625.	143.	0.00	0.79	
40																	
282		40		5.65	5.65	0.	26.	0.00	0.12		5.65	5.65	625.	143.	0.00	0.79	
40																	

283		40		5.65	5.65	0.	46.	0.00	0.20		5.65	5.65	557.	70.	0.00	0.45	
22																	
284		40		5.65	5.65	0.	13.	0.00	0.06		5.65	5.65	557.	70.	0.00	0.45	
22																	
285		40		5.65	5.65	0.	42.	0.00	0.19		5.65	5.65	651.	68.	0.00	0.46	
23																	
286		40		5.65	5.65	86.	6.	0.00	0.05		5.65	5.65	651.	68.	0.00	0.46	
23																	
287		40		5.65	5.65	0.	24.	0.00	0.11		5.65	5.65	419.	47.	0.00	0.31	
16																	
288		40		5.65	5.65	115.	14.	0.00	0.11		5.65	5.65	419.	47.	0.00	0.31	
16																	
289		40		5.65	5.65	0.	39.	0.00	0.17		5.65	5.65	166.	25.	0.00	0.15	
9																	
290		40		5.65	5.65	136.	17.	0.00	0.14		5.65	5.65	166.	25.	0.00	0.15	
8																	
291		40		5.65	5.65	0.	42.	0.00	0.19		5.65	5.65	64.	5.	0.00	0.04	
10																	
292		40		5.65	5.65	104.	22.	0.00	0.13		5.65	5.65	64.	5.	0.00	0.04	
7																	

COEF. GUSCI MAX %	spess	SUPERIORE ORIZZONTALE						SUPERIORE VERTICALE									
		Af	Afc	Mom	Nor	epsC	epsF	Af	Afc	Mom	Nor	epsC	epsF				
175		40		5.65	5.65	2154.	41.	0.00	0.73		5.65	5.65	174.	5.	0.00	0.07	
35																	
176		40		5.65	5.65	595.	30.	0.00	0.28		5.65	5.65	174.	5.	0.00	0.07	
14																	
177		40		5.65	5.65	2174.	33.	0.02	0.70		5.65	5.65	182.	23.	0.00	0.15	
34																	
178		40		5.65	5.65	669.	32.	0.00	0.31		5.65	5.65	182.	23.	0.00	0.15	
15																	
179		40		5.65	5.65	2349.	9.	0.11	0.64		5.65	5.65	148.	48.	0.00	0.25	
31																	
180		40		5.65	5.65	760.	26.	0.00	0.31		5.65	5.65	148.	48.	0.00	0.25	
15																	
181		40		5.65	5.65	3294.	4.	0.17	0.86		5.65	5.65	205.	68.	0.00	0.35	
42																	
182		40		5.65	5.65	943.	8.	0.03	0.28		5.65	5.65	205.	68.	0.00	0.35	
18																	
183		40		5.65	5.65	3690.	16.	0.17	1.01		5.65	5.65	79.	69.	0.00	0.33	
49																	
184		40		5.65	5.65	1033.	12.	0.03	0.32		5.65	5.65	79.	69.	0.00	0.33	
17																	
185		40		5.65	5.65	4220.	22.	0.19	1.17		5.65	5.65	728.	94.	0.00	0.67	
57																	
186		40		5.65	5.65	1137.	25.	0.00	0.40		5.65	5.65	728.	94.	0.00	0.67	
34																	
187		40		5.65	5.65	4231.	21.	0.19	1.17		5.65	5.65	722.	94.	0.00	0.67	
57																	
188		40		5.65	5.65	1139.	25.	0.00	0.40		5.65	5.65	722.	94.	0.00	0.67	
34																	
189		40		5.65	5.65	3698.	16.	0.17	1.01		5.65	5.65	80.	69.	0.00	0.33	
49																	
190		40		5.65	5.65	1034.	12.	0.03	0.32		5.65	5.65	80.	69.	0.00	0.33	
17																	
191		40		5.65	5.65	3300.	4.	0.17	0.86		5.65	5.65	207.	68.	0.00	0.35	
42																	
192		40		5.65	5.65	944.	8.	0.03	0.28		5.65	5.65	207.	68.	0.00	0.35	
18																	
193		40		5.65	5.65	2348.	9.	0.11	0.64		5.65	5.65	147.	48.	0.00	0.25	
31																	
194		40		5.65	5.65	760.	26.	0.00	0.31		5.65	5.65	147.	48.	0.00	0.25	
15																	
195		40		5.65	5.65	2173.	33.	0.02	0.70		5.65	5.65	182.	23.	0.00	0.15	
34																	
196		40		5.65	5.65	668.	32.	0.00	0.31		5.65	5.65	182.	23.	0.00	0.15	
15																	
197		40		5.65	5.65	2153.	40.	0.00	0.72		5.65	5.65	174.	5.	0.00	0.07	
35																	
198		40		5.65	5.65	595.	30.	0.00	0.28		5.65	5.65	174.	5.	0.00	0.07	
14																	
269		40		5.65	5.65	2151.	40.	0.00	0.72		5.65	5.65	174.	5.	0.00	0.07	
35																	
270		40		5.65	5.65	595.	30.	0.00	0.28		5.65	5.65	174.	5.	0.00	0.07	

14													
271	40	5.65	5.65	2172.	33.	0.02	0.70	5.65	5.65	182.	23.	0.00	0.15
34													
272	40	5.65	5.65	668.	32.	0.00	0.31	5.65	5.65	182.	23.	0.00	0.15
15													
273	40	5.65	5.65	2348.	26.	0.05	0.71	5.65	5.65	149.	48.	0.00	0.25
35													
274	40	5.65	5.65	761.	26.	0.00	0.31	5.65	5.65	149.	48.	0.00	0.25
15													
275	40	5.65	5.65	3306.	32.	0.10	0.98	5.65	5.65	214.	68.	0.00	0.35
48													
276	40	5.65	5.65	946.	8.	0.03	0.28	5.65	5.65	214.	68.	0.00	0.35
18													
277	40	5.65	5.65	3707.	53.	0.09	1.17	5.65	5.65	84.	69.	0.00	0.33
57													
278	40	5.65	5.65	1037.	12.	0.03	0.32	5.65	5.65	84.	69.	0.00	0.33
17													
279	40	5.65	5.65	4243.	77.	0.11	1.41	5.65	5.65	728.	95.	0.00	0.67
69													
280	40	5.65	5.65	1142.	25.	0.00	0.40	5.65	5.65	728.	95.	0.00	0.67
34													
281	40	5.65	5.65	4232.	30.	0.18	1.21	5.65	5.65	726.	98.	0.00	0.68
59													
282	40	5.65	5.65	1142.	26.	0.00	0.41	5.65	5.65	726.	98.	0.00	0.68
35													
283	40	5.65	5.65	3699.	24.	0.15	1.04	5.65	5.65	78.	70.	0.00	0.33
51													
284	40	5.65	5.65	1037.	13.	0.02	0.32	5.65	5.65	78.	70.	0.00	0.33
17													
285	40	5.65	5.65	3300.	11.	0.15	0.89	5.65	5.65	200.	68.	0.00	0.35
43													
286	40	5.65	5.65	947.	10.	0.01	0.28	5.65	5.65	200.	68.	0.00	0.35
18													
287	40	5.65	5.65	2348.	9.	0.10	0.64	5.65	5.65	150.	48.	0.00	0.25
31													
288	40	5.65	5.65	763.	26.	0.00	0.31	5.65	5.65	150.	48.	0.00	0.25
15													
289	40	5.65	5.65	2171.	33.	0.02	0.70	5.65	5.65	183.	23.	0.00	0.15
34													
290	40	5.65	5.65	670.	32.	0.00	0.31	5.65	5.65	183.	23.	0.00	0.15
15													
291	40	5.65	5.65	2150.	40.	0.00	0.72	5.65	5.65	174.	5.	0.00	0.07
35													
292	40	5.65	5.65	596.	30.	0.00	0.28	5.65	5.65	174.	5.	0.00	0.07
14													

L'ARMATURA È OVUNQUE > DELLA QUANTITÀ RICHIESTA: IL PUNTO 2.3 DELLE NTC È VERIFICATO (Rd > Ed)

VERIFICHE A FESSURAZIONE (EFFETTO MEMBRANA + PIASTRA)

CASI DI CARICO: ->

Nome	Descrizione
30	SLE1Rara Vento dom (RARA)
31	SLE2Rara Solo Vento (RARA)
32	SLE3Rara Acc dom (RARA)
33	SLE4Neve dom (RARA)
34	SLE5Soccorso POS.1 (RARA)

DATI:

copriferro inferiore (asse armatura): 3 cm
 copriferro superiore (asse armatura): 3 cm

Af = area effettiva tesa (cm2 al metro)
 Afc = area effettiva compressa (cm2 al metro)
 Mom = momento flettente [daNcm/cm]
 Nor = sforzo normale [daN]
 sigC = tensione calcestruzzo [daN/cm2]
 valore max per combinazione rara = 149.4 daN/cm2
 " " " " " " " " quasi permanente = 112 daN/cm2
 sigF = tensione acciaio [daN/cm2]
 valore max per combinazione rara = 3600 daN/cm2
 wkF = apertura caratteristica per combinazione frequente (mm) - valore max = 0.4 mm
 wkP = " " " " " " " " " quasi permanente (mm) - " " " " = 0.3 mm

DATI FRC (calcestruzzo fibrorinforzato, verifica secondo Linee Guida maggio 2022):
 fFtsk = tensione di progetto in esercizio = 0 daN/cm2

<-

ARMATURA INFERIORE ORIZZONTALE

GUSCI			COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE			
	Af	Afc	Mom	Nor	sigC	sigF	Mom	Nor	WkF	Mom	Nor	sigC	WkP
175	5.65	5.65	0.	27	0.00	236.	0.	0.	0.000	0.	0.	0.00	0.000
176	5.65	5.65	5	17	0.00	152.	0.	0.	0.000	0.	0.	0.00	0.000
177	5.65	5.65	0.	21	0.00	187.	0.	0.	0.000	0.	0.	0.00	0.000
178	5.65	5.65	21	16	0.00	155.	0.	0.	0.000	0.	0.	0.00	0.000
179	5.65	5.65	0.	1	0.00	9.	0.	0.	0.000	0.	0.	0.00	0.000
180	5.65	5.65	1	6	0.00	57.	0.	0.	0.000	0.	0.	0.00	0.000
181	5.65	5.65	0.	-11	0.26	-4.	0.	0.	0.000	0.	0.	0.00	0.000
182	5.65	5.65	0.	-3	0.07	-1.	0.	0.	0.000	0.	0.	0.00	0.000
183	5.65	5.65	0.	-5	0.11	-2.	0.	0.	0.000	0.	0.	0.00	0.000
184	5.65	5.65	0.	2	0.00	15.	0.	0.	0.000	0.	0.	0.00	0.000
185	5.65	5.65	0.	-2	0.05	-1.	0.	0.	0.000	0.	0.	0.00	0.000
186	5.65	5.65	0.	9	0.00	80.	0.	0.	0.000	0.	0.	0.00	0.000
187	5.65	5.65	0.	-2	0.04	-1.	0.	0.	0.000	0.	0.	0.00	0.000
188	5.65	5.65	0.	9	0.00	80.	0.	0.	0.000	0.	0.	0.00	0.000
189	5.65	5.65	0.	-4	0.11	-2.	0.	0.	0.000	0.	0.	0.00	0.000
190	5.65	5.65	0.	2	0.00	15.	0.	0.	0.000	0.	0.	0.00	0.000
191	5.65	5.65	0.	-11	0.26	-4.	0.	0.	0.000	0.	0.	0.00	0.000
192	5.65	5.65	0.	-3	0.06	-1.	0.	0.	0.000	0.	0.	0.00	0.000
193	5.65	5.65	0.	1	0.00	9.	0.	0.	0.000	0.	0.	0.00	0.000
194	5.65	5.65	0.	6	0.00	57.	0.	0.	0.000	0.	0.	0.00	0.000
195	5.65	5.65	0.	21	0.00	186.	0.	0.	0.000	0.	0.	0.00	0.000
196	5.65	5.65	20	16	0.00	155.	0.	0.	0.000	0.	0.	0.00	0.000
197	5.65	5.65	0.	27	0.00	236.	0.	0.	0.000	0.	0.	0.00	0.000
198	5.65	5.65	4	17	0.00	151.	0.	0.	0.000	0.	0.	0.00	0.000
269	5.65	5.65	0.	27	0.00	236.	0.	0.	0.000	0.	0.	0.00	0.000
270	5.65	5.65	5	17	0.00	152.	0.	0.	0.000	0.	0.	0.00	0.000
271	5.65	5.65	0.	21	0.00	186.	0.	0.	0.000	0.	0.	0.00	0.000
272	5.65	5.65	22	16	0.00	156.	0.	0.	0.000	0.	0.	0.00	0.000
273	5.65	5.65	0.	1	0.00	9.	0.	0.	0.000	0.	0.	0.00	0.000
274	5.65	5.65	2	6	0.00	58.	0.	0.	0.000	0.	0.	0.00	0.000
275	5.65	5.65	0.	-11	0.26	-4.	0.	0.	0.000	0.	0.	0.00	0.000
276	5.65	5.65	0.	-3	0.06	-1.	0.	0.	0.000	0.	0.	0.00	0.000
277	5.65	5.65	0.	-4	0.11	-2.	0.	0.	0.000	0.	0.	0.00	0.000
278	5.65	5.65	0.	2	0.00	15.	0.	0.	0.000	0.	0.	0.00	0.000
279	5.65	5.65	0.	-2	0.04	-1.	0.	0.	0.000	0.	0.	0.00	0.000
280	5.65	5.65	0.	9	0.00	80.	0.	0.	0.000	0.	0.	0.00	0.000
281	5.65	5.65	0.	-2	0.05	-1.	0.	0.	0.000	0.	0.	0.00	0.000
282	5.65	5.65	0.	9	0.00	80.	0.	0.	0.000	0.	0.	0.00	0.000
283	5.65	5.65	0.	-4	0.11	-2.	0.	0.	0.000	0.	0.	0.00	0.000
284	5.65	5.65	0.	2	0.00	15.	0.	0.	0.000	0.	0.	0.00	0.000
285	5.65	5.65	0.	-11	0.26	-4.	0.	0.	0.000	0.	0.	0.00	0.000
286	5.65	5.65	0.	-3	0.06	-1.	0.	0.	0.000	0.	0.	0.00	0.000
287	5.65	5.65	0.	1	0.00	9.	0.	0.	0.000	0.	0.	0.00	0.000
288	5.65	5.65	2	6	0.00	58.	0.	0.	0.000	0.	0.	0.00	0.000
289	5.65	5.65	0.	21	0.00	186.	0.	0.	0.000	0.	0.	0.00	0.000
290	5.65	5.65	22	16	0.00	156.	0.	0.	0.000	0.	0.	0.00	0.000
291	5.65	5.65	0.	27	0.00	236.	0.	0.	0.000	0.	0.	0.00	0.000
292	5.65	5.65	6	17	0.00	152.	0.	0.	0.000	0.	0.	0.00	0.000

ARMATURA INFERIORE VERTICALE

GUSCI			COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE			
	Af	Afc	Mom	Nor	sigC	sigF	Mom	Nor	WkF	Mom	Nor	sigC	WkP
175	5.65	5.65	15	2	0.00	22.	0.	0.	0.000	0.	0.	0.00	0.000
176	5.65	5.65	15	2	0.00	22.	0.	0.	0.000	0.	0.	0.00	0.000
177	5.65	5.65	84	14	0.00	163.	0.	0.	0.000	0.	0.	0.00	0.000
178	5.65	5.65	84	14	0.00	163.	0.	0.	0.000	0.	0.	0.00	0.000
179	5.65	5.65	216	24	0.00	325.	0.	0.	0.000	0.	0.	0.00	0.000
180	5.65	5.65	216	24	0.00	325.	0.	0.	0.000	0.	0.	0.00	0.000
181	5.65	5.65	391	29	0.00	458.	0.	0.	0.000	0.	0.	0.00	0.000
182	5.65	5.65	391	29	0.00	458.	0.	0.	0.000	0.	0.	0.00	0.000
183	5.65	5.65	503	2	3.75	273.	0.	0.	0.000	0.	0.	0.00	0.000
184	5.65	5.65	503	2	3.75	273.	0.	0.	0.000	0.	0.	0.00	0.000
185	5.65	5.65	323	51	0.00	619.	0.	0.	0.000	0.	0.	0.00	0.000
186	5.65	5.65	323	51	0.00	619.	0.	0.	0.000	0.	0.	0.00	0.000
187	5.65	5.65	321	51	0.00	621.	0.	0.	0.000	0.	0.	0.00	0.000
188	5.65	5.65	321	51	0.00	621.	0.	0.	0.000	0.	0.	0.00	0.000
189	5.65	5.65	504	2	3.76	273.	0.	0.	0.000	0.	0.	0.00	0.000
190	5.65	5.65	504	2	3.76	273.	0.	0.	0.000	0.	0.	0.00	0.000
191	5.65	5.65	393	29	0.00	458.	0.	0.	0.000	0.	0.	0.00	0.000
192	5.65	5.65	393	29	0.00	458.	0.	0.	0.000	0.	0.	0.00	0.000

193	5.65	5.65	217	24	0.00	326.	0.	0.	0.000	0.	0.	0.00	0.000
194	5.65	5.65	217	24	0.00	326.	0.	0.	0.000	0.	0.	0.00	0.000
195	5.65	5.65	84	14	0.00	163.	0.	0.	0.000	0.	0.	0.00	0.000
196	5.65	5.65	84	14	0.00	163.	0.	0.	0.000	0.	0.	0.00	0.000
197	5.65	5.65	16	2	0.00	22.	0.	0.	0.000	0.	0.	0.00	0.000
198	5.65	5.65	16	2	0.00	22.	0.	0.	0.000	0.	0.	0.00	0.000
269	5.65	5.65	16	2	0.00	22.	0.	0.	0.000	0.	0.	0.00	0.000
270	5.65	5.65	16	2	0.00	22.	0.	0.	0.000	0.	0.	0.00	0.000
271	5.65	5.65	86	14	0.00	164.	0.	0.	0.000	0.	0.	0.00	0.000
272	5.65	5.65	86	14	0.00	164.	0.	0.	0.000	0.	0.	0.00	0.000
273	5.65	5.65	220	24	0.00	328.	0.	0.	0.000	0.	0.	0.00	0.000
274	5.65	5.65	220	24	0.00	328.	0.	0.	0.000	0.	0.	0.00	0.000
275	5.65	5.65	396	29	0.00	460.	0.	0.	0.000	0.	0.	0.00	0.000
276	5.65	5.65	396	29	0.00	460.	0.	0.	0.000	0.	0.	0.00	0.000
277	5.65	5.65	507	2	3.78	274.	0.	0.	0.000	0.	0.	0.00	0.000
278	5.65	5.65	507	2	3.78	274.	0.	0.	0.000	0.	0.	0.00	0.000
279	5.65	5.65	323	51	0.00	621.	0.	0.	0.000	0.	0.	0.00	0.000
280	5.65	5.65	323	51	0.00	621.	0.	0.	0.000	0.	0.	0.00	0.000
281	5.65	5.65	326	51	0.00	623.	0.	0.	0.000	0.	0.	0.00	0.000
282	5.65	5.65	326	51	0.00	623.	0.	0.	0.000	0.	0.	0.00	0.000
283	5.65	5.65	510	2	3.80	275.	0.	0.	0.000	0.	0.	0.00	0.000
284	5.65	5.65	510	2	3.80	275.	0.	0.	0.000	0.	0.	0.00	0.000
285	5.65	5.65	398	29	0.00	460.	0.	0.	0.000	0.	0.	0.00	0.000
286	5.65	5.65	398	29	0.00	460.	0.	0.	0.000	0.	0.	0.00	0.000
287	5.65	5.65	220	24	0.00	327.	0.	0.	0.000	0.	0.	0.00	0.000
288	5.65	5.65	220	24	0.00	327.	0.	0.	0.000	0.	0.	0.00	0.000
289	5.65	5.65	86	14	0.00	164.	0.	0.	0.000	0.	0.	0.00	0.000
290	5.65	5.65	86	14	0.00	164.	0.	0.	0.000	0.	0.	0.00	0.000
291	5.65	5.65	16	2	0.00	22.	0.	0.	0.000	0.	0.	0.00	0.000
292	5.65	5.65	16	2	0.00	22.	0.	0.	0.000	0.	0.	0.00	0.000

ARMATURA SUPERIORE ORIZZONTALE

GUSCI	COMBINAZIONE RARA						COMB. FREQUENTE			COMB. QUASI PERMANENTE			
	Af	Afc	Mom	Nor	sigC	sigF	Mom	Nor	WkF	Mom	Nor	sigC	WkP
175	5.65	5.65	1344	27	9.21	919.	0.	0.	0.000	0.	0.	0.00	0.000
176	5.65	5.65	358	17	1.68	333.	0.	0.	0.000	0.	0.	0.00	0.000
177	5.65	5.65	1397	21	9.89	896.	0.	0.	0.000	0.	0.	0.00	0.000
178	5.65	5.65	403	16	2.17	351.	0.	0.	0.000	0.	0.	0.00	0.000
179	5.65	5.65	1523	1	11.46	786.	0.	0.	0.000	0.	0.	0.00	0.000
180	5.65	5.65	449	6	3.20	285.	0.	0.	0.000	0.	0.	0.00	0.000
181	5.65	5.65	1900	-11	14.48	878.	0.	0.	0.000	0.	0.	0.00	0.000
182	5.65	5.65	527	-3	4.01	245.	0.	0.	0.000	0.	0.	0.00	0.000
183	5.65	5.65	2144	-5	16.24	1055.	0.	0.	0.000	0.	0.	0.00	0.000
184	5.65	5.65	574	2	4.29	308.	0.	0.	0.000	0.	0.	0.00	0.000
185	5.65	5.65	2397	-2	18.11	1205.	0.	0.	0.000	0.	0.	0.00	0.000
186	5.65	5.65	608	9	4.31	389.	0.	0.	0.000	0.	0.	0.00	0.000
187	5.65	5.65	2397	-2	18.10	1207.	0.	0.	0.000	0.	0.	0.00	0.000
188	5.65	5.65	609	9	4.32	390.	0.	0.	0.000	0.	0.	0.00	0.000
189	5.65	5.65	2143	-4	16.23	1056.	0.	0.	0.000	0.	0.	0.00	0.000
190	5.65	5.65	575	2	4.30	308.	0.	0.	0.000	0.	0.	0.00	0.000
191	5.65	5.65	1899	-11	14.48	878.	0.	0.	0.000	0.	0.	0.00	0.000
192	5.65	5.65	527	-3	4.01	246.	0.	0.	0.000	0.	0.	0.00	0.000
193	5.65	5.65	1523	1	11.47	786.	0.	0.	0.000	0.	0.	0.00	0.000
194	5.65	5.65	450	6	3.20	285.	0.	0.	0.000	0.	0.	0.00	0.000
195	5.65	5.65	1397	21	9.89	896.	0.	0.	0.000	0.	0.	0.00	0.000
196	5.65	5.65	403	16	2.17	351.	0.	0.	0.000	0.	0.	0.00	0.000
197	5.65	5.65	1343	27	9.21	918.	0.	0.	0.000	0.	0.	0.00	0.000
198	5.65	5.65	358	17	1.68	333.	0.	0.	0.000	0.	0.	0.00	0.000
269	5.65	5.65	1342	27	9.20	918.	0.	0.	0.000	0.	0.	0.00	0.000
270	5.65	5.65	358	17	1.68	333.	0.	0.	0.000	0.	0.	0.00	0.000
271	5.65	5.65	1396	21	9.88	896.	0.	0.	0.000	0.	0.	0.00	0.000
272	5.65	5.65	403	16	2.17	351.	0.	0.	0.000	0.	0.	0.00	0.000
273	5.65	5.65	1524	1	11.47	786.	0.	0.	0.000	0.	0.	0.00	0.000
274	5.65	5.65	450	6	3.20	286.	0.	0.	0.000	0.	0.	0.00	0.000
275	5.65	5.65	1902	-11	14.49	879.	0.	0.	0.000	0.	0.	0.00	0.000
276	5.65	5.65	528	-3	4.02	246.	0.	0.	0.000	0.	0.	0.00	0.000
277	5.65	5.65	2147	-4	16.26	1057.	0.	0.	0.000	0.	0.	0.00	0.000
278	5.65	5.65	576	2	4.31	309.	0.	0.	0.000	0.	0.	0.00	0.000
279	5.65	5.65	2401	-2	18.13	1209.	0.	0.	0.000	0.	0.	0.00	0.000
280	5.65	5.65	612	9	4.34	391.	0.	0.	0.000	0.	0.	0.00	0.000
281	5.65	5.65	2403	-2	18.15	1209.	0.	0.	0.000	0.	0.	0.00	0.000
282	5.65	5.65	613	9	4.35	391.	0.	0.	0.000	0.	0.	0.00	0.000
283	5.65	5.65	2148	-4	16.27	1058.	0.	0.	0.000	0.	0.	0.00	0.000
284	5.65	5.65	577	2	4.31	309.	0.	0.	0.000	0.	0.	0.00	0.000
285	5.65	5.65	1903	-11	14.50	879.	0.	0.	0.000	0.	0.	0.00	0.000

286		5.65	5.65	529	-3	4.03	247.	0.	0.	0.000	0.	0.	0.00	0.000
287		5.65	5.65	1524	1	11.47	786.	0.	0.	0.000	0.	0.	0.00	0.000
288		5.65	5.65	451	6	3.21	286.	0.	0.	0.000	0.	0.	0.00	0.000
289		5.65	5.65	1396	21	9.88	895.	0.	0.	0.000	0.	0.	0.00	0.000
290		5.65	5.65	404	16	2.18	351.	0.	0.	0.000	0.	0.	0.00	0.000
291		5.65	5.65	1342	27	9.20	918.	0.	0.	0.000	0.	0.	0.00	0.000
292		5.65	5.65	359	17	1.68	333.	0.	0.	0.000	0.	0.	0.00	0.000

ARMATURA SUPERIORE VERTICALE

GUSCI				COMBINAZIONE RARA				COMB. FREQUENTE			COMB. QUASI PERMANENTE			
	Af	Afc		Mom	Nor	sigC	sigF	Mom	Nor	WkF	Mom	Nor	sigC	WkP
175		5.65	5.65	137	2	0.99	83.	0.	0.	0.000	0.	0.	0.00	0.000
176		5.65	5.65	137	2	0.99	83.	0.	0.	0.000	0.	0.	0.00	0.000
177		5.65	5.65	149	14	0.00	197.	0.	0.	0.000	0.	0.	0.00	0.000
178		5.65	5.65	149	14	0.00	197.	0.	0.	0.000	0.	0.	0.00	0.000
179		5.65	5.65	173	24	0.00	303.	0.	0.	0.000	0.	0.	0.00	0.000
180		5.65	5.65	173	24	0.00	303.	0.	0.	0.000	0.	0.	0.00	0.000
181		5.65	5.65	215	29	0.00	366.	0.	0.	0.000	0.	0.	0.00	0.000
182		5.65	5.65	215	29	0.00	366.	0.	0.	0.000	0.	0.	0.00	0.000
183		5.65	5.65	310	2	2.29	174.	0.	0.	0.000	0.	0.	0.00	0.000
184		5.65	5.65	310	2	2.29	174.	0.	0.	0.000	0.	0.	0.00	0.000
185		5.65	5.65	611	51	0.00	769.	0.	0.	0.000	0.	0.	0.00	0.000
186		5.65	5.65	611	51	0.00	769.	0.	0.	0.000	0.	0.	0.00	0.000
187		5.65	5.65	616	51	0.00	774.	0.	0.	0.000	0.	0.	0.00	0.000
188		5.65	5.65	616	51	0.00	774.	0.	0.	0.000	0.	0.	0.00	0.000
189		5.65	5.65	311	2	2.30	174.	0.	0.	0.000	0.	0.	0.00	0.000
190		5.65	5.65	311	2	2.30	174.	0.	0.	0.000	0.	0.	0.00	0.000
191		5.65	5.65	216	29	0.00	366.	0.	0.	0.000	0.	0.	0.00	0.000
192		5.65	5.65	216	29	0.00	366.	0.	0.	0.000	0.	0.	0.00	0.000
193		5.65	5.65	173	24	0.00	302.	0.	0.	0.000	0.	0.	0.00	0.000
194		5.65	5.65	173	24	0.00	302.	0.	0.	0.000	0.	0.	0.00	0.000
195		5.65	5.65	149	14	0.00	197.	0.	0.	0.000	0.	0.	0.00	0.000
196		5.65	5.65	149	14	0.00	197.	0.	0.	0.000	0.	0.	0.00	0.000
197		5.65	5.65	137	2	0.99	83.	0.	0.	0.000	0.	0.	0.00	0.000
198		5.65	5.65	137	2	0.99	83.	0.	0.	0.000	0.	0.	0.00	0.000
269		5.65	5.65	137	2	0.99	83.	0.	0.	0.000	0.	0.	0.00	0.000
270		5.65	5.65	137	2	0.99	83.	0.	0.	0.000	0.	0.	0.00	0.000
271		5.65	5.65	149	14	0.00	197.	0.	0.	0.000	0.	0.	0.00	0.000
272		5.65	5.65	149	14	0.00	197.	0.	0.	0.000	0.	0.	0.00	0.000
273		5.65	5.65	173	24	0.00	303.	0.	0.	0.000	0.	0.	0.00	0.000
274		5.65	5.65	173	24	0.00	303.	0.	0.	0.000	0.	0.	0.00	0.000
275		5.65	5.65	218	29	0.00	367.	0.	0.	0.000	0.	0.	0.00	0.000
276		5.65	5.65	218	29	0.00	367.	0.	0.	0.000	0.	0.	0.00	0.000
277		5.65	5.65	312	2	2.31	175.	0.	0.	0.000	0.	0.	0.00	0.000
278		5.65	5.65	312	2	2.31	175.	0.	0.	0.000	0.	0.	0.00	0.000
279		5.65	5.65	617	51	0.00	774.	0.	0.	0.000	0.	0.	0.00	0.000
280		5.65	5.65	617	51	0.00	774.	0.	0.	0.000	0.	0.	0.00	0.000
281		5.65	5.65	625	51	0.00	778.	0.	0.	0.000	0.	0.	0.00	0.000
282		5.65	5.65	625	51	0.00	778.	0.	0.	0.000	0.	0.	0.00	0.000
283		5.65	5.65	315	2	2.33	176.	0.	0.	0.000	0.	0.	0.00	0.000
284		5.65	5.65	315	2	2.33	176.	0.	0.	0.000	0.	0.	0.00	0.000
285		5.65	5.65	218	29	0.00	367.	0.	0.	0.000	0.	0.	0.00	0.000
286		5.65	5.65	218	29	0.00	367.	0.	0.	0.000	0.	0.	0.00	0.000
287		5.65	5.65	173	24	0.00	303.	0.	0.	0.000	0.	0.	0.00	0.000
288		5.65	5.65	173	24	0.00	303.	0.	0.	0.000	0.	0.	0.00	0.000
289		5.65	5.65	149	14	0.00	197.	0.	0.	0.000	0.	0.	0.00	0.000
290		5.65	5.65	149	14	0.00	197.	0.	0.	0.000	0.	0.	0.00	0.000
291		5.65	5.65	137	2	0.99	83.	0.	0.	0.000	0.	0.	0.00	0.000
292		5.65	5.65	137	2	0.99	83.	0.	0.	0.000	0.	0.	0.00	0.000

CALCOLO SBALZO IN C.A. – ORECCHIETTA 45x20

Il calcolo in esame si riferisce ad uno sbalzo incastrato ad un cordolo o trave di bordo in c.a.
Il momento max nella sezione di incastro del risulta dato dalla seguente espressione:

$M_{max} = q l^2 / 2$

CARATTERISTICHE GEOMETRICHE		
Luce di Calcolo	mt.	0.45
Spessore estremità	mt.	0.2
Spessore all'incastro	mt.	0.2
CARICHI AGENTI		
Carico Permanente	daN/m	500
Coeff. Parzializzazione	γ_g	1.3
Carico accidentale	daN/m	14000
Coeff. Parzializzazione	γ_q	1.5
Coeff. Di utilizzo	Φ_0	0.7
$Q_{tot} = Q_p * \gamma_g + Q_a * \gamma_q + Q_{ki} * \Phi_{02} * \gamma_{q2}$		
TOTALE		
Incremento sismico	daN/mq	20900
	daN/mq	8360.
MATERIALI IMPIEGATI		
Acciaio in barre tipo		B450C
Calcestruzzo		C25/30
Armatura superiore della sezione	cmq	5.65
Armatura inferiore della sezione	cmq	2.26
RISULTATI PER VERIFICHE		
Reazione vincolare	daN	13167.
Momento Massimo incastro	daNm	2963.
Taglio massimo	daN	13167.
Base sezione verifica	cm.	100.
Altezza sezione verifica	cm.	20.

COEFFICIENTI DI CALCOLO

Rapporto Armatura Compresa/Armatura Tesa $u = A_a' / A_a = .4$

% meccanica armatura $\omega = A_a / (b * h) * f_{yd} / \alpha_{fcd} = .091$

$\omega_1 = \xi_1 * \beta / (s - s' * u) = .119$

$\omega_2 = \xi_2 * \beta / (s - s' * u) = .32$

$\omega_3 = \xi_3 * \beta / (s - s' * u) = .93$

C A S I S T I C A

$\omega < \omega_1$	Campo 2a
$\omega_1 < \omega < \omega_2$	Campo 2b
$\omega_2 < \omega < \omega_3$	Campo 3
$\omega > \omega_3$	Campo 4

RISULTATI DELLA VERIFICA						
ξ	ϵ_c	η_0	β	s'	$\omega(1-s'*u) - \xi \beta$	k
.147	.00172	.86132	.614	.02636	.0001	.3645

Posizione asse neutro $x = \text{cm.}$

2.5716

Braccio coppia interna $\zeta = \text{cm.}$

.9455

$M_{rd} = A_a * \zeta * d * f_{yd} / 1000 = \text{daNm } 3496.7 > M_{max}$

VERIFICA A TAGLIO

$V_{rd} = \{0.18 * k * (100 * \rho_1 * f_{ck})^{1/3} / \gamma_c + 0.15 * \sigma_{cp}\} * b_w * d \geq (v_{min} + 0.15 * \sigma_{cp}) * b_w * d$

con

$k = 1 + (200/d)^{1/2} \leq 2$

$v_{min} = 0.035 k^{3/2} f_{ck}^{1/2}$

e dove

d è l'altezza utile della sezione (in mm);

$\rho_1 = A_{s1} / (b_w * d)$ è il rapporto geometrico di armatura longitudinale ($\leq 0,02$);

$\sigma_{cp} = N_{Ed} / A_c$ è la tensione media di compressione nella sezione ($\leq 0,2 f_{cd}$);

b_w è la larghezza minima della sezione (in mm).

RISULTATI

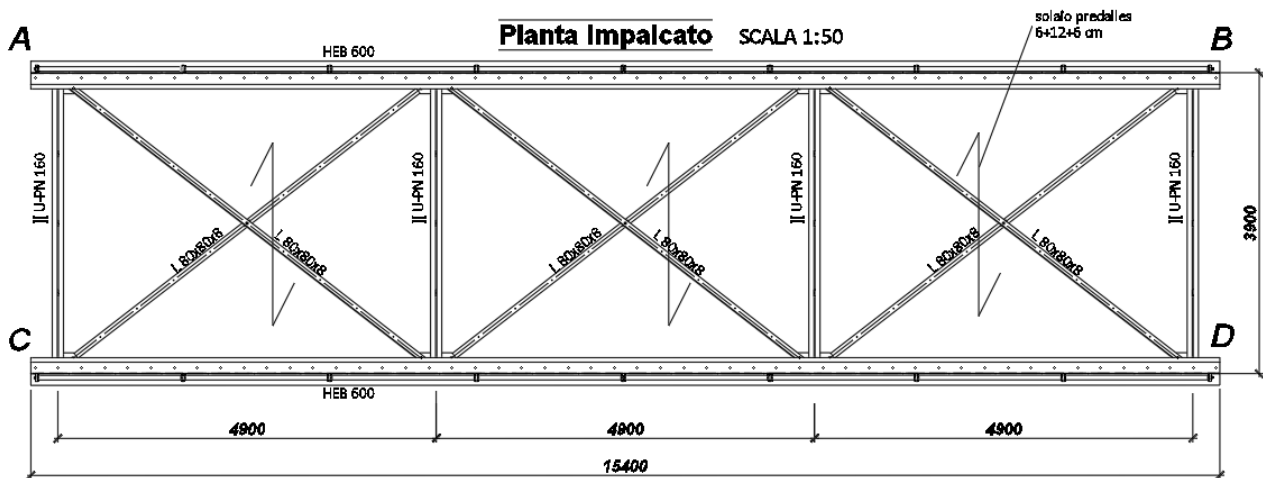
$T_{max} = \text{daN } 13167.$

$(v_{min} + 0,15 * \sigma_{cp}) * b_w * d = \text{daN } 8466.25$

$V_{rd} = \{0.18 * k * (100 * \rho_1 * f_{ck})^{1/3} / \gamma_c + 0,15 * \sigma_{cp}\} * b_w * d = \text{daN } 10906. \geq (v_{min} + 0,15 * \sigma_{cp}) * b_w * d$

Tmax < Tultimo SEZIONE VERIFICATA

Calcolo Solaio Predalles



Solaio a Lastre in C.A.N. - Metodo di Calcolo: D.M. 17/01/2018 - Stati Limite Gruppo A

Solaio tipo 1 - Solaio a Lastre in C.A.N. - Altezza totale Solaio = 24.0 cm - Interasse = 120.0 cm
LASTRE AUTOPORTANTI Altezza Solaio: 6.0 + 12.0 + 6.0 = 24.0 cm Interasse Solaio: 120.0 cm
Peso proprio Solaio: 375 daN/mq Peso Manufatto: 180 daN/mq Rompitratta: 0.00 / 0.00 m Interasse Nervature: 60.0 cm
Nervature: Numero tot.: 3 Numero laterali: 2 Larghezza lat.: 12.00 cm Numero centrali: 1 Larghezza centr.: 12.00
Spessore Lastra: 6.0 cm Altezza Nervature: 12.0 cm Larghezza totale Nervature: 36.0 cm Spessore Cappa: 6.0
Spessore Soletta collaborante: 6.0 cm Larghezza Nervature collaboranti: 36.0 cm Coefficiente Omogeneizzazione N: 15
Interposto Polistirolo: Numero: 2 Larghezza: 42.0 cm Altezza: 12.0 cm Taglio: 100 cm Peso: 0.00 daN
Tralicci: Numero T.N.L.: 1 Numero T.N.C.: 1 Tipo: 2 fi 5.0 Inf. + 1 fi 7.0 Sup. + St. fi 5.0 / 20.0 cm - 12.5 cm
Armatura diffusa nella Lastra: 1 fi 5.0 / 19.0 cm parallela ai Tralicci - 1 fi 5.0 / 25.0 cm ortogonale ai Tralicci
Armatura Ripartizione Cappa: RETE FI 6 - MAGLIA 20X20 Le Sollecitazioni e le Verifiche sono riferite all'Interasse
Copriferri Armature: Tral.: 2.0 cm Diff.: 2.0 cm Rip.: 3.0 cm Camp.: 2.0 cm Sup. App.: 2.0 cm Inf. App.: 4.5 cm
Armature considerate in Verifica: Tralicci: 1.18 cmq Armatura diffusa: 1.24 cmq Armatura di Rip.ne: 0.00 cmq
Calcestruzzo Manufatto: Rck: 300 daN/cm ² Fck: 249 daN/cm ² acc: 0.85 γc: 1.5 Fcd: 141.10 daN/cm ² Ec: 314472 daN/cm ²
Calcestruzzo Manufatto: σcr: 149.40 daN/cm ² σcqp: 112.05 daN/cm ² Riduzione Fcd/σcr/σcqp spessori < 5cm: -20%/ -20%/ -20%
Calcestruzzo Getto in Opera: Rck: 300 daN/cm ² Fck: 249 daN/cm ² acc: 0.85 γc: 1.5 Fcd: 141.10 daN/cm ² Ec: 314472 daN/cm ²
Calcestruzzo Getto in Opera: σcr: 149.40 daN/cm ² σcqp: 112.05 daN/cm ² Riduzione Fcd/σcr/σcqp spessori < 5cm: -20%/ -20%/ -20%
Acciaio: γs: 1.15 σs: 0.8*Fyk Campate Fyk: 4500 daN/cm ² Appoggi Fyk: 4500 daN/cm ² Traliccio Fyk: 4500 daN/cm ²
Acciaio: Campate Fyd: 3913 daN/cm ² Campate σs: 3600 daN/cm ² Appoggi Fyd: 3913 daN/cm ² Appoggi σs: 3600 daN/cm ²
Acciaio: Traliccio Fyd/ σs inf.: 3913/3600 daN/cm ² Fyd/ σs sup.: 1881/1731 daN/cm ² Fyd/ σs St. 1763/1622 daN/cm ²
Condizioni ambientali: Ordinarie Classe di esposizione: XC1 Fessurazione: W _r /W _f /W _p : ***/0.40/0.30 mm
Coefficienti Incremento Carichi: GammaG1: 1.00-1.30 GammaG2: 0.80-1.50 GammaQ: 0.00-1.50 Psi0: 0.70 Psi1: 0.50 Psi2: 0.30
Autoportanza - Nervature gettate: Larghezza: 12.0 cm Altezza: 12.0 cm - Carico acc.: 100 daN/mq
Autoportanza - Soletta gettata: Larghezza: 0.0 cm Altezza: 0.0 cm - Carico acc.: 120 daN/m
Vincoli App. estremi: 0: App. semplice 1: Incastro Altro: Semincastro
SN55FE360-CLASTREFBM1APPFBM1APPFBM1LASTRAFBM1
Caratt. Staffe: Posizione: Per Tral/Trav (3 St./Interasse) Tipologia: Tipo 2-S-2BV - 2 Bracci verticali Area Staffe: A _{sw} = Area(Φ Staffe)*2*3
Le Freccie del Solaio (Vedi Tabella 'Sollecitazioni/Verifiche Campate: Stato Limite di Esercizio-Combinazione Rara'), sono calcolate:
La Freccia istantanea (a tempo breve): Per combinazione rara - La Freccia differita (a tempo infinito): Per combinazione quasi permanente

Schema 1 - CAMPATA A

Carichi distribuiti: Stato Limite di Esercizio - Combinazione Rara (SLE-CR)

Camp.	Sigla	Luce calcolo cm	Luce netta cm	Zona piena Sx Or./Nec. cm	Zona piena Dx Or./Nec. cm	Tipo Solaio	Allin. Estrad.	Peso proprio daN/mq	Carico perm. daN/mq	Carico perm. non strutturale daN/mq	Carico variabile daN/mq	Carico totale daN/mq
1	A	420	390	15/35	15/35	1	Si	375	0	370	500	1245

Carichi distribuiti: Stato Limite di Esercizio - Combinazione Frequente (SLE-CF)

Camp.	Sigla	Luce calcolo cm	Luce netta cm	Zona piena Sx Or./Nec. cm	Zona piena Dx Or./Nec. cm	Tipo Solaio	Allin. Estrad.	Peso proprio daN/mq	Carico perm. daN/mq	Carico perm. non strutturale daN/mq	Carico variabile daN/mq	Carico totale daN/mq
1	A	420	390	15/35	15/35	1	Si	375	0	370	250	995

Carichi distribuiti: Stato Limite di Esercizio - Combinazione Quasi Permanente (SLE-CQP)

Camp.	Sigla	Luce calcolo cm	Luce netta cm	Zona piena Sx Or./Nec. cm	Zona piena Dx Or./Nec. cm	Tipo Solaio	Allin. Estrad.	Peso proprio daN/mq	Carico perm. daN/mq	Carico perm. non strutturale daN/mq	Carico variabile daN/mq	Carico totale daN/mq
1	A	420	390	15/35	15/35	1	Si	375	0	370	150	895

Carichi distribuiti: Stato Limite Ultimo (SLU)

Camp.	Sigla	Luce calcolo cm	Luce netta cm	Zona piena Sx Or./Nec. cm	Zona piena Dx Or./Nec. cm	Tipo Solaio	Allin. Estrad.	Peso proprio daN/mq	Carico perm. daN/mq	Carico perm. non strutturale daN/mq	Carico variabile daN/mq	Carico totale daN/mq
1	A	420	390	15/35	15/35	1	Si	487	0	555	750	1793

Distinta Armature Appoggi / Singolo Traliccio

Appoggio	Num. 1	Diam. 1 mm	Lun. 1 cm	Num. 2	Diam. 2 mm	Lun. 2 cm	Num. 3	Diam. 3 mm	Lun. 3 cm
1 sup.	2	10	120	0	0	0	0	0	0
2 sup.	2	10	120	0	0	0	0	0	0

Distinta Armature Inferiori Campate

Campata	Trallicci	Num. 1	Diam. 1 mm	Lun. 1 cm	Num. 2	Diam. 2 mm	Lun. 2 cm	Num. 3	Diam. 3 mm	Lun. 3 cm	N./Φ/Passo Staffe N./mm/cm	Tratto Staffe Iniz./Fine/Lungh. cm
1-A	Lat.	2	10	440	0	0	0	0	0	0	Sx - ***	Sx - ***
	Centr.	2	10	440	0	0	0	0	0	0	Dx - ***	Dx - ***

Sollecitazioni / Verifiche Appoggi: Stato Limite di Esercizio - Combinazione Rara (SLE-CR)

Appoggio	Coefficiente Riduzione Momenti	Coefficiente Momento Fittizio	Momento Flettente daN*cm	Momento Fittizio daN*cm	Reazione Vincolare daN	Lato Appoggio	Area Tesa cmq	Asse Neutro cm	Compr. Cls daN/cm ²	Trazione Acciaio daN/cm ²
1	1.00	14.00	-44100 (-44100)	-131544 (-131544)	3070 (2192)	Sx	0.00	0.00	0	0
						Dx	4.71	4.27	22	1361
2	1.00	14.00	-44100 (-44100)	-131544 (-131544)	3070 (2192)	Sx	4.71	4.27	22	1361
						Dx	0.00	0.00	0	0

Sollecitazioni / Verifiche Appoggi: Stato Limite di Esercizio - Combinazione Frequente (SLE-CF)

Appoggio	Coefficiente Riduzione Momenti	Coefficiente Momento Fittizio	Momento Flettente daN*cm	Momento Fittizio daN*cm	Reazione Vincolare daN	Lato Appoggio	Area Tesa cmq	Asse Neutro cm	Compr. Cls daN/cm ²	Trazione Acciaio daN/cm ²
1	1.00	14.00	-22050 (-22050)	-93744 (-93744)	2440 (1562)	Sx	0	0.00	0.00	0.00
						Dx	4.71	4.27	16	970
2	1.00	14.00	-22050 (-22050)	-93744 (-93744)	2440 (1562)	Sx	4.71	4.27	16	970
						Dx	0	0.00	0.00	0.00

Sollecitazioni / Verifiche Appoggi: Stato Limite di Esercizio - Combinazione Quasi Permanente (SLE-CQP)

Appoggio	Coefficiente Riduzione Momenti	Coefficiente Momento Fittizio	Momento Flettente daN*cm	Momento Fittizio daN*cm	Reazione Vincolare daN	Lato Appoggio	Area Tesa cmq	Asse Neutro cm	Compr. Cls daN/cm ²	Trazione Acciaio daN/cm ²
1	1.00	14.00	-13230 (-13230)	-78624 (-78624)	2188 (1310)	Sx	0	0.00	0.00	0.00
						Dx	4.71	4.27	13	814
2	1.00	14.00	-13230 (-13230)	-78624 (-78624)	2188 (1310)	Sx	4.71	4.27	13	814
						Dx	0	0.00	0.00	0.00

Sollecitazioni / Verifiche Appoggi: Stato Limite Ultimo (SLU)											
Appoggio	Coefficiente Riduzione Momenti	Coefficiente Momento Fittizio	Momento Flettente (MEd1) daN*cm	Momento Fittizio (MEd2) daN*cm	Reazione Vincolare daN	Lato Appoggio	Momento Ultimo (MRd) daN*cm	Area Tesa cmq	Asse Neutro cm	Deform. Max Cls %	Deform. Max Acc. %
1	1.00	14.00	-66150 (-66150)	-197316 (-197316)	4429 (3289)	Sx	0	0.00	0.00	0.00	0.00
						Dx	-400580	4.71	1.71	0.35	4.17
2	1.00	14.00	-66150 (-66150)	-197316 (-197316)	4429 (3289)	Sx	-400580	4.71	1.71	0.35	4.17
						Dx	0	0.00	0.00	0.00	0.00

Sollecitazioni / Verifiche Autoportanza Campate: Stato Limite di Esercizio - Condizione Residua (SLE-CR)								
Campata	Mom. Flett.Res. daN*cm	Compr. Res. Cls daN/cm	Traz. Res. Acc. daN/cm	Taglio Residuo daN	Tens. Tang. Max Res. daN/cm	Traz. Compr. Inf./Sup./Staf. daN/cm	Freccia Elast. Res. mm	Arm. Compr. Camp./Men. cm
1-A	85556	99	950	878	5	950/0/0	0.48	0.00

Sollecitazioni / Verifiche Autoportanza Campate: Stato Limite Ultimo (SLU)								
Campata	Mom. Flett.Res. daN*cm	Mom. Ultimo daN*cm	Def. Max Cls %	Def. Max Acc. %	Taglio Residuo daN	Taglio Ultimo daN	Traz. Compr. Inf./Sup./Staf. daN/cm	Arm. Compr. Camp./Men. cm
1-A	111223	205810	0.3	0.1	1141	4334	0/0/0	0.00

Sollecitazioni / Verifiche Campate: Stato Limite di Esercizio - Combinazione Rara (SLE-CR)											
Campata	Coeff. Mom. Fitt.	Mom. Flettente daN*cm	Mom. Fittizio daN*cm	X Mom. Max cm	Taglio Sx daN	Taglio Dx daN	Area Tesa cmq	Asse Neutro cm	Compr. Cls daN/cm	Traz. Acciaio daN/cm	Freccia Ist./Dif.(Dif.Dep.)/Contr. mm
1-A	8.00	271658 (186102)	315758 (230202)	210	3070 (2192)	-3070 (-2192)	7.13	5.43	35	2549	1.0/1.8(1.3)/0.0

Sollecitazioni / Verifiche Campate: Stato Limite di Esercizio - Combinazione Frequente (SLE-CF)											
Campata	Coeff. Mom. Fitt.	Mom. Flettente daN*cm	Mom. Fittizio daN*cm	X Mom. Max cm	Taglio Sx daN	Taglio Dx daN	Area Tesa cmq	Asse Neutro cm	Compr. Cls daN/cm	Traz. Acciaio daN/cm	
1-A	8.00	227558 (142002)	249608 (164052)	210	2440 (1562)	-2440 (-1562)	7.13	5.43	25	2090	

Sollecitazioni / Verifiche Campate: Stato Limite di Esercizio - Combinazione Quasi Permanente (SLE-CQP)											
Campata	Coeff. Mom. Fitt.	Mom. Flettente daN*cm	Mom. Fittizio daN*cm	X Mom. Max cm	Taglio Sx daN	Taglio Dx daN	Area Tesa cmq	Asse Neutro cm	Compr. Cls daN/cm	Traz. Acciaio daN/cm	
1-A	8.00	209918 (124362)	223148 (137592)	210	2188 (1310)	-2188 (-1310)	7.13	5.43	21	1906	

Sollecitazioni / Verifiche Campate: Stato Limite Ultimo (SLU)												
Campata	Coeff. Mom. Fitt.	Mom. Flettente (MEd1) daN*cm	Mom. Fittizio (MEd2) daN*cm	X Mom. Max cm	Taglio Sx daN	Taglio Dx daN	Mom. Ultimo (MRd) daN*cm	Area Tesa cmq	Asse Neutro cm	Def. Max Cls %	Def. Max Acc. %	Fessure Rara/Freq./QPerm. mm
1-A	8.00	390376 (279153)	456526 (345303)	210	4429 (3289)	-4429 (-3289)	591640	7.13	1.97	0.35	3.55	***/0.070/0.061

Sollecitazioni / Verifiche Limite Zone Piene: Stato Limite di Esercizio - Combinazione Rara (SLE-CR)											
Campata	Zona piena	Lar. Sottom. Interposto cm	Mom. Flettente daN*cm	Area Tesa cmq	Asse Neutro cm	Compr. Cls daN/cm	Traz. Acciaio daN/cm	Taglio daN	Tau daN/cm	Arm. Taglio Res. minima cmq	
1-A	Sx	21	56057 (29915)	7.13	5.14	4	207	2558 (1827)	7.12	0.85	
	Dx	21	56057 (29914)	7.13	5.14	4	207	-2558 (-1827)	7.12	0.85	

Sollecitazioni / Verifiche Limite Zone Piene: Stato Limite di Esercizio - Combinazione Frequente (SLE-CF)											
Campata	Zona piena	Lar. Sottom. Interposto cm	Mom. Flettente daN*cm	Area Tesa cmq	Asse Neutro cm	Compr. Cls daN/cm	Traz. Acciaio daN/cm	Taglio daN	Tau daN/cm	Arm. Taglio Res. minima cmq	
1-A	Sx	21	56057 (29915)	7.13	5.14	4	207	2033 (1302)	6.38	0.68	
	Dx	21	56057 (29914)	7.13	5.14	4	207	-2033 (-1302)	6.38	0.68	

Sollecitazioni / Verifiche Limite Zone Piene: Stato Limite di Esercizio - Combinazione Quasi Permanente (SLE-CQP)

Campata	Zona piena	Lar. Sottom. Interposto cm	Mom. Flettente daN*cm	Area Tesa cmq	Asse Neutro cm	Compr. Cls daN/cm ²	Traz. Acciaio daN/cm ²	Taglio daN	Tau daN/cm ²	Arm. Taglio Res. minima cmq
1-A	Sx	21	56057 (29915)	7.13	5.14	4	207	1823 (1092)	6.09	0.61
	Dx	21	56057 (29914)	7.13	5.14	4	207	-1823 (-1092)	6.09	0.61

Sollecitazioni / Verifiche Limite Zone Piene: Stato Limite Ultimo (SLU)

Campata	Zona piena	Mom. Flettente (MEd) daN*cm	Mom. Ultimo (MRd) daN*cm	Area Tesa cmq	Asse Neutro cm	Def. Max Cls %	Def. Max Acciaio %	Taglio (VEd) daN	Taglio Ultimo (VRd) daN	Arm. Taglio Res. minima cmq
1-A	Sx	78857 (44872)	580373	6.99	1.97	0.35	3.56	3691 (2740)	5199	1.13
	Dx	78857 (44872)	580373	6.99	1.97	0.35	3.56	-3691 (-2741)	5199	1.13

